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# Bioleaching of refractory primary copper sulfides using the metal/carbon catalysts

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https://hdl.handle.net/2324/4060152

出版情報:Kyushu University, 2019, 博士(工学), 課程博士 バージョン: 権利関係:



# **Bioleaching of refractory primary copper sulfides**

# using the metal/carbon catalysts

by

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A thesis submitted to Kyushu University for the degree of Doctor of Engineering

March 2020

#### Abstract

Recent serious depletion in copper (Cu)-grade of ore and increase in the contamination of arsenic (As) becomes an increasingly serious problem in the Cu mining industry, requiring the development of Cu exploitation process from As-bearing refractory copper minerals such as enargite (Cu<sub>3</sub>AsS<sub>4</sub>). Bioleaching, using the microbiological activity to extract metals from minerals, is considered as one of the promising technique, while this process still needs to be improved due to the slow Cu dissolution kinetics. This suggests the necessity of reaction accelerator such as a catalyst for faster Cu solubilization in order to satisfy the economic feasibility. This thesis is, therefore, consisted of two main purposes: screening of useful catalysts for bioleaching of refractory copper sulfides (**chapters 4**, **5**, and **6**; fundamental studies) and its application to practical conditions (**chapter 7**; application study).

In **chapter 1**, the background of enargite bioleaching using mesophiles/moderate thermophiles or thermophiles was overviewed. Siver-/Carbon-assisted bioleaching of chalcopyrite (CuFeS<sub>2</sub>), which is also recognized as the refractory minerals, were also summarized to propose the possible catalyst that is assumed useful for enargite bioleaching.

In chapter 2, methodologies used in this work were described.

Prior to the bioleaching experiment, in **chapter 3**, the inhibitory effect of Cu and iron (Fe) ions on molybdenum blue method (usually employed as the colorimetric As determination method) was tested for the development of As detection method that is applicable to Cu sulfide leachate. The co-presence of solo metal (e.g.  $Fe^{2+}$ ,  $Fe^{3+}$ , or  $Cu^{2+}$ ) showed no inhibition to the As determination, while the large amount of mixed metals ions (25 mM Fe<sup>2+</sup>, 25 mM Fe<sup>3+</sup>, and 50 mM Cu<sup>2+</sup>) slightly oxidized the As(III) to As(V), resulting in the underestimation of As(III) concentration. This oxidation ratio, however, remained negligibly small amount (only 4%), suggesting the applicability of the molybdenum blue method to Cu sulfide leachate for the analysis of the changes in As(III) concentration. In the following chapters, As(III) concentration was thus determined by this molybdenum blue method.

In **chapter 4**, the catalytic effect of silver on bioleaching of enargite concentrate was evaluated, and its underlying mechanisms were elucidated. Increasing addition of silver sulfide ( $Ag_2S$ ) as a silver catalyst facilitates enargite dissolution, achieving 96% final Cu recovery in the presence of 0.04%  $Ag_2S$ . On the other hand, the dissolution of pyrite, co-existing in enargite

concentrate, was suppressed with the addition of  $Ag_2S$  due to (i) the  $E_h$ -reduction along with  $Ag_2S$  addition and (ii) preferential subjectivity of  $Ag_2S$  to the oxidation by  $Fe^{3+}$ , rather than pyrite, based on the difference in rest potential. Arsenic immobilization was also enhanced by  $Ag_2S$  addition, resulting in 56% immobilization of once-dissolved As from enargite as ferric arsenate. Solid residue analyses and thermodynamical calculation revealed that enargite dissolution was promoted via the combination of two different mechanisms: (i) the replacement of Cu in enargite structure with Ag ion in the solution, and (ii) enargite transformation into easily soluble intermediate, chalcocite (Cu<sub>2</sub>S). These observations confirmed the utility of Ag as a catalyst for bioleaching of enargite concentrate. Although an alternative catalyst with similar catalytic property was not found, it was expected the possibility of an economically feasible process by the reuse of added silver.

In **chapter 5**, catalytic effect of activated carbon (AC) on bioleaching of enargite concentrate was evaluated and its underlying mechanisms were elucidated. Along with AC addition, final Cu recovery was improved from 36% (0% AC) to 53% (0.2% AC), confirming the usefulness of the AC catalyst. Lowered  $E_h$  with AC addition was observed, which was attributed to the Fe<sup>3+</sup>-reduction coupled with RISCs oxidation on the AC surface, clarified by abiotic experiment. This lowered  $E_h$  led to the suppression of pyrite dissolution, eventually resulting in the prolonged enargite dissolution without Fe passivation. Accompanying with Cu solubilization, As dissolved from enargite was successively immobilized as ferric arsenate, while it starts to re-solubilize, triggered by pyrite dissolution. Overall, control of pyrite dissolution by AC-catalyzed  $E_h$ -reduction was found a key factor of Cu solubilization and As immobilization during bioleaching of enargite concentrate.

In **chapter 6**, the physicochemical properties determining the  $E_h$ -reduction ability of AC was clarified through the comparison of various AC with different surface characteristics to find optimal AC for bioleaching of enargite concentrate. Series of abiotic experiment and Raman analysis found that the well-developed graphene structure formed via the chemical-activation process significantly promoted coupling reaction (Fe<sup>3+</sup>-reduction coupled with RISCs oxidation), which is the result of its superiority in  $E_h$ -reduction ability. On the other hand, the abundant surface functional groups on the steam-activated carbon derived from well-developed defect structure seemed to be suitable for the oxidative reaction rather than the coupling reaction. Same trend was confirmed even in the bioleaching experiment, and rather, powder AC enabled to retain faster enargite dissolution. As a result, it was concluded that the

powder-type chemical-activated carbon is the most desirable for  $E_h$ -control and enhanced Cu solubilization in bioleaching of enargite concentrate.

In **chapter 7**, the catalytic effect of AC was tested in bioleaching of As-bearing copper concentrate at the high pulp density in the stirred tank reactor for further process development and future implementation into the mining industry. Pulp density of bioleaching successfully increased up to 10% (w/v) by subsequently transferring the pre-grown culture at lower pulp density to that at higher pulp density. AC addition to this high pulp density bioleaching improved Cu recovery from 80% (0% AC) to almost 100 % (0.05% and 0.5% AC), by accelerating the dissolution of chalcopyrite and enargite via (i) optimal potential achievement by AC-catalyzed  $E_h$ -control and (ii) enhanced galvanic reaction though the frequent contact between AC and minerals. Moreover, As immobilization as Fe-As precipitates were also facilitated, confirming the utility of AC even in the practical condition (high pulp density, complex mineralogy, and reactor scale).

In **chapter 8**, whole findings were summarized as a conclusion, and the recommendations for future work were provided.

#### 要旨

近年の銅生産の現場における、鉱石中銅品位の低減化、それに伴う砒素含有率の増加は 深刻な問題となっており、enargite (Cu<sub>3</sub>AsS<sub>4</sub>)を始めとした砒素含有銅鉱物中からの銅回収プ ロセスの発展が熱望されている。微生物反応を利用したバイオリーチングは有効な技術とし て注目を集めているが、銅浸出速度に依然として課題があり、触媒等、反応促進要因の必要 性が示唆されている。本博士論文では、難処理硫化銅鉱物のバイオリーチングにおける有 用触媒の探求および比較 (第4、5、6章;基礎研究)、さらに、より実践的条件への適応 (第7章;応用研究)で構成される。

第1章では、砒素含有鉱物として従来研究対象とされてきた enargite のバイオリーチングに 関して総括した。さらに、enargite と並んで難処理性が認識されている chalcopyrite (CuFeS<sub>2</sub>) のバイオリーチングにおいて、有用性が示唆されている銀触媒および炭素触媒に関してまと め、enargite のバイオリーチングにも適応可能な候補を提示した。

第2章では、本博士論文中の実験における一般的手順および分析方法等について記述した。

**第3章**では、実験の前段階として、砒素含有鉱物のバイオリーチング中において重要となる、砒素の定量法に関する検討を行った。具体的には、従来砒素定量に利用されてきた吸光光度法であるモリブデンブルー法の銅および鉄イオンによる阻害を議論し、銅浸出溶液中の砒素定量が同法によって可能か検討した。各種イオンが単独で砒素と共存する際は定量への阻害は確認されなかったが、多量の鉄および銅イオンが共存する際には、As(III)のAs(V)への酸化が確認され、サンプル中のAs(III)濃度を過小評価する結果となった。しかし、その酸化割合は4%程度に留まったため、ほぼ無視できる程度の誤差と考えられ、モリブデンブルー法がAs(III)濃度変化の傾向評価に利用できることが示された。以後の章において、As(III)濃度は、このモリブデンブルー法によって定量した。

第4章では、enargite 精鉱のバイオリーチングにおける銀触媒添加の影響を評価し、代替 触媒探求のためにメカニズム解明に取り組んだ。銀触媒として硫化銀を添加するに伴い、バ イオリーチング中での enargite からの銅浸出が促進され、0.04% (w/v)の硫化銀存在下で、72 日後に 96%の最終銅浸出率を達成した。一方で、enargite 精鉱中に共存する pyrite (FeS<sub>2</sub>) の溶解は(i) 硫化銀の添加に伴う溶液電位の低減化および(ii) 硫化銀自身の低い静止電 位に起因する選択的酸化よって抑制された。銀の添加に伴い、非晶質の ferric arsenite とし て最大 56%の砒素が不動化していることも認められた。種々の固体残渣分析および熱力学 的考察により、enargite の溶解は(i) 溶液中の銀イオンと enargite 結晶中の銅イオンの置換に よる銅浸出、および、(ii) 中間体 Cu<sub>2</sub>S を介した銅浸出の 2 つのメカニズムによって進んでい ることが推察された。以上より、enargite 精鉱のバイオリーチングにおける銀触媒の極めて高い有用性が確認された。同様のメカニズムで作用する安価な代替触媒の発見には至らなかったが、添加した銀触媒の回収により、経済的なプロセス実現の可能性が示唆された。

第5章では、enarigte 精鉱のバイオリーチングにおける活性炭添加の影響を評価し、そのメ カニズム解明に取り組んだ。活性炭添加に伴い 36% (0% AC)であった最終銅回収率が 53% (0.2%)へと向上し、活性炭の有用性が示された。活性炭添加に伴う溶液電位の低減化が確 認され、化学実験により、活性炭表面での Fe<sup>3+</sup>還元と RISCs (Reduced inorganic sulfur compounds; 無機還元型硫黄化合物)酸化のカップリング反応が、その要因であると判明し た。これに伴い、高電位で高速溶解する pyrite の溶解も抑制され、これが、鉄被膜が存在し ない状態での息の長い enargite の溶解に繋がることにより、最終銅浸出率が向上したと予想 された。砒素は enargite の溶解に伴い随時 ferric arsenate として沈殿していたが、pyrite の溶 解に伴い沈殿が溶解、液中に再溶出した。以上を踏まえ、活性炭による電位低減化により、 pyrite の溶解をコントロールすることが、enargite 精鉱のバイオリーチングでの銅浸出および 砒素不動化において極めて重要であると判明した。

第6章では、種々の活性炭を比較検討することにより、活性炭の電位低減化能を決定する物性を解明し、enargite精鉱のバイオリーチングに最適な活性炭の選定を行った。結果として、薬品賦活炭が有する発達したグラフェン構造により、Fe<sup>3+</sup>還元-RISCs酸化カップリング反応が促進され、最も優れた電位低減化効果を示すことが判明した。一方で水蒸気賦活炭はそのディフェクト構造の豊富さから表面官能基を多く有し、カップリング反応よりも酸化反応の影響が顕著に見受けられた。バイオリーチングにおいても同様に薬品賦活炭が優れた溶液電位低減化効果を示し、さらに粉状の活性炭を用いると、溶液電位低減化による enargite の溶解の低速化を打ち消すように銅浸出が促進されることも確認された。結果として、粉状の薬品賦活炭が enargite 精鉱のバイオリーチングにおいて最も適していると結論付けた。

第7章では、産業化を視野に入れたプロセスの発展のために、リアクターを用いた高パル プ濃度砒素含有銅精鉱バイオリーチングでの活性炭の影響評価を行った。中度好熱性微 生物叢を高パルプ濃度の系に段階的に継代することにより、最終的に 10%までパルプ濃度 を向上させることに成功した。ここに活性炭を添加したところ、活性炭無添加では易溶解性鉱 物の溶解が中心的で80%に留まった銅浸出が、活性炭の(i) 溶液電位の低減化効果および (ii) 高接触頻度によるガルバニック反応促進効果により、enargite および chalcopyrite の溶解 を著しく促進、ほぼ全ての銅溶出につながった。また、砒素 – 鉄沈殿としての砒素不動化効 率も活性炭の存在により向上し、より実践的な実験条件下(高パルプ濃度、複雑組成銅精鉱 利用、リアクタースケール)においても活性炭の有用性を確認することができた。

第8章では、上記検討結果を総括して結論とし、将来的な研究への提言を記した。

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01-089-1370), En: enargite ( $Cu_3AsS_4$ ; PDF No. 00-035-0775), Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>; PDF No. 01-070-3755).

- Figure 4.4 Microbial population structure on day 15, 30, and 72 in pp. 104 bioleaching cultures of enargite concentrate at 0% and 0.04% of Ag<sub>2</sub>S. N1, ICP, and KU indicate *Am. ferrooxidans* ICP, *Sb. sibiricus* N1, and *At. caldus* KU, respectively.
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- Figure 5.3 Changes in the Fe<sup>2+</sup> concentration (a),  $E_h$  (b), and sulfate pp. 144 production (c) during abiotic experiment for evaluation of catalytic capability of AC. Cultures containing 0.1% (w/v) AC + Fe<sup>3+</sup> ( $\blacktriangle$ ; condition (i)), 0.1% AC + Fe<sup>2+</sup> ( $\bigtriangledown$ ; condition (ii)), 0.1% AC + tetrathionate ( $\diamondsuit$ ; condition (iii)), Fe<sup>3+</sup> + tetrathionate ( $\bigcirc$ ; condition (iv)), 0.1% AC + Fe<sup>3+</sup> + tetrathionate ( $\blacksquare$ ; condition (v)), or 0.1% AC + Fe<sup>3+</sup> + yeast extract ( $\times$ ; condition (vi)) were tested. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.
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- Figure 5.6 Relationship between solution potential (*E*<sub>h</sub>) and electrode pp. 150 potential (a) of enargite (●), pyrite (■), and AC (◆), or galvanic current (b) in enargite-pyrite (■) or enargite-AC (◆) system. Difference in the electrode potential between minerals corresponds to the galvanic electromotive force.
- Figure 5.7 Kinetic modeling on abiotic leaching (open symbol) or pp. 152 bioleaching (closed symbol) of enargite concentrate in the presence of 0% ( $\bigcirc$ ,  $\bigcirc$ ), 0.1% ( $\blacktriangle$ ), 0.2% ( $\checkmark$ ), and 0.3% (w/v) ( $\square$ ,  $\blacksquare$ ) AC; (a) surface chemical reaction (1 (1-X)<sup>1/3</sup> =  $k_r$ t) and (b) diffusion through product film (1 + 2(1-X) 3(1-X)<sup>2/3</sup> =  $k_d$ t). Linear lines were drawn until where R<sup>2</sup> values increase.
- Figure 5.8 Changes in the concentration of total soluble As (a), pp. 156 immobilized As (b), and soluble As (III) (c) during abiotic leaching (open symbol) or bioleaching (closed symbol) of enargite concentrate at 0% (○, ●), 0.1% (▲), 0.2% (▼), or 0.3% (w/v) (□, ■) of AC. Backscattered electron image of an enargite grain bioleached for 30 or 60 days with 0.2% (w/v) AC at the 2700-fold or 1000-fold magnification was also depicted, respectively. White brighter grain (enargite) was covered with gray layer at day 30, which disappeared at day 60.
- Figure 5.9 EPMA elemental mapping of enargite concentrate residue pp. 157 bioleached for 30 days with 0.2% AC: The backscattered electron image at 3000-fold magnification (a) was mapped for Cu (b), S (c), Fe (d), As (e) and O (f). The surface of an enargite grain is covered with Fe-, As-, O-containing secondary mineral, ferric arsenate.
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- Figure 6.5 Changes in pH (a), E<sub>h</sub> (b), Fe<sup>2+</sup> concentration (c), and total Fe pp. 176 concentration (d), during abiotic experiment in the presence of 10 mM Fe<sup>3+</sup> for the evaluation of catalytic capability of three AC: A-powder (●), B-granular (▲), and B-powder (●). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.
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- Figure 6.13 Summary of results in bioleaching of enargite concentrate in pp. 188 the absence ( $\bigcirc$ ) or presence of 0.1 ( $\triangle$ ), 0.2 ( $\bigtriangledown$ ), and 0.3% (w/v) ( $\blacksquare$ ) B-granular as the AC catalyst; (a) pH, (b) *E*<sub>h</sub>, (c) cell density , (d) Fe<sup>2+</sup> concentration, (e) total Cu concentration, (f) total Fe concentration, (g) total As concentration, and (f) immobilized As concentration. Data

points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

- Figure 6.14 Summary of results in bioleaching of enargite concentrate in pp. 189 the absence ( $\bigcirc$ ) or presence of 0.02 ( $\checkmark$ ), 0.04 ( $\checkmark$ ), 0.06 ( $\diamondsuit$ ), and 0.08% (w/v) ( $\blacksquare$ ) B-powder as the AC catalyst; (a) pH, (b)  $E_h$ , (c) cell density , (d) Fe<sup>2+</sup> concentration, (e) total Cu concentration, (f) total Fe concentration, (g) total As concentration, and (f) immobilized As concentration. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.
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- Figure 6.17 Kinetic fitting with surface chemical reaction model on pp. 193 bioleaching of enargite concentrate in the presence of 0 (●), 0.02 (▲), 0.04 (♥), 0.06 (◆) and 0.08% (■) A-powder (a) or B-powder (b), or 0 (●), 0.1 (▲), 0.2 (♥), and 0.3% (■) B-granular (c). Fitting duration was restricted until when rapid Fe dissolution was initiated during bioleaching.
- Figure 6.18 Kinetic fitting with diffusion through product film model on pp. 194 bioleaching of enargite concentrate in the presence of 0 (●), 0.02 (▲), 0.04 (▼), 0.06 (◆) and 0.08% (■) A-powder (a) or B-powder (b), or 0 (●), 0.1 (▲), 0.2 (▼), and 0.3% (■) B-granular (c). Fitting duration was restricted until when rapid Fe dissolution was initiated during bioleaching.

- Figure 7.1 Changes in pH (a), E<sub>h</sub> (b), cell density (c), total soluble Cu pp. 206 concentration (d), total soluble Fe concentration (e), and total soluble As concentration (f) during bioleaching of D3 concentrate at the pulp density of 2% (●), 3% (▲), 5% (▼), 8% (◆), and 10% (■). Pre-grown culture was inoculated at day 1.
- Figure 7.2 Composition of Cu (a), Fe (b), and As (c) contents dissolved pp. 207 from each mineral in D3 concentrate.
- Figure 7.3 Changes in pH (a), E<sub>h</sub> (b), cell density (c), total soluble Cu pp. 209 concentration (d), Fe(II) concentration (e), total soluble Fe concentration (f), As(III) concentration (g) and total soluble As concentration (h) during bioleaching of D3 concentrate at the pulp density of 10% in the absence (●) or presence of 0.05% (▲) and 0.5% (w/v) (■) AC. Pre-grown culture was inoculated at day 1.
- Figure 7.4 Changes in the Cu (a), Fe (b), and As recovery (c) corrected pp. 210 by the solution volume during bioleaching of D3 concentrate at the pulp density of 10% in the absence (●) or presence of 0.05% (▲) and 0.5% (w/v) (■) AC. Pre-grown culture was inoculated at day 1.
- Figure 7.5 Separately collected solid residue after 30 days of bioleaching pp. 211 of D3 concentrate in the absence or presence of 0.05% and 0.5% AC. Reacted residue: floated and well-mixed part of leaching reside with whiter color. Unreacted residue: settled and coagulated part of leaching residue with black color.
- Figure 7.6 Changes in the Cu (a), Fe (b), and As recovery (c) corrected pp. 214 by the solution volume and the amount of unreacted residue during bioleaching of D3 concentrate at the pulp density of 10% in the absence (●) or presence of 0.05% (▲) and 0.5% (w/v) (■) AC. Pre-grown culture was inoculated at day 1.
- Figure 7.7 MLA results of original D3 concentrate and bioleached pp. 215 reacted residue recovered on day 30 from cultures containing 0%, 0.05%, or 0.5% AC.

- Figure 7.8 Changes in the  $E_{normal}$  during bioleaching of D3 concentrate at pp. 216 the pulp density of 10% in the absence ( $\bigcirc$ ) or presence of 0.05% ( $\land$ ) and 0.5% (w/v) ( $\square$ ) AC.
- Figure 7.9 X-ray diffraction patterns of bioleached residue recovered on pp. 218 day 30 from cultures containing 0%, 0.05%, or 0.5% AC. E: enargite (Cu<sub>3</sub>AsS<sub>4</sub>; PDF No. 00-035-0775), Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>; PDF No. 01-070-3755), J: jarosite  $(K(Fe_3(SO_4)_2(OH)_6);$ PDF No. 01-076-0629), chalcopyrite (CuFeS<sub>2</sub>; Cp: PDF No. 01-075-6866), Tennantite  $(Cu_{12}As_4S_{13};$ PDF No. 01-074-1027)..
- Figure 7.10 SEM image (a) and elemental mapping (b-f) of reacted pp. 219 residue recovered at day 30 from the culture containing 0.5% AC: Cu (b), As (c), S (d), O (e), and Fe (f). Aggregation of ultrafine particle (< 1  $\mu$ m) composed of Cu, As, S, O, and Fe was found.
- Figure 8.1 Brief flowsheet of the exploitation process for As-bearing pp. 229 copper ores.
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- Figure 8.3 Proposed flowsheet of AC-catalyzed bioleaching of enargite pp. 231 concentrate.

#### Abbreviations

ABS	Acidophilic basal salts
AC	Activated carbon
Ac.	Acidianus
Am.	Acidimicrobium
AMD	Acid mine drainage
At.	Acidithiobacillus
As(III)	Arsenite (H <sub>3</sub> AsO <sub>3</sub> )
As(V)	Arsenate ( $H_2AsO_4^-$ )
ATR-FTIR	Attenuated total reflection-Fourier transform infrared
	spectroscopy
BET	Brunauer–Emmett–Teller
Cu <sup>2+</sup>	Cupric copper
EPMA	Electron probe micro analyzer
EPS	Extracellular polymeric substances
HBS	Heterotrophic basal salts
ICP-OES	Inductively coupled plasma optical emission spectrometry
Lp.	Leptosprillum
Ms.	Metallosphaera
MLA	Mineral liberation analyzer
Fe <sup>2+</sup>	Ferrous iron
Fe <sup>3+</sup>	Ferric iron
Fm.	Ferrimicrobium
PCR	Polymerase chain reaction
Sf.	Sulfolobus
Sb.	Sulfobacillus
SEM	Scanning electron microscope
w/v	weight per volume
XRD	X-ray diffraction

Introduction

#### **1.1 Introduction**

#### 1.1.1 Copper

Copper (Cu) is one of the essential metals for the daily life of human beings. Its high electrical and heat conductivity are applied for electric wires and cooking devices, respectively. The mixture of it with other metals (i.e. alloy) generate high quality materials, being able to apply for wider usages. Recent development of electronic devices also accelerates the consumption of copper as its components. This situation shows that stable copper supply is necessary for the future human society.

Chile is well-known as the best copper producer in the world to meet such a large amount of copper demand. The world copper production in 2011 was reported as 16,100,000 ton, and the copper production in Chile accounts for 34% of it as a major copper producer, followed by Peru, China, USA, Australia, Zambia, Russia, Indonesia, Canada, and Congo. On the other hand, the total minable reserve is considered as 690,000,000 tons in 2011, meaning that world copper might be exhausted approximately 30 years later based on brief calculation.

Majority of copper reserves are derived from porphyry copper deposit that accounts for 65% of world copper reserve. This type of deposit is composed of three types of layers: (i) copper oxides, (ii) secondary copper sulfides, and (iii) primary copper sulfides. A layer of copper oxides exist on the upper part of the deposit and show high coppergrade (> 1%), consisting of copper oxides such as cuprite (Cu<sub>2</sub>O) and malachite (Cu<sub>2</sub>CO<sub>3</sub>(OH)<sub>2</sub>). Under the oxides layer, there are secondary copper sulfides such as chalcocite (Cu<sub>2</sub>S) and covellite (CuS). Although these secondary sulfides layer shows lower copper-grade (1-3%) than that of copper oxides, today, it is also used for copper production due to its high solubility into leaching solution. At the bottom part of the deposit, primary copper sulfides are present such as chalcopyrite (CuFeS<sub>2</sub>), bornite (Cu<sub>5</sub>FeS<sub>4</sub>), and enargite (Cu<sub>3</sub>AsS<sub>4</sub>), showing the lowest copper-grade (< 1%) and refractory property.

The exploitation of these primary sulfides has hardly been conducted in the past decades due to its difficulty in application to real operation. However, researchers' attention has recently been shifted toward these primary minerals since (i) the reserve of oxides and secondary sulfides were continuously decreasing and (ii) they (i.e. primary sulfide minerals) account for 70% of the world copper reserve (Sillitoe, 2010).

This situation requires the development of technique to recover the copper from primary copper sulfides.

#### 1.1.2 Arsenic

Arsenic (As) is the 20th most abundant element in the earth's crust, and it is basically used for semiconductor products such as gallium arsenide (GaAs), which usually compose light-emitting diode (LED) and high-speed transistor. However, arsenic shows high toxicity on the living things. Since arsenic is categorized as a carcinogen, environmental regulation for arsenic exposure is strictly set as 0.01 mg/L by the World Health Organization (WHO) in 1993 (Leist et al., 2000).

There are two types of As occurrence: (i) natural sources and (ii) anthropogenic sources. In the former case, arsenic in the mineral is released via rock weathering, including the effect of microorganisms' activity (Oremland and Stolz, 2005), while, in the latter case, it is derived from human activities, such as mining, manufacturing, industry and chemical weapon (Lièvremont et al., 2009). As a result, serious arsenic problems have been reported in many parts of the world such as Argentina, Bangladesh, Chile, China, Hungary, India (West Bengal), Mexico, Romania, Taiwan, Vietnam, and many parts of the USA (Smedley and Kinniburgh, 2002).

Arsenic is a common impurity in the metallurgical process because it is frequently associated with sulfur, iron, copper, silver, and gold. Current techniques to remove these arsenic contaminations are as below: ion exchange, adsorption on activated alumina and carbon, ultrafiltration, reverse osmosis, and co-precipitation or adsorption by metals (Leist et al., 2000). However, these techniques still have some problems with its cost and stability. The attention against arsenic treatment is therefore increasing, and it is necessary to improve the technique of arsenic removal and immobilization.

There are two predominant chemical oxidation states of arsenic in aqueous phase: trivalent arsenic (As(III)) and pentavalent arsenic (As(V)) (Riveros et al., 2001). Since it is well-known that trivalent arsenic is more toxic than pentavalent one, oxidation of trivalent to pentavalent is necessary as the first step of the arsenic treatment process (Matschullat, 2000).

#### **1.1.3 Primary sulfide minerals**

As mentioned above, primary sulfide minerals have increasingly been paid attention by researchers due to the harsh situation of future copper supply. In this section, as an example of primary sulfide minerals, chalcopyrite (CuFeS<sub>2</sub>) and enargite (Cu<sub>3</sub>AsS<sub>4</sub>) are introduced.

#### 1.1.3.1 Chalcopyrite

Chalcopyrite (CuFeS<sub>2</sub>) is one of the primary sulfide minerals, showing golden yellow color, which is composed of copper, iron, and sulfur in the tetragonal crystal structure (Burdick et al., 1917). Since this mineral accounts for the majority of primary sulfide ore, researchers tend to employ chalcopyrite as an objective material. However, its refractoriness disturbs the economical operation of copper extraction from it.

#### 1.1.3.2 Enargite

Enargite (Cu<sub>3</sub>AsS<sub>4</sub>) is also one of the primary sulfide minerals, showing black color. This mineral is composed of copper, arsenic, and sulfur in the orthorhombic crystal structure and well-known as semiconducting materials (Henao et al. 1994). Enargite has several properties in common with chalcopyrite: (i) sulfide mineral composed of copper and another metal and (ii) refractory behavior against leaching treatment. It is generally associated with chalcopyrite, however, its similar property with chalcopyrite prevents effective separation.

Moreover, arsenic, included in enargite structure, requires arsenic treatment process after the leaching process, which is inferior to chalcopyrite from the economic point of view. However, the potential of enargite as the copper resource is not negligible, thus requiring the development of a novel process for enargite treatment, where only copper can be extracted, but arsenic remains in the solid phase.

# **1.2.** The application of bioleaching for efficient copper extraction from sulfide minerals

#### 1.2.1 Pyrometallurgy and hydrometallurgy

Until now, a number of techniques to obtain metals from minerals have been proposed and improved. These techniques are able to be divided into two categories: (i) pyrometallurgy, and (ii) hydrometallurgy. The former techniques such as calcination, roasting, smelting, and refining, are applicable to only high Cu-grade ore because the heating process is economically infeasible for the application to low Cu-grade ore. On the other hand, the latter techniques such as bioleaching, acid leaching, pressure leaching, are effective in the exploitation of low Cu-grade ore due to its lower cost in terms of energy consumption. Especially, bioleaching is a promising process from economic and environmental points of view. In this section, the definition, general mechanism, advantages and disadvantages of bioleaching are summarized.

#### 1.2.2. Bioleaching

Bioleaching is one of the biohydrometallurgical techniques to extract objective metals from minerals by using microorganisms. Various metals can be the candidate of the objective metals, such as copper (Yang et al., 2009), zinc (Deveci et al., 2004), lead (Nasernejad et al., 1999), gold (Curreli et al., 1997), silver (Frías et al., 2002) and cobalt (Olson et al., 1990).

#### 1.2.2.1 General mechanism of bioleaching

During the bioleaching process, microbial reactions are key factors, contributed by iron-oxidizing and sulfur-oxidizing microorganisms.

When the biological reaction proceeds, three different bioleaching strategies are considered (Rodriguez et al., 2003);

(i) Indirect bioleaching, whereby the microbial action is restricted to re-generation of the bioleaching reagent (i.e.  $Fe^{3+}$ )

(ii) Contact bioleaching, which entails attachment of microorganisms to the mineral surface and these organisms provide the medium and facilitate the mineral attack through an electrochemical dissolution involving Fe<sup>3+</sup> contained in the microbe's extracellular polymeric substances (EPS)

(iii) Cooperative bioleaching, which entails cooperation between microorganisms attached to the mineral surface and free bacteria in solution. The attached microbes, through contact bioleaching, release chemicals to the solution that constitute the energy source for the organisms that are free in solution.

In order to comprehend the general mechanism of bioleaching, pyrite (FeS<sub>2</sub>) was taken as an example, since it is general impurity of ores and dissolution of pyrite is the fundamental reaction of bioleaching.

At the beginning of the bioleaching reaction, pyrite is slightly oxidized by the oxygen when pyrite is exposed to the air. Under such condition, if those ores become wet by rainwater, pyrite starts to dissolve and release  $Fe^{2+}$  and sulfate.

$$2\text{FeS}_2 + 7\text{O}_2 + 2\text{H}_2\text{O} \rightarrow 4\text{SO}_4^{2-} + 2\text{Fe}^{2+} + 4\text{H}^+ \text{ (chemical reaction)}$$
 (Eq. 1-1)

Produced Fe<sup>2+</sup> is then oxidized by iron-oxidizing microbes to Fe<sup>3+</sup>.

$$4Fe^{2+} + O_2 + 4H^+ \rightarrow 4Fe^{3+} + 2H_2O \text{ (biological reaction)}$$
(Eq. 1-2)

Oxidized iron (i.e.  $Fe^{3+}$ ) is used for further oxidation of pyrite due to its property as strong oxidizer, producing  $Fe^{2+}$  and elemental sulfur.

$$\text{FeS}_2 + 2\text{Fe}^{3+} \rightarrow 3\text{Fe}^{2+} + 2\text{S}^0$$
 (chemical reaction) (Eq. 1-3)

Elemental sulfur formed by the above reaction is the main reaction-inhibitor for further dissolution of pyrite. In order to promote the reaction even after the formation of elemental sulfur, sulfur-oxidizing microbes oxidize it to sulfate and remove it from pyrite surface.

$$2S^0 + 3O_2 + 2H_2O \rightarrow 2SO_4^{2-} + 4H^+$$
 (biological reaction) (Eq. 1-4)

As a result, further dissolution of pyrite continuously proceeds. The summarized reaction of pyrite dissolution by microbiological oxidation is described as below;

$$FeS_2 + 14Fe^{3+} + 8H_2O \rightarrow 15Fe^{2+} + 2SO_4^{2-} + 16H^+$$
 (Eq. 1-5)

In the bioleaching process, these reactions must be strictly managed. If these reactions spontaneously occur, the serious environmental problem occur since the highly acidic water containing large amount of heavy metals is discharged into the river, which is called acid mine drainage (AMD).

In the case of enargite bioleaching, the basic reaction is almost same. However, in the case of enargite bioleaching, since enargite includes no iron in its composition,  $Fe^{3+}$  as oxidizing reagent should be externally supplied.

$$Cu_{3}AsS_{4} + 11Fe^{3+} 4H_{2}O \rightarrow 3Cu^{2+} + 11Fe^{2+} + H_{2}AsO_{4} + 4S^{0} + 6H^{+}$$
(Eq. 1-6)
(chemical reaction)

As mentioned above,  $Fe^{2+}$  produced via the oxidation of enargite is re-oxidized to  $Fe^{3+}$  by iron-oxidizing microbes.

As a result, further dissolution of enargite is continuously proceeded as shown in Fig. 1.1.

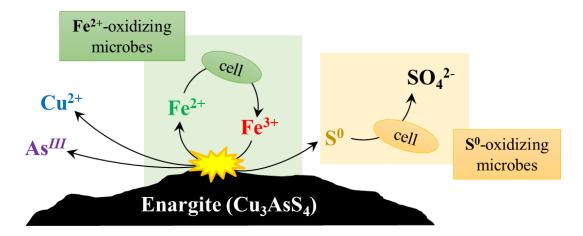


Fig. 1.1 The schematic image of enargite bioleaching.

#### 1.2.2.2 Representative microorganisms used for bioleaching

#### At. (formerly Thiobacillus) ferrooxodans

*At. ferrooxidans* is an autotrophic, acidophilic, and moderately thermophilic bacterium, capable of growing on ferrous iron or sulfur compounds as the electron donor. In general, it grows optimally at pH 1.5-2.5 at 45-50°C. Therefore, it is commonly found in acid mine drainage containing various metal ions at low pH. Although it basically grows under aerobic conditions, it is able to grow under anaerobic conditions using ferric iron as the electron acceptor, instead of oxygen (Ohmura et al., 2002).

#### At. (formerly Thiobacillus) thiooxidans

*At. thiooxidans* is an autotrophic, acidophilic, and mesophilic bacterium, capable of growing on elemental sulfur as a primary electron donor under strictly aerobic conditions. The optimum temperature and pH for its growth are 28-30°C and less than 4.0, respectively. Additionally, it grows also on thiosulfate ( $S_2O_3^{2-}$ ) and tetrathionate ( $S_4O_6^{2-}$ ), but not hydrogen sulfide and sulfides (Waksman et al., 1922).

#### At. (formerly Thiobacillus) caldus

*At. caldus* is an mixotrophic, acidophilic, and moderately thermophilic bacterium, capable of growing on elemental sulfur and tetrathionate, but not on ferrous iron. The optimum temperature and pH for active growth of *A. caldus* are 45°C and 2.0-2.5, respectively (Hallberg et al., 1994).

#### Ac. brierleyi

*Ac. brierleyi* is a thermophilic and extremely acidophilic archaeon. It autotrophically grows on elemental sulfur and ferrous iron as the electron donor, at optimum pH of 1.5-2.0 and temperature of 70°C. It is able to also grow under anaerobic conditions by reducing sulfur (Segerer et al., 1986).

#### Lp. ferrooxidans

*Lp. ferrooxidans* is an obligately autotrophic, mesophilic, and acidophilic bacterium, capable of growing ferrous iron, but incapable of oxidizing elemental sulfur and RISCs (reduced inorganic sulfur compounds) (Hippe 2000). The optimum temperature and pH

for its growth are 25-35°C and 2.5-3.0, respectively. Therefore, *L. ferrooxidans* is often applied to bioleaching of sulfide minerals with *At. ferrooxidans* or *At. thiooxidans* (Bosecker, 1997).

#### Lp. ferriphilum

*Lp. ferriphilum* is an obligately autotrophic, moderately thermophilic, and acidophilic bacterium. It grows aerobically at optimum pH of 1.5 and temperature of 43°C. It obtains energy for growth by oxidizing ferrous iron as an electron donor. It was reported to grow on also pyrite, but not tetrathionate (Okibe et al., 2003).

#### Sb. thermosulfidooxidans

*Sb. thermosulfidooxidans* is a moderately thermophilic and acidophilic bacterium, capable of growing either heterotrophically or autotrophically on ferrous iron, tetrathionate, elemental sulfur, thiosulfate, and sulfide minerals (Pina et al., 2010; Xia et al., 2010). It is able to grow in a wide range of temperature and pH; at 20-60°C and pH 1.5-5.5, respectively. Optimum temperature and pH are 50-55°C and 1.9-2.4, respectively.

#### Sf. metallicus

*Sf. metallicus* is an extremely thermophilic, obligately autotrophic, and acidophilic archaeon. It grows aerobically at 50-75°C and pH 1.0-4.5 on elemental sulfur and sulfide (Huber et al., 1991; Gautier et al., 2008; Morales et al., 2011). Additionally, its growth via oxidation of pyrite and ferrous iron was also observed (Norris et al., 2000).

#### **1.2.3 Enargite bioleaching**

As mentioned above, recent depletion of high-grade copper ore has directed the researcher's attention toward low-grade and refractory sulfides such as chalcopyrite (CuFeS<sub>2</sub>) and enargite (Cu<sub>3</sub>AsS<sub>4</sub>). In order to improve dissolution efficiency of these minerals, not only chemical leaching such as pressure leaching (Ruiz et al., 2011; Padilla et al., 2015) and acid leaching (Safarzadeh and Miller, 2014) but also biological leaching has been investigated by several research groups (Acevedo et al., 1998; Sasaki et al., 2009). Since enargite includes arsenic in its structure, researchers have tended to

engage in the study on chalcopyrite bioleaching, rather than enargite bioleaching, resulting in the limited number of studies involving in enargite bioleaching. However, according to the recent gradual increase of contamination of arsenic as an impurity in copper deposit, it has become no longer negligible to study involving in bioleaching of enargite. In this section, recent developments of techniques of enargite bioleaching are introduced.

#### **1.2.3.1** Bioleaching of enargite by using thermophiles

Since enargite shows highly-refractory property during the leaching process, higher temperature conditions (60-70°C) are favorable for faster enargite dissolution, despite its economic infeasibility in real operation.

Escobar et al. (2000) conducted bioleaching of enargite at 70°C using *Sulfolobus* BC, which is thermophilic and extremely acidophilic iron- and sulfur-oxidizing microorganisms. In the study, enargite was bioleached at 70°C by *Sulfolobus* BC in shake-flasks experiments and 52% of copper extraction was obtained after 23 days of leaching at highest. In the absence of Fe<sup>3+</sup> as an oxidizing reagent, *Sulfolobus* BC catalyzed the bioleaching of enargite possibly based on the direct mechanism, where microbe adheres onto the surface of enargite and attack it. In this case, since solubilized arsenic by microbial attack remained in the solution, 90% of inhibition of bacterial growth and activity was observed due to the toxicity of arsenic. On the other hand, in the presence of 1 g/L of Fe<sup>3+</sup>, it was precipitated with arsenic as ferric arsenate to immobilize arsenic in the solid phase, preventing the presence of highly concentrated arsenic in the solution. As a result, no significant bacterial inhibition occurred, resulting in proceeding further dissolution of enargite. This arsenic behavior in the leaching solution is one of the key factors during bioleaching of enargite.

Muñoz et al. (2006) conducted bioleaching of enargite by using thermophilic archaeon, *Sf. metallicus*, at 68°C. The results obtained in this study obviously showed that high-temperature condition (68°C) is significantly effective on enargite dissolution: copper recovery reached over 84%. Additionally, the amount of iron precipitates formed on the surface of enargite increased at higher temperature, indicating that the immobilization of arsenic co-precipitated with iron was also enhanced with increase in temperature.

Lee et al. (2011) also conducted comparative bioleaching of enargite at ambient laboratory temperature and higher temperature,  $65^{\circ}$ C. High copper recovery (> 81%) was also observed as same as the study conducted by Muñoz et al. (2006) at high temperature, while almost no copper extraction was seen at lower temperature conditions.

Takatsugi et al. (2011) and Sasaki et al. (2011) used *Ac. brierleyi* as iron- and sulfuroxidizing microorganism during bioleaching of enargite at 70°C. In these studies, over 90% of copper extraction was achieved within 27 days. Moreover, arsenic recovery was only 6%, while almost all copper was solubilized from enargite, indicating that the majority of solubilized arsenic was re-immobilized during the bioleaching period. They indeed confirmed the formation of scorodite (FeAsO<sub>4</sub>·2H<sub>2</sub>O), which is one of the forms of ferric arsenate with high crystallinity and stability, and low iron requirement. These studies proposed the possibility of an ideal bioleaching process, where simultaneous achievement of both high copper extraction and arsenic immobilization can be realized. The studies of enargite bioleaching using thermophiles under different conditions, such as microbiological system, initial pH, temperature, and pulp density were summarized as below.

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	Microorganism(s)	Initial pH	Temp. (°C)	Cu leached As leached (%) (%)	As leached (%)	Leaching periods (days)	Pulp density (%)	Enargite grade (%)	Volume	Conditions	Ref.
	Sulfolobus BC	1.6	70	52	17	23	2	≈100	100 mL (△250 mL)	$1.0 \text{ g/L Fe}^{3+}$	Escobar et al 2000
	Sulfolobus BC	1.6	70	12	12	23	2	≈100	100 mL (∆250 mL)	without Fe <sup>3+</sup>	Escobar et al 2000
	Sf. metallicus	1.8	68	84	N.D.	34	10	16	40 mL (△500 mL)		Munoz et al 2006
10	Sf. metallicus	1.8	70	98	N.D.	30	5	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008
	Sf. metallicus	1.8	70	93	N.D.	30	10	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008
	Sf. metallicus	1.8	70	65	N.D.	30	15	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008
	Sf. metallicus	1.8	70	42	N.D.	30	20	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008
	Sf. metallicus	1.8	70	36	N.D.	30	25	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008
	Sf. metallicus	1.8	70	27	N.D.	30	30	16.4	300 mL (△1000 mL)	Successively adapted culture	Astudillo et al 2008

Table 1.1 The list of the previous studies in enargite bioleaching using thermophiles.

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ions Ref.	aptation 2008	dominant ing mineral Lee et al 2011	dominant ing mineral Lee et al 2011	ominant Lee et al 2011					
Conditions	Without adaptation	Chalcocite dominant as Cu containing mineral	Chalcocite dominant as Cu containing mineral	Covellite dominant					
Volume	300 mL (∆1000 mL)	300 mL (△1000 mL)	Column leaching	Column leaching	Column				
Enargite grade (%)	16.4	16.4	16.4	16.4	16.4	16.4	2.45% as Cu (4.2% as enargite)	5.62% as Cu (2.9% as enargite)	0.63% as Cu
Pulp density (%)	5	10	15	20	25	30	1	ı	ı
Leaching periods (days)	30	30	30	30	30	30	264	475	335
As leached (%)	N.D.	N.D.	N.D.						
Cu leached (%)	61	52	29	15	11	6	96	86	88
Initial pH Temp. (°C) Cu leached As leached (%) (%)	70	70	70	70	70	70	70	70	02
Initial pH	1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8
Microorganism(s)	Sf. metallicus	Acidianus, Metallospheara, Sulfolobus	Acidianus, Metallospheara, Sulfolobus	Acidianus, Metallospheara,					

L	Microorganism(s)	Initial pH	Temp. (°C)	Initial pH Temp. $(^{\circ}C)$ Cu leached As leached $(^{\circ})$ $(^{\circ})$	As leached (%)	Leaching periods (days)	Pulp density (%)	Enargite grade (%)	Volume	Conditions	Ref.
	Acidianus, Metallospheara, Sulfolobus	1.8	70	95	N.D.	577	ı	0.59% as Cu (20% as enargite)	Column leaching	Covellite dominant as Cu containing mineral	Lee et al 2011
	Acidianus, Metallospheara, Sulfolobus	1.8	70	81	N.D.	335	ı	0.73% as Cu (94.7% as enargite)	Column leaching	Enargite dominant as Cu containing mineral	Lee et al 2011
	Acidianus, Metallospheara, Sulfolobus	1.8	70	06	N.D.	335	ı	1.06% as Cu (95.9% as enargite)	Column leaching	Enargite dominant as Cu containing mineral	Lee et al 2011
	Ac. brierleyi	1.5	70	62	12	76	1	88.1	50 mL (△200 mL)	$0.9 \text{ g/L Fe}^{2+}$	Sasaki et al 2011
	Ac. brierleyi	1.5	70	91	35	27	1	88.1	50 mL (△200 mL)	1.8 g/L Fe <sup>2+</sup>	Sasaki et al 2011
	Ac. brierleyi	1.5	70	91	6	27	1	88.1	50 mL (△200 mL)	2.7 g/L Fe <sup>2+</sup>	Sasaki et al 2011
	Ac. brierleyi	1.5	70	17	11	19	1	88.1	50 mL (△200 mL)	3.6 g/L Fe <sup>2+</sup>	Sasaki et al 2011
	Ac. brierleyi	1.5	70	83	N.D.	40	0.5	88.1	50 mL (△200 mL)	2.7 g/L Fe <sup>2+</sup>	Sasaki et al 2011
	Ac. brierleyi	1.5	70	91	N.D.	27	1	88.1	50 mL (△200 mL)	2.7 g/L Fe <sup>2+</sup>	Sasaki et al 2011

L	Microorganism(s)	Initial pH	Initial pH Temp. (°C) $Cu$ leached As leached (%) (%)	Cu leached (%)	As leached (%)	Leaching periods (days)	Pulp density (%)	Enargite grade (%)	Volume	Conditions	Ref.
	Ac. brierleyi	1.5	70	81	N.D.	40	2	88.1	50 mL (∆200 mL)	2.7 g/L Fe <sup>2+</sup>	Sasaki et al 2011
	Ac. brierleyi	1.5	70	91	6	27	1	88.1	50 mL (∆200 mL)	2.7 g/L Fe <sup>2+</sup>	Takatsugi et al 2011
	Ms. hakonensis	2.0	75	15	N.D.	27	1	09	50 mL (∆200 mL)	Pure culture	Ai et al 2017
- 15 -	Ms. sedula	2.0	75	09	N.D.	27	1	09	50 mL (∆200 mL)	Pure culture (ARS50-2)	Ai et al 2017
	Ms. sedula	2.0	75	62	N.D.	27	1	09	50 mL (∆200 mL)	Pure culture (cop A mutant)	Ai et al 2017
	Ms. sedula Ms. hakonensis	2.0	75	62	N.D.	27	1	09	50 mL (∆200 mL)	Mixed culture (copA mutant)	Ai et al 2017
	Ms. sedula Ms. hakonensis	2.0	75	35	N.D.	27	3	60	50 mL (∆200 mL)	Mixed culture (copA mutant)	Ai et al 2017
	Ms. sedula Ms. hakonensis	2.0	75	67	N.D.	27	1	60	50 mL (∆200 mL)	Mixed culture ( <i>cop</i> A mutant and ARS50-2)	Ai et al 2017
	Ms. sedula Ms. hakonensis	2.0	75	62	N.D.	27	б	60	50 mL (∆200 mL)	Mixed culture ( <i>cop</i> A mutant and ARS50-2)	Ai et al 2017

## **1.2.3.2** Bioleaching of enargite using mesophiles and/or moderate thermophiles

Although high-temperature conditions enable the bioleaching of enargite to simultaneously achieve high copper recovery and low arsenic solubilization, the application of this process into real operation is unrealistic form economical point of view. Therefore, bioleaching of enargite at low-temperature conditions have also been conducted by several researchers.

Escobar et al. (1997) carried out chemical and biological leaching of enargite at 30°C by using iron-and sulfur-oxidizing bacteria, *At. ferrooxidans*. Even though bioleaching achieved higher copper recovery than acid leaching as chemical leaching, its recovery was only 11% even after 32 days of the experimental period.

Bioleaching of enargite samples associated with arsenopyrite (FeAsS) (Corkhill et al., 2008) and pyrite (FeS<sub>2</sub>) (Canales et al., 2002) have also been conducted at  $30^{\circ}$ C. In both cases, not enargite but concomitant minerals were selectively attacked by microorganisms, confirming the refractoriness of enargite.

Sasaki et al. (2010) also conducted bioleaching of enargite under low temperature condition ( $25^{\circ}$ C) by using *At. ferrooxidans*. This study found that the formation of amorphous ferric arsenate but not scorodite, revealing that the arsenic precipitation formed during bioleaching at lower temperature is less crystallized and lack of stability as arsenic-bearing waste.

In each case, copper extraction was significantly lower than that under hightemperature conditions. Moreover, arsenic precipitates need to be further stabilized compared with that under high-temperature conditions. These results suggest the necessity of the reaction-accelerator such as a catalyst to achieve high copper extraction from enargite and form highly stable arsenic precipitation even at low temperature conditions.

The study of enargite bioleaching using mesophiles and/or moderate thermophiles under different conditions, such as microbiological system, initial pH, temperature, and pulp density were summarized below. Table 1.2 The list of previous studies in enargite bioleaching using mesophiles/moderate thermophiles.

Ref.	Escobar et al 1997	Escobar et al 1997	Acevedo et al 1998	Acevedo et al 1998	Acevedo et al 1998	Acevedo et al 1998	Acevedo et al 1998
Conditions	wihtout Fe <sup>3+</sup>	3.0 g/L Fe <sup>3+</sup>	air supply	1% CO <sub>2</sub>	2% CO <sub>2</sub>	3% CO <sub>2</sub>	4% CO <sub>2</sub>
Volume	100 mL (△250 mL)	100 mL (∆250 mL)	1.3 L (2 L fermenter)	1.3 L (2 L fermenter)	1.3 L (2 L fermenter)	1.3 L (2 L fermenter)	1.3 L (2 L fermenter)
Enargite grade (%)	46% as Cu	46% as Cu	41	41	41	41	41
Pulp density (%)	5	5	4	4	4	4	4
Leaching periods (days)	32	32	24	24	24	24	24
As leached (%)	6	8	19	19	24	25	21
Cu leached (%)	6	11	16	19	19	19	18
Temp. (°C)	30	30	35	35	35	35	35
Initial pH	1.6	1.6	2.4	2.4	2.4	2.4	2.4
Microorganism(s)	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans
	$ \begin{tabular}{ l l l l l l l l l l l l l l l l l l l$	Initial pHTemp. (°C)Cu leachedLeachingPulpEnargite gradeConditions1.6309632546% as Cu $100 \text{ mL}$ wintout Fe <sup>3+</sup>	Initial pHTemp. (°C)Cu leached (%)Leaching (%)Pulp (%)Enargie grade (%)VolumeConditions1.6309632546% as Cu $100 \text{ mL}$ wintout Fe <sup>3+</sup> 1.63011832546% as Cu $(\triangle 250 \text{ mL})$ wintout Fe <sup>3+</sup>	Initial pHTemp. (C)Cu leachedLeachingPulpPulpEnargie gradeVolumeConditions1.6 $30$ 96 $32$ 5 $46\%$ as Cu $100 \text{ mL}$ wintout Fe <sup>3+</sup> 1.6 $30$ 18 $32$ 5 $46\%$ as Cu $(\Delta 250 \text{ mL})$ wintout Fe <sup>3+</sup> 2.4 $30$ 118 $32$ 5 $46\%$ as Cu $(\Delta 250 \text{ mL})$ $3.0 \text{ g/L Fe^{3+}}$ 2.4 $35$ 1619244 $41$ $(1.3 \text{ L})$ $3.0 \text{ g/L Fe^{3+}}$	Initial pHTemp. (vC)Cu leached (%)Leaching (%)Pulp (%)Enargie grade (%)VolumeConditions1.6309632546% as Cu100 mLwittout $Fe^{3+}$ 1.63011832546% as Cu $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.43311832546% as Cu $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$ 2.435161924441 $(\triangle 250 \text{ mL})$ $3.0 \text{ g/L} Fe^{3+}$	Initial pHTemp. (c)U leacted (w)Leacting priods (dons)Pulp (w)Emargie grade (most)Volume (most)Conditions1.6309632546% as Cu100 mLwintout Fe <sup>3+</sup> 1.63011832546% as Cu100 mLwintout Fe <sup>3+</sup> 2.43311832546% as Cu100 mLan supply2.435161924441 $(\Delta 250 \text{ mL})$ 3.0 g/L Fe <sup>3+</sup> 2.435161924441 $(\Delta 250 \text{ mL})$ an supply2.435161924441 $(\Delta 250 \text{ mL})$ $(\Delta 200 \text{ mL})$ 2.4351924441 $(\Delta 1.50 \text{ mL})$ $(\Delta 0.2, \Delta 0.5)$ 2.435192424441 $(\Delta 2.50 \text{ mL})$ $(\Delta 0.2, \Delta 0.5)$ 2.435192424441 $(\Delta 2.50 \text{ mL})$ $(\Delta 0.2, \Delta 0.2)$ 2.435192424441 $(\Delta 2.50 \text{ mL})$ $(\Delta 0.2, \Delta 0.2)$ 2.435192424441 $(\Delta 2.50 \text{ mL})$ $(\Delta 0.2, \Delta 0.2)$ 2.43519242444 $(\Delta 0.2, \Delta 0.2)$ $(\Delta 0.2, \Delta 0.2)$ 2.43519242444 $(\Delta 0.2, \Delta 0.2)$ $(\Delta 0.2, \Delta 0.2)$ 2.43519242444 $(\Delta 0.2, \Delta 0.2)$ $(\Delta 0.2, \Delta 0.2)$	Initial PHTemp. (C)Cu leached (%)As leached (%)PulpEnurgic grade (%)VolumeConditions1.6309632546% as Cu100 mLwithout Fe <sup>3+</sup> 1.63011832546% as Cu100 mLwithout Fe <sup>3+</sup> 1.63011832546% as Cu100 mL3.0 g/L Fe <sup>3+</sup> 2.435161924441 $(\Delta 250 mL)$ $3.0 g/L Fe^{3+}$ 2.435191924441 $(1.3 L)$ $3.0 g/L Fe^{3+}$ 2.435191924441 $(1.3 L)$ $1.9 CO_2$ 2.435192424441 $(2.L fermenter)$ $2.9 CO_2$ 2.435192524441 $(2.L fermenter)$ $3.9 CO_2$ 2.435192524441 $(2.L fermenter)$ $3.9 CO_2$

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Initial pHTemp. (°C)Cu leachedAs leachedLeachingPulp1.833N.D. $(\%)$ $(\%)$ $(\%)$ $(\%)$ 1.833N.D.2.5861.833N.D. $2.5$ 861.833N.D. $<0.1$ 818
N.D. <0.1 8
1 g/L as 8 34 Cu
8 9 32
6 5 65
7 7 157

Microorganism(s)	Initial pH	Initial pH Temp. (°C) Cu leached As leached (%) (%)	Cu leached (%)	As leached (%)	Leaching periods (days)	Pulp density (%)	Enargite grade (%)	Volume	Conditions	Ref.
At. ferrooxidans	2.34	22	6		44	3.3	~ 100	75 mL (∆300 mL)	Inoculated from above culture	Fantauzzi et al 2009
At. ferrooxidans	7	25	L	٢	130	0.7	88.1	150 mL (△500 mL)	Arsenic adapted bacterial culture	Sasaki et al 2010
At. ferrooxidans	7	25	9	٢	130	0.7	88.1	150 mL (△500 mL)	Non-adapted bacterial culture	Sasaki et al 2010
Acidithiobacillus, Leptospirillum	1.8	20-22	06	N.D.	301	I	2.45% as Cu (4.2% as enargite)	Column leaching	Chalcocite dominant as Cu containing mineral	Lee et al 2011
Acidithiobacillus, Leptospirillum	1.8	20-22	98	N.D.	653	ı	5.62% as Cu (2.9% as enargite)	Column leaching	Chalcocite dominant as Cu containing mineral	Lee et al 2011
Acidithiobacillus, Leptospirillum	1.8	20-22	< 20	N.D.	241	I	0.63% as Cu (12.8% as enargite)	Column leaching	Covellite dominant as Cu containing mineral	Lee et al 2011
Acidithiobacillus, Leptospirillum	1.8	20-22	< 20	N.D.	637	I	0.59% as Cu (20% as enargite)	Column leaching	Covellite dominant as Cu containing mineral	Lee et al 2011

	Initial pH	Temp. (°C)	Cu leached (%)	As leached (%)	Leaching periods (days)	Pulp density (%)	Enargite grade (%)	Volume	Conditions	Ref.
Acidithiobacillus, Leptospirillum	1.8	20-22	< 20	N.D.	234	ı	0.73% as Cu (94.7% as enargite)	Column leaching	Enargite dominant as Cu containing mineral	Lee et al 2011
Acidithiobacillus, Leptospirillum	1.8	20-22	< 20	N.D.	234	I	1.06% as Cu (95.9% as enargite)	Column leaching	Enargite dominant as Cu containing mineral	Lee et al 2011

#### 1.3 Catalyst for bioleaching of sulfide minerals

Previous researches on bioleaching of enargite have suggested the necessity of some catalyst to enhance copper solubilization even under low temperature conditions. However, the number of studies using some catalysts on enargite leaching is limited. In order to obtain the valuable information of the possible catalyst that is useful for improvement of enargite bioleaching, studies investigating the effects of various catalysts on leaching of sulfide mineral, especially for chalcopyrite, are introduced.

#### 1.3.1 Catalytic effect of metals

#### 1.3.1.1 Catalytic effect of metals on chalcopyrite dissolution

A number of studies have investigated the effect of co-existing metal ions on the improvement of chalcopyrite dissolution. Muñoz et al. (2007) conducted chalcopyrite bioleaching in the presence of antimony (Sb), cobalt (Co), silver (Ag), bismuth (Bi), nickel (Ni), tin (Sn) and manganese (Mn). The results showed that only silver greatly enhanced chalcopyrite dissolution, but no other co-existing metals showed positive effects on it. Hiroyoshi et al. (2007) confirmed the positive effect of silver on accelerating copper extraction from chalcopyrite. In this study, bismuth was also found effective in enhancing chalcopyrite dissolution, which was not observed in the study conducted by Muñoz et al. (2007), since bismuth is likely to show inhibitory effect on microbial activity; bismuth is likely only useful in abiotic chemical leaching of chalcopyrite. Ballester et al. (1990) also tested various metal ions, Co, Bi, Ag, and mercury (Hg) in chalcopyrite bioleaching, observing the effectiveness of Hg as a catalytic metal as well as silver. However, considering its toxicity, it is inapplicable to real operation, suggesting that the silver is the only possible candidate for strongly enhancing the dissolution of refractory chalcopyrite.

#### 1.3.1.2 Catalytic effect of silver on chalcopyrite dissolution

In order to investigate the reason of strong catalytic capability of Ag, underlying mechanism have been discussed in decades and several possibilities have been proposed: (i) improvement of electrical conductivity by the formation of silver sulfide inside elemental sulfur layer on chalcopyrite surface, (ii) silver atom diffusion into metal-deficient sulfur-rich layer formed on chalcopyrite surface and (iii) silver sulfide

formation which consumes hydrogen sulfide produced via chalcopyrite reduction, indirectly accelerating chalcopyrite dissolution .

The first theory, proposed by Nazari et al. (2011, 2012a, 2012b, 2012c), is based on the electron transfer catalyzed by silver-doped pyrite. In the presence of pyrite contacted with chalcopyrite, electron transfer between chalcopyrite and pyrite enable the corrosion of the chalcopyrite surface, resulting in the faster dissolution behavior of chalcopyrite. However, the formation of elemental sulfur via the dissolution of chalcopyrite inhibits the contact between the surface of chalcopyrite and pyrite, resulting in a weak galvanic effect. Instead of pure pyrite, silver-coated pyrite was employed to further enhance electron transfer between chalcopyrite can be transformed into Ag<sub>2</sub>S, consequently retaining the electrochemical contact between chalcopyrite and pyrite and pyrite and pyrite with the intermediate of Ag<sub>2</sub>S. As a result, chalcopyrite dissolution was dramatically accelerated, indicating that electron transfer between chalcopyrite grains and external regions (i.e. leaching solution, pyrite, and other materials) is assumed a key factor during silver-added leaching of chalcopyrite.

The second theory, proposed by Ghahremaninezhad et al. (2010, 2013, 2015), is based on the formation of metal-deficient sulfide film ( $Cu_{1-x}Fe_{1-y}S_{2-z}$ ), which is considered as one of the passivation layers formed during chalcopyrite leaching. The existence of this layer possibly hinders the interaction between chalcopyrite and leaching solution, and diffusion of metal ions (i.e. Fe, Cu) passing through this layer rate-limits the dissolution of chalcopyrite. In the presence of silver, silver atom diffuses into the metal-deficient sulfide layer, resulting in the formation of silver sulfide ( $Ag_2S$ ). As a result, electrical interaction between chalcopyrite and leaching solution is maintained with the intermediate of  $Ag_2S$ . In addition, oxidation of the silver sulfide is capable of releasing the silver atom into the solution and leaving behind porous elemental sulfur, which enables direct interaction between chalcopyrite and leaching solution. The most important point in this theory is diffusion of the silver atom into metal-deficient sulfide film, and reform of its structure.

The third theory, proposed by Hiroyoshi et al. (2000, 2001, 2002, 2004, 2008a, 2008b), is based on the redox potential of the leaching solution. In this theory, chalcopyrite dissolution is considered to be greatly enhanced within the certain range of redox

potential, which is determined by critical potential,  $E_c$ , and oxidation potential,  $E_{ox}$ : critical potential is the redox potential where reduction of chalcopyrite to more soluble copper sulfide (Cu<sub>x</sub>S) occur, and oxidation potential is the redox potential where oxidation of Cu<sub>x</sub>S to Cu<sup>2+</sup> occur. In the presence of the silver, hydrogen sulfide (H<sub>2</sub>S), produced via the reduction of chalcopyrite, is immediately consumed for the formation of silver sulfide by precipitating with silver ion in the leaching solution. As a result, chemical equilibrium is shifted toward the reaction for further chalcopyrite reduction. Consequently, chalcopyrite reduction to Cu<sub>x</sub>S, followed by its oxidation to Cu<sup>2+</sup>, is easily happened compared to the case in the absence of silver. The role of silver in this theory is the indirect contribution that consumption of hydrogen sulfide due to its high affinity with silver ion to form silver sulfide.

## 1.3.1.3 Catalytic effect of silver in chalcopyrite bioleaching

The catalytic advantage of Ag has also been actively tested not only in the abiotic acid leaching but also in bioleaching, even though its toxicity on the microbial activity is widely recognized. Various experimental conditions employed to evaluate the catalytic ability of Ag are listed in Table 1.3. Mesophiles such as *At. ferrooxidnas, At. thiooxidans, Lp. ferrooxidans* have been frequently used for those tests under relatively low temperature conditions. Even such harsh conditions for faster dissolution of chalcopyrite, higher Cu recovery (> 90%) has been indeed achieved in some cases (Yuehua et al., 2002; Muñoz et al., 2007; Abdollahi et al., 2015). These results indicate that silver is a promising catalyst for enhancing the dissolution of refractory copper sulfide even in the ioleaching process.

	Ref.	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990	Ahonen et al. 1990
ioleaching.	Conditions					Silver added after 5 days of leaching	Silver added after 5 days of leaching			
list of previous studies in silver-catalyzed chalcopyrite bioleaching.	Volume	100  mL ( riangle 250)	100 mL (∆250)	100 mL (△250)	100 mL (△250)	100 mL (△250)	100 mL (△250)	100 mL (△250)	100 mL (△250)	100 mL (∆250)
/er-catalyz	Chalcopyrite grade (%)	6	9	6	13	13	13	56	95	95
s in silv	Pulp density (%)	1.5	1.5	1.5	5	5	5	2	2	2
us studie	Leaching periods (days)	49	49	49	40	40	40	49	49	49
st of previo	Ag addition	ı	9.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	31.6 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	8.9 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	8.9 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	29.6 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	3 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	3 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	30 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>
.3 The li	Cu leached (%)	37	39	66	5	11	35	5	10	42
Table 1.3 The	Initial pH Temp. (°C) Cu leached (%)	28	28	28	28	28	28	28	28	28
	Initial pH	2	2	2	2	2	2	2	5	2
	Microorganism(s)	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli	Acidithiobacilli

Initial pH	Initial pH Temp. (°C) Cu leached	Cu leached (%)	Ag addition	Leaching periods (days)	Pulp density (%)	Chalcopyrite grade (%)	Volume	Conditions	Ref.
	35	06	30  mg Ag/L as $\text{Ag}_2\text{SO}_4$	16	S	7	300 mL (500 mL glass reactor)	Air and 1% $CO_2(v/v)$ supply	Ballester et al. 1990
	45	32	0.5  mg Ag/L as $Ag_2SO_4$	27	5	19% as Cu	100 mL (△250)		Gómez et al. 1999
	45	59	1.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	72	5	19% as Cu	100  mL ( riangle 250)		Gómez et al. 1999
	45	53	2.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	27	5	19% as Cu	100 mL (△250)		Gómez et al. 1999
	50	27	1.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	26	5	19% as Cu	100 mL (△250)		Gómez et al. 1999
	50	39	0.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	27	5	19% as Cu	$\begin{array}{c} 100 \text{ mL} \\ (\bigtriangleup 250) \end{array}$		Gómez et al. 1999
	50	99	1.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	27	5	19% as Cu	100 mL (△250)		Gómez et al. 1999
	50	72	2.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	27	5	19% as Cu	100 mL (△250)		Gómez et al. 1999
1.8	50	47	2.5 mg Ag/L as Ag <sub>2</sub> SO <sub>4</sub>	26	S	19% as Cu	100 mL (△250)		Gómez et al. 1999

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Microorganism(s)	Initial pH	Initial pH Temp. (°C) Cu leached (%)	Cu leached (%)	Ag addition	Leaching periods (days)	Pulp density (%)	Chakopyrite grade (%)	Volume	Conditions	Ref.
At. ferrooxidans	1.3	25	58	135 mg/L as AgCl	20	2	20% as Cu	200 mL (∆250)		Sato et al. 2000
At. ferrooxidans	1.3	25	62	665 mg/L as AgCl	20	2	20% as Cu	200 mL (∆250)		Sato et al. 2000
At. ferrooxidans	1.3	25	65	1330 mg/L as AgCl	20	2	20% as Cu	200 mL (∆250)		Sato et al. 2000
At. ferrooxidans	1.3	25	65	1330 mg/L as AgCl	20	2	20% as Cu	200 mL (∆250)	with contact between chaleopyrite and silver chloride	Sato et al. 2000
At. ferrooxidans	1.3	25	18	1330 mg/L as AgCl	20	2	20% as Cu	200 mL (∆250)	without contact between chalcopyrite and silver chloride	Sato et al. 2000
At. ferrooxidans, At. thiooxidans, Lp. ferrooxidans	2	30	73	100 mg/L as Ag <sub>2</sub> S	28	5	≈100%	100 mL (∆250)		Yuehua et al. 2002
At. ferrooxidans, At. thiooxidans, Lp. ferrooxidans	2	30	76	200 mg/L as Ag <sub>2</sub> S	28	5	≈100%	100 mL (△250)		Yuehua et al. 2002
At. ferrooxidans, At. thiooxidans, Lp. ferrooxidans	2	30	39	10 mg/L as Ag <sub>2</sub> S	20	5	0.33% as Cu	100 mL (△250)		Yuehua et al. 2002
At. ferrooxidans, At. thiooxidans, Lp. ferrooxidans	2	30	85	50 mg/L as Ag <sub>2</sub> S	20	S	0.33% as Cu	100 mL (∆250)		Yuehua et al. 2002

i									
Ref.	Yuehua et al. 2002	Muñoz et al. 2007							
Conditions									
Volume	100 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)
Chalcopyrite grade (%)	0.33% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu	0.68% as Cu
Pulp density (%)	5	10	2.5	5	7.5	10	15	10	10
Leaching periods (days)	20	15	44	44	44	44	44	27	27
Ag addition	100 mg/L as Ag <sub>2</sub> S	9 mg/L as Ag	46 mg/L as Ag	91 mg/L as Ag	137 mg/L as Ag	182 mg/L as Ag	274 mg/L as Ag	9 mg/L as Ag	23 mg/L as Ag
Cu leached (%)	16	94	26	92	86	84	72	16	26
Initial pH Temp. (°C) Cu leached	30	35	35	35	35	35	35	35	35
Initial pH	2	2	2	2	2	2	2	2	2
Microorganism(s)	At. ferrooxidans, At. thiooxidans, Lp.ferrooxidans	Acidithiobacilli, Leptospirilli							

tions Ref.	Muñoz et al. 2007	Muñoz et al.							
e Conditions									
Volume	80 mL (∆250)	80 mL							
Chalcopyrite grade (%)	0.68% as Cu								
Pulp density (%)	10	10	10	10	10	10	10	10	10
Leaching periods (days)	27	27	27	14	14	14	14	14	14
Ag addition	36 mg/L as Ag	91 mg/L as Ag	137 mg/L as Ag	9 mg/L as Ag	9 mg/L as Ag	9 mg/L as Ag	9 mg/L as Ag	9 mg/L as Ag	9 mg/L
Cu leached (%)	<i>L</i> 6	26	68	98	16	26	68	82	26
Initial pH Temp. (°C)	35	35	35	35	35	35	35	35	35
Initial pH	2	2	2	1.2	1.5	1.8	2	2.5	3
Microorganism(s)	Acidithiobacilli, Leptospirilli								

Ref.	Muñoz et al. 2007	Muñoz et al. 2007	Muñoz et al. 2007						
Conditions	Deionized water	1/10 0K medium	0K medium	Cl-free 0K medium	without Fe <sup>3+</sup>	with 0.1 g/L Fe <sup>3+</sup>	with 0.25 g/L $\mathrm{Fe}^{3+}$	with 0.5 g/L Fe <sup>3+</sup>	with 1 g/L $\mathrm{Fe}^{3+}$
Volume	80 mL (△250)	80 mL (∆250)	80 mL (△250)	80 mL (∆250)	80 mL (∆250)	80 mL (∆250)	80 mL (△250)	80 mL (∆250)	80 mL (∆250)
Chalcopyrite grade (%)	0.68% as Cu	0.68% as Cu	0.68% as Cu						
Pulp density (%)	10	10	10	10	10	10	10	10	10
Leaching periods (days)	14	14	14	14	14	14	14	14	14
Ag addition	9 mg/L as Ag	9 mg/L as Ag	9 mg/L as Ag						
Cu leached (%)	67	94	93	88	94	95	96	96	85
Temp. (°C) Cu leached (%)	35	35	35	35	35	35	35	35	35
Initial pH	5	2	2	2	2	2	2	2	2
Microorganism(s)	Acidithiobacilli, Leptospirilli	Acidithiobacilli, Leptospirilli	Acidithiobacilli, Leptospirilli						

Microorganism(s)	Initial pH	Temp. (°C)	Initial pH Temp. (°C) Cu leached (%)	Agaddition	Leaching periods (days)	Pulp density (%)	Chalcopyrite grade (%)	Volume	Conditions	Ref.
Acidithiobacilli, Leptospirilli	2	35	81	9 mg/L as Ag	14	10	0.68% as Cu	80 mL (△250)	with 3 gL $\mathrm{Fe}^{3+}$	Muñoz et al. 2007
Acidithiobacilli, Leptospirilli	2	35	56	9 mg/L as Ag	14	10	0.68% as Cu	80 mL (∆250)	with 5 g/L Fe <sup>3+</sup>	Muñoz et al. 2007
<ul> <li>At. ferrooxidans,</li> <li>Acidithiobicillus- like isolate,</li> <li>Lp. ferrooxidans,</li> <li>β-proteobaccterium isolate,</li> <li>Firmicute isolate,</li> <li>Sulfobacillus isolate,</li> <li>Thiomonus sp.,</li> <li>At. thiooxidans,</li> <li>Acidobacterium sp.,</li> </ul>	7	30	33	< 0.02 mg/L as Ag	30	0	20	100 mL (∆250)		Johnson et al. 2008
At. ferrooxidans, At. ferrooxidans, Lp. ferrooxidans, $\beta$ -proteobacterium isolate, Firmicute isolate, Sulfobacillus isolate, Thiomonas sp., At thiooxidans, Acidiphilum sp., Acidobacterium sp.	6	30	27	0.52 mgL as Ag	30	7	70	100 mL (∆250)		Johnson et al. 2008

		xt al.	x al.				
	Ref.	Johnson et al. 2008	Johnson et al. 2008				
	Conditions						
	Volume	100 mL (∆250)	100 mL (∆250)				
Chalcopyrite	grade (%)	~ 66	45-50				
Pulp	density (%)	0	6				
Leaching	periods (days)	30	30				
	Ag addition	l6 mg/L as Ag	30 mg/L as Ag				
Cu laarhad	(%)	87	∞ ∞				
	Initial pH Temp. (°C) Cu Earled (%)	30	33				
	Initial pH	0	0				
	Microorganism(s)	<ul> <li>At. ferrooxidans,</li> <li>Acidithiobicillus- like isolate,</li> <li>Lp. ferrooxidans,</li> <li>β-proteobacterium isolate,</li> <li>Firmicute isolate,</li> <li>Sulfobacillus isolate,</li> <li>At. thiooxidans,</li> <li>At. thiooxidans,</li> <li>Acidiphilum sp.,</li> <li>Acidobacterium sp.</li> </ul>	<ul> <li>At. ferrooxidans,</li> <li>Acidithiobicillus-like isolate,</li> <li>Lp. ferrooxidans,</li> <li>β-proteobacterium isolate,</li> <li>Fim acidiphilum,</li> <li>Firmicute isolate,</li> <li>Sulfobacillus isolate,</li> <li>At thiooxidans,</li> <li>Acidiohans,</li> <li>Acidobacterium sp.</li> </ul>				

Ref.	Johnson et al. 2008								
Conditions									
Volume	100 mL (△250)								
Chalcopyrite grade (%)	20								
Pulp density (%)	71								
Leaching periods (days)	30								
Ag addition	< 0.02 mg/L as Ag								
Cu leached (%)	2								
Initial pH Temp. (°C) Cu leached (%)	31								
Initial pH	2								
Microorganism(s)	<ul> <li>At. ferrooxidans,</li> <li>At. ferrooxidans,</li> <li>Lp. ferrooxidans,</li> <li>P-proteobacterium isolate,</li> <li>Fm. acidiphilum,</li> <li>Firmicute isolate,</li> <li>Sulfobacillus isolate,</li> <li>Sulfobacillus isolate,</li> <li>Sulfobacillus isolate,</li> <li>At. thiooxidans,</li> <li>Acidobacterium sp.,</li> <li>Acidobacterium sp.,</li> <li>Acidobacterium sp.,</li> <li>Acidobacterium sp.,</li> <li>Fx. thermotolerans,</li> <li>Sb. benefaciens,</li> <li>Firmicute isolate,</li> <li>At. caldus,</li> <li>Acidicallus organivorans,</li> <li>Acidicallus organivorans,</li> </ul>								

Ref.	Johnson et al. 2008
Conditions	
Volume	100 mL (∆250)
Chalcopyrite grade (%)	02
Pulp density (%)	71
Leaching periods (days)	30
Ag addition	0.52 mg/L as Ag
Initial pH Temp. (°C) Cu leached (%)	47
Temp. (°C)	37
Initial pH	0
Microorganism(s)	<ul> <li>At. ferrooxidans, Acidithiobicillus-like isolate, Lp. ferrooxidans, Firmicute isolate, Firmicute isolate, Sulfobacillus isolate, Thiomonas sp., At. thiooxidans, Acidobacterium sp., Acidobacterium sp., Lp. ferriphilum, Am. ferrooxidans, Ferroplasma sp., Fx. thermotolerans, Sb. thermosulfidooxidans, Sb. thermosulfidooxidans, Sb. thermosulfidooxidans, Sb. thermotolerans, Sb. thermosulfidooxidans, Firmicute isolate, At. caldus, Acidicaldus organivorans, Alicyclobacillus isolate</li> </ul>

Ref.	Johnson et al. 2008							
Conditions								
Volume	100 mL (∆250)							
Chalcopyrite grade (%)	× Se							
Pulp density (%)	71							
Leaching periods (days)	30							
Ag addition	16 mg/L as Ag							
Initial pH Temp. (°C) Cu leached (%)	82							
Temp. (°C)	37							
Initial pH	0							
Microorganism(s)	<ul> <li>At. ferrooxidans, Acidithiobicillus-like isolate, Lp. f errooxidans, Fm. acidiphilum, Firmicute isolate, Sulfobacillus isolate, Thiomonas sp., At. thiooxidans, Acidobacterium sp., Acidobacterium sp., Lp. ferriphilum, Am. ferrooxidans, Ferroplasma sp., Fx. thermosulfidooxidans, Sb. thermosulfidooxidans, Sb. thermosulfidooxidans, Sb. thermosulfidooxidans, Firmicute isolate, At. caldus, At. caldus, At. caldus, solate</li> </ul>							

Ref.	Johnson et al. 2008	Johnson et al. 2008			
Conditions					
Volume	100 mL (∆250)	100 mL (△250)			
Chalcopyrite grade (%)	45-50	20			
Pulp density (%)	2	а			
Leaching periods (days)	8	30			
Ag addition	30 mg/L as Ag	< 0.02 mg/L as Ag			
Cu leached (%)	ß	8			
Initial pH Temp. (°C)	37	37			
Initial pH	0	0			
Microorganism(s)	<ul> <li>At. ferrooxidans,</li> <li>Acidithiobicillus- like isolate,</li> <li>Lp. ferrooxidans,</li> <li>B-proteobacterium isolate,</li> <li>Fm. acidiphilum,</li> <li>Firmicute isolate,</li> <li>Sulfobacillus isolate,</li> <li>Thiomonas sp.,</li> <li>At. thiooxidans,</li> <li>Acidobacterium sp,</li> <li>Acidobacterium sp,</li> <li>Lp. ferriphilum,</li> <li>Am. ferrooxidans,</li> <li>Ferroplasma sp,</li> <li>Firmicute isolate,</li> <li>Sb. hermosulfidooxidans,</li> <li>Sb. thermotolerans,</li> <li>Sb. thermotolerans,</li> <li>Sb. thermotolerans,</li> <li>Sb. thermosulfidooxidans,</li> <li>Firmicute isolate,</li> <li>At. caldus,</li> <li>Aciditations organivorans,</li> <li>Alicyclobacillus isolate</li> </ul>	Lp. ferriphilum, Am. ferrooxidans, Ferroplasma sp., Fx. thermotolerans, Sb. thermosulfidooxidans, Sb. thermosulfidooxidans, Sb. benefaciens, Firmicute isolate, At. caldus, Acidicaldus organivorans, Alicyclobacillus isolate			

Microorganism(s)	Initial pH	Temp. (°C)	Temp. (°C) Cu leached	Ag addition	Leaching periods (days)	Pulp density (%)	Chalcopyrite grade (%)	V olume	Conditions	Ref.
Lp. ferriphilum, Am. ferropasma sp., Ferroplasma sp., Fx. thermotolerans, Sb. thermosulfidooxidans, Sb. benefaciens, Sb. benefaciens, Firmicute isolate, At. caldus, At. caldus, Alicyclobacillus isolate	2	37	20	0.52 mg/L as Ag	30	0	70	100 mL (∆250)		Johnson et al. 2008
Lp. ferriphilum, Am. ferrooxidans, Am. ferroplasma sp., Ferroplasma sp., Sb. thermotolerans, Sb. acidophilus, Sb. benefaciens, Firmicute isolate, At. caldus, At. caldus, Alicyclobacillus isolate	7	37	76	16 mg/L as Ag	30	0	< 60	100 mL (∆250)		Johnson et al. 2008
Lp. ferriphilum, Am. ferrooxidans, Am. ferroplasma sp., Fx. thermotolerans, Sb. thermosulfdooxidans, Sb. benefaciens, Sb. benefaciens, Firmicute isolate, At. caldus, Acidicaldus organivorans, Alicyclobacillus isolate	7	37	31	30 mg/L as Ag	30	0	45-50	100 mL (∆250)		Johnson et al. 2008

Ref.	Feng et al. 2013	Feng et al. 2013	Feng et al. 2013	Feng et al. 2013	Abdollahi et al. 2015				
Conditions					10 g/L ${\rm Fe}^{2+}$ and 10 g/L ${\rm S}^0$	10 g/L ${\rm Fe}^{2\pm}$ and 10 g/L ${\rm S}^0$	10 g/L ${\rm Fe}^{2+}$ and 10 g/L ${\rm S}^0$	10 g/L ${\rm Fe}^{2\pm}$ and 10 g/L ${\rm S}^0$	10 g/L ${\rm Fe}^{2+}$ and 10 g/L ${\rm S}^0$
Volume	100 mL (∆500)	100 mL (∆500)	100 mL (∆500)	100 mL (∆500)	N.D.	N.D.	N.D.	N.D.	N.D.
Chalcopyrite grade (%)	ю	3	З	ŝ	2.1	2.1	2.1	2.1	2.1
Pulp density (%)	1	1	1	1	3	3	3	3	3
Leaching periods (days)	20	20	20	20	30	30	30	30	30
Ag addition	0.5 mg/L as Ag	2 mg/L as Ag	10 mg/L as Ag	50 mg/L as Ag	30 mg/L as Ag	60 mg/L as Ag	120 mg/L as Ag	200 mg/L as Ag	400 mg/L as Ag
Cu leached (%)	38	50	48	52	84	83	96	96	66
Initial pH Temp. (°C) Cu leached (%)	30	30	30	30	32	32	32	32	32
Initial pH	5	2	2	2	1.6	1.6	1.6	1.6	1.6
Microorganism(s)	At. ferrooxidans Acidithiobacillus sp.	At. ferrooxidans Acidithiobacillus sp.	At. ferrooxidans Acidithiobacillus sp.	At. ferrooxidans Acidithiobacillus sp.	At. ferrooxidans, At. thiooxidnas, Lp. ferrooxidans				

Ref.	Abdollahi et al. 2015	Xia et al. 2018	Xia et al. 2018	Xia et al. 2018	Xia et al. 2018	
Conditions	10 g/L Fe <sup>2+</sup> and 10 g/L S <sup>0</sup>					
Volume	N.D.	200 mL (△500)	200 mL (△500)	200 mL (△500)	200 mL (△500)	
Chalcopyrite grade (%)	2.1	≈100%	≈100%	≈100%	≈100%	
Pulp density (%)	3	1	1	1	1	
Leaching periods (days)	30	8	8	8	8	
Ag addition	Ag addition 1000 mg/L as Ag		5 mg/L as Ag	10 mg/L as Ag	20 mg/L as Ag	
Initial pH Temp. (°C) Cu leached (%)	55	68	68	68	64	
Temp. (°C)	32	32	32	32	32	
Initial pH	1.6	1.7	1.7	1.7	1.7	
Microorganism(s)	At. ferrooxidans, At. thiooxidnas, Lp. ferrooxidans					

#### 1.3.1.4 Catalytic effect of silver on enargite dissolution

As mentioned above, a number of researchers have engaged in the study on chalcopyrite leaching with catalyst, especially for silver-catalyzed chalcopyrite bioleaching. However, in the case of enargite, the number of studies investigating the effect of silver on enargite leaching is limited. Miki et al. (2016) performed the enargite leaching with the addition of silver as a catalyst, achieving higher copper extraction rate (75% of recovery within one day). The study assumed that the reactions proposed by Hiroyoshi also occurred during enargite leaching, however, the detailed mechanism of silver catalytic effect on enargite dissolution is still unclear.

#### 1.3.1.5 The issues of Ag-application into the mining operation

As was mention in past decades, the utilization of Ag in real operation is economically infeasible. Nazari et al. (2011) proposed the application of Ag-doped pyrite to minimize the Ag-loss in the process by attaching the silver ion on the surface of pyrite, while its loss was inevitable (around 10% of silver was not recycled). This fact suggests the necessity of alternative catalyst, which is cheap and certainly disposable. Based on the previous study using silver as a catalyst, the required property for alternative instead of silver is as bellows: (i) high electrical conductivity, (ii) high affinity for sulfide formation, or (iii) lower ion tendency than copper. Even though mercury is likely thought one of the possibilities, it is also not able to be used as a catalyst due to its high toxicity from the environmental point of view. New insight to find the novel catalyst is thus desperately required for further development in the exploitation of primary copper sulfides.

#### **1.3.2** Catalytic effect of carbon materials

Carbon materials have recently attracted researchers' attention due to their electrochemically catalytic effect on the dissolution of refractory copper sulfides. Originally, the utility of AC as one of the carbon materials has been reported in the chalcopyrite bioleaching experiment (Nakazawa et al., 1998; Zhang et al., 2007; Liang et al., 2010). In these studies, chalcopyrite dissolution was thought to be enhanced basically through galvanic interaction between electrically nobler AC and electrically poorer chalcopyrite. Olvera et al. (2013) tested its catalytic effect in enargite leaching by electrochemical study, suggesting its potential for the enhancement of enargite dissolution by causing galvanic effect as well as modifying semi-conductive surface property of enargite. Jahromi et al. (2016) indeed confirmed the effectiveness of AC in enargite leaching, where enargite dissolution was promoted based on (i) the oxidation of Fe<sup>2+</sup> to Fe<sup>3+</sup> (oxidant regeneration) and (ii) direct enargite oxidation by in-situ hydrogen peroxide production. These mechanisms were proposed by Ahumada et al. (2002), where the oxidation reactions occur on the surface of AC as follows;

$$2C_{red} + O_2 + 2H_2O = 2H_2O_2 + 2C_{ox}$$
 (Eq. 1-7)

$$2Fe^{2+} + H_2O_2 + 2H^+ = 2Fe^{3+} + 2H_2O$$
 (Eq. 1-8)

 $C_{red}$  and  $C_{ox}$  indicate that surface functional groups on the surface of AC. Eq. 1-7 shows the generation of hydrogen peroxide occurring on the surface of AC through the reaction of quinone or other oxidative functional groups such as carboxylic acid, anhydrides, hydroxyls, lactol groups, lactone groups, and phenol groups. This hydrogen peroxide is subsequently (i) consumed to directly oxidize enargite or (ii) used for the oxidation of Fe<sup>2+</sup> to Fe<sup>3+</sup> (Eq. 1-8), followed by enargite oxidation by produced Fe<sup>3+</sup>. Modification of functional groups on the surface of AC with sulfuric acid, hydrochloric acid, or nitric acid was tested, confirming that the oxidation ability of AC was indeed varied with different acid treatments even in the leaching process (Jahromi et al., 2019).

On the other hand, it has been reported that the presence of AC suppress Eh rise during bioleaching process, implying that AC would also catalyze the Fe(III)-reduction

(Nakazawa et al., 1998; Zhang et al., 2007; Ma et al., 2017; Hao et al., 2018). This adverse catalytic effect of AC was confirmed in the chemical experiment conducted by Vargas et al. (2009), where  $Fe^{3+}$ -reduction to  $Fe^{2+}$  was able to be catalyzed by the AC. Liang et al. (2010) observed the decrease in  $Fe^{3+}/Fe^{2+}$  ratio with the addition of AC during chalcopyrite bioleaching, ensuring that  $Fe^{3+}$  was indeed catalytically reduced to  $Fe^{2+}$  by AC even in the presence of microorganisms. Although the reduction mechanism has yet been well-described, not only  $Fe^{2+}$ -oxidation but also  $Fe^{3+}$ -reduction have to be considered as the catalytic reaction caused by AC during the bioleaching process. Bioleaching of chalcopyrite catalyzed by carbon materials are summarized in Table 1.4.

	Ref.	Nakazawa et al. 1998						
hing.	Conditions			70+100 mesh	-200+280 mesh	-400 mesh	-400 mesh	400 mesh
te bioleac	Volume	200 mL (∆250)						
Table 1.4 The list of previous studies in carbon-assisted chalcopyrite bioleaching.	Chalcopyrite grade (%)	20.39% as Cu						
-assisted	Pulp density (%)	2	2	2	2	2	2	2
n carbon-	Leaching periods (days)	19	19	38	35	35	35	35
studies i	Carbon addition	0.5 g/L	2.5 g/L	2.5 g/L	2.5 g/L	2.5 g/L	5 g/L	5 g/L
previous	Carbon type	Activated carbon						
ne list of	Cu leached (%)	33	42	44	52	55	73	56
ole 1.4 T	Initial pH Temp. (°C)	25	25	25	25	25	25	25
Ta	Initial pH	1.3	1.3	1.3	1.3	1.3	I	1.3
	Microorganism(s)	At. ferrooxidans						

wite bioleaching ted chalc -4 Table 1 4 The list of nr

Volume Conditions Ref.	200 mL (△250) –400 mesh 1998	200 mL −400 mesh 1998 1998	200 mL $-400$ mesh Nakazawa et al. ( $\triangle 250$ ) without contact 1998	200 mL $-400$ mesh Nakazawa et al. $(\triangle 250)$ with contact 1998	$\begin{array}{ c c c c } 100 \text{ mL} & < 7.4 \mu \text{m of AC} & Zhang et al. \\ \hline (\bigtriangleup 250) & 2007 \end{array}$	$\begin{array}{ c c c c } 100 \text{ mL} & <7.4 \ \mu\text{m of AC} & Zhang et al. \\ (\triangle 250) & <7.4 \ \mu\text{m of AC} & 2007 \end{array}$	
Chalcopyrite grade (%)	20.39% as Cu	20.39% as Cu	20.39% as Cu	20.39% as Cu	0.4% as Cu	0.4% as Cu	
Pulp density (%)	2	7	5	7	25	25	
Leaching periods (days)	35	35	35	35	25	25	
Carbon addition	5 g/L	5 g/L	2.5 g/L	2.5 g/L	0.5 g/L	2.0 g/L	
Carbon type	Activated carbon	Activated carbon	Activated carbon	Activated carbon	Activated carbon	Activated carbon	
Cu leached (%)	50	41	12	68	64	70	
Initial pH Temp. (°C) Cu leached (%)	25	25	25	25	30	30	
Initial pH	1.5	1.7	1.3	1.3	1.2	1.2	
Microorganism(s)	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidans	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	

Ref.	Zhang et al. 2007	Zhang et al. 2007	Zhang et al. 2007	Zhang et al. 2007	Zhang et al. 2007	Zhang et al. 2007	Liang et al. 2010
Conditions	< 7.4 µm of AC	< 7.4 µm of AC 0 day resting time	< 7.4 µm of AC 1 day resting time	< 7.4 µm of AC 2 day resting time	< 7.4 µm of AC 4 day resting time	< 7.4 µm of AC 6 day resting time	
Volume	100 mL (∆250)	100 mL (∆250)	100 mL (∆250)	100 mL (∆250)	100 mL (∆250)	100 mL (∆250)	100 mL (∆250)
Chalcopyrite grade (%)	0.4% as Cu	0.4% as Cu	0.4% as Cu	0.4% as Cu	0.4% as Cu	0.4% as Cu	≈100%
Pulp density (%)	25	25	25	25	25	25	1
Leaching periods (days)	25	25	25	25	25	25	10
Carbon addition	5.0 g/L	3.0 g/L	3.0 g/L	3.0 g/L	3.0 g/L	3.0 g/L	1.0 g/L
Carbon type	Activated carbon	Activated carbon	Activated carbon	Activated carbon	Activated carbon	Activated carbon	Activated carbon
Initial pH Temp. (°C) Cu leached (%)	60	65	84	86	72	66	06
Temp. (°C)	30	30	30	30	30	30	65
Initial pH	1.2	1.2	1.2	1.2	1.2	1.2	1.5
Microorganism(s)	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	At. ferrooxidan, At. thiooxidans	Ac. manzaensis

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Microorganism(s)	Initial pH	Temp. (°C)	Initial pH Temp. (°C) Cu leached (%)	Carbon type	Carbon addition	Leaching periods (days)	Pulp density (%)	Chalcopyrite grade (%)	Volume	Conditions	Ref.
Ac. manzaensis	1.5	65	94	Activated carbon	2.0 g/L	10	1	≈ 100%	100 mL (△250)		Liang et al. 2010
Ac. manzaensis	1.5	65	93	Activated carbon	3.0 g/L	10	1	≈100%	100 mL (△250)		Liang et al. 2010
Ac. manzaensis	1.5	65	88	Activated carbon	4.0 g/L	10	1	≈ 100%	100 mL (△250)		Liang et al. 2010
Ac. brierleyi Ac. manzaensis Ms. sedula Sf. metallicus	1.5	65	56	Activated carbon	2.0 g/L	8	1	33.69% as Cu	100 mL (△250)	37-74 µm of AC	Ma et al. 2017
Lp. ferriphilum, At. caldus, Sb. thermosulfidooxidans, Fp. thermophilum	1.8	45	77	Graphite	2.0 g/L	15	2	2.3% as Cu	100 mL (△250)	$2 \text{ m}^2/\text{g}$ in specific surface are <75 $\mu$ m in size	Hao et al. 2018
Lp. ferriphilum, At. caldus, Sb. thermosulfidooxidans, Fp. thermophilum	1.8	45	86	Activated carbon	2.0 g/L	15	2	2.3% as Cu	100 mL (△250)	400 m <sup>2</sup> /g in specific surface are < 75 μm in size	Hao et al. 2018
Lp. ferriphilum, At. caldus, Sb. thermosulfidooxidans, Fp. thermophilum	1.8	45	95	Activated carbon	2.0 g/L	15	2	2.3% as Cu	100 mL (△250)	800 m <sup>2</sup> /g in specific surface are < 75 μm in size	Hao et al. 2018
Lp. ferriphilum, At. caldus, Sb. thermosulfidooxidans, Fp. thermophilum	1.8	45	66	Activated carbon	2.0 g/L	15	2	2.3% as Cu	100 mL (△250)	$1200 \text{ m}^2/\text{g}$ in specific surface are < 75 $\mu$ m in size	Hao et al. 2018

The addition of AC also shows a positive effect on the formation of scorodite (FeAsO<sub>4</sub>·2H<sub>2</sub>O) as an immobilized form of once-dissolved As from enargite (Jahromi et al., 2018). This would attribute to the catalytic reaction on the surface of AC; Asoxidation was greatly enhanced in the presence of AC, possibly by hydrogen peroxide generated (Radzinski et al., 2016). The enhanced As-oxidation on the AC surface led to the As(V) supply for the in-situ formation of scorodite during enargite leaching, consequently promoting the immobilization of As in the solid phase (Jahromi et al., 2018).

Although the catalytic mechanism of AC in the leaching process is roughly summarized as (i) electrochemical reaction to accelerate the electron transfer (e.g. galvanic interaction and other redox reaction) and (ii) chemical reaction by surface functional groups to produce the oxidant (e.g. Fe(III) and hydrogen peroxide), further discussion is still necessary to reach a consensus among researchers. Moreover, the number of studies investigating the effect of AC on enargite bioleaching is still limited, while the addition of AC in chemical enargite leaching are shown effective in enhanced Cu dissolution and As immobilization.

#### 1.4 The objective of this thesis

The objective of this thesis was set to seek a useful catalyst for the enhancement of Cu solubilization in enargite bioleaching. This work is divided into two parts; fundamental studies and application studies.

In the former part (fundamental studies), the catalytic effects of Ag and AC were evaluated in bioleaching of enargite concentrate and its catalytic mechanisms were elucidated. Prior to the bioleaching test, the applicability of molybdenum blue method to Cu sulfides leachate was tested for the determination of As(III) concentration in **chapter 3**. In **chapters 4 and 5**, the catalytic effect of Ag and AC was indeed tested in bioleaching of enargite concentrate using the mixed culture of moderately thermophilic microorganisms at 45°C. Clarification of the underlying catalytic mechanism was the main purpose of these chapters. Based on the result obtained in **chapter 5**, the detailed catalytic mechanism of AC was further tested by comparing the various type of AC in **chapter 6**. The most appropriate AC was determined for the enhancement of Cu solubilization from enargite during the bioleaching process.

In the latter part (application studies), obtained information from fundamental studies were applied to As-bearing copper concentrate for the further development of AC-catalyzed bioleaching system. AC-catalyzed bioleaching of As-bearing Cu concentrate with high pulp density was conducted in the stirred tank reactor to evaluate the catalytic effect of AC in scale-up system (**chapter 7**).

Finally, whole phenomena in the presence of catalysts were summarized, and future research strategy was proposed for the further development of the enargite bioleaching system.

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# Chapter 2

Methodology

# 2.1 Culture medium and chemical reagents

# 2.1.1 Culture media

# 2.1.1.1 Heterotrophic basal salts (HBS)

Solution composition of HBS  $(50 \times)$ 

22.5 g/L (NH4)<sub>2</sub>SO4
2.5 g/L KCl
2.5 g/L KH<sub>2</sub>PO4
25 g/L MgSO<sub>4</sub>·7H<sub>2</sub>O
0.7 g/L Ca(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O
7.1 g/L Na<sub>2</sub>SO4
Solubilized into distilled w
To make 1 L of HBS (1×) t

Solubilized into distilled water, stored in the sterilized bottle at ambient temperature. To make 1 L of HBS (1 $\times$ ) media, 20 mL of HBS stock (50 $\times$ ) was mixed with 980 mL of deionized water and sterilized by autoclave (120°C, 20 min).

# 2.1.1.2 Acidophilic basal salts (ABS)

Solution composition of ABS  $(50 \times)$ 

22.5 g/L (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> 2.5 g/L KCl 2.5 g/L KH<sub>2</sub>PO<sub>4</sub> 25 g/L MgSO<sub>4</sub>·7H<sub>2</sub>O 0.7 g/L Ca(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O 7.5 g/L Na<sub>2</sub>SO<sub>4</sub>·10H<sub>2</sub>O

Solubilized into distilled water, stored in sterilized bottle at ambient temperature. To make 1 L of ABS (1 $\times$ ) media, 20 mL of ABS stock (50 $\times$ ) was mixed with 980 mL of deionized water and sterilized by autoclave (120°C, 20 min).

# 2.1.2 Chemical reagents

# 1M Ferric iron stock solution

Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>·nH<sub>2</sub>O (n = 5-7; Wako pure chemicals) was solubilized into acidic distilled water (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>), and Fe<sup>3+</sup> concentration was measured by *o*-phenanthroline method using ascorbic acid as reducing agent. Based on the Fe<sup>3+</sup> concentration, the Fe<sup>3+</sup> stock was diluted with acidic distilled water until its Fe concentration becomes 1 M. Filtrated (0.2 µm) and stored in the sterilized bottle at  $4^{\circ}$ C.

#### 1M Ferrous iron stock solution

FeSO<sub>4</sub>·7H<sub>2</sub>O (Wako pure chemicals) was solubilized into acidic distilled water (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>), filtrated (0. 2 µm), and stored in the sterilized bottle at 4°C.

# 10 g/l As(III) stock solutions

NaAsO<sub>2</sub> (Sigma-Aldrich) was added into distilled water and acidified to pH 1.5 with  $H_2SO_4$ . The stock solutions were filter-sterilized through 0.2 µm polyethersulfone membranes (Steritop, Millipore) and stored at 4°C.

# 10 g/l As(V) stock solutions

Na<sub>2</sub>HAsO<sub>4</sub>·7H<sub>2</sub>O (Junsei Chemical) was added into distilled water and acidified to pH 1.5 with H<sub>2</sub>SO<sub>4</sub>. The stock solutions were filter-sterilized through 0.2  $\mu$ m polyethersulfone membranes (Steritop, Millipore) and stored at 4°C.

# 10% (w/v) Yeast extract stock solution

Yeast extract (Sigma-Aldrich) was solubilized into acidic distilled water (pH 2.0 with  $H_2SO_4$ ), filtered (0.2 µm), and stored in the sterilized bottle at 4°C.

# *Trace elements (1000×) stock solution*

The following chemicals (Wako pure chemicals) were solubilized into distilled water, filtrated ( $0.2 \mu m$ ), and stored in sterilized bottle at 4°C.  $10 \text{ mg/L ZnSO}_4 \cdot 7H_2O$   $1 \text{ mg/L CuSO}_4 \cdot 5H_2O$   $1 \text{ mg/L CuSO}_4 \cdot 5H_2O$   $1 \text{ mg/L CoSO}_4 \cdot 7H_2O$   $0.39 \text{ mg/L Cr}_2(SO_4)_3 \cdot 7H_2O$   $0.6 \text{ mg/L H}_3BO_3$   $0.5 \text{ mg/L Na}_2MoO_4 \cdot 2H_2O$   $0.1 \text{ mg/L NaSO}_4 \cdot 6H_2O$   $0.51 \text{ mg/L Na}_2SeO_4$  $0.1 \text{ mg/L Na}_2WO_4 \cdot 2H_2O$ 

# Sterilized elemental sulfur powder

Powder of elemental sulfur (Wako pure chemicals) was sterilized in the oven (100°C, overnight, thrice) and stored in the sterilized bottle at 4°C.

# 2.2 Microorganisms used in this study

All the cultures were maintained in 300 mL Erlenmeyer flask containing 100 mL HBS or ABS media (pH adjusted as the above) supplemented with the electron donors and yeast extract or trace elements, as is described below.

# 2.2.1 Acidimicrobium ferrooxidans strain ICP<sup>T</sup> (DSM 10331)

*Am. ferrooxidans* ICP (Clark and Norris, 1996) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>) with 10 mM  $Fe^{2+}$  and 0.02% (w/v) yeast extract. Flasks were incubated at 45°C, shaken at 150 rpm (G·BR-200, Taitec).

# 2.2.2 Sulfobacillus sibiricus strain N1<sup>T</sup> (DSM 17363)

*Sb. sibiricus* N1 (Melamud et al., 2003) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>) with 10 mM Fe<sup>2+</sup> and 0.02% (w/v) yeast extract. Flasks were incubated at 45°C, shaken at 150 rpm (G·BR-200, Taitec).

# 2.2.3 Acidithiobacillus caldus strain KU<sup>T</sup> (DSM 8584)

*At. caldus* KU (Hallberg and Lindström, 1994) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>) with 0.01% (w/v) S<sup>0</sup> and trace element solution (×1). Flasks were incubated at 45°C, shaken at 150 rpm (G·BR-200, Taitec).

#### 2.2.4 Acidiplasma sp. strain Fv-Ap

*Acidiplasma* sp. Fv-Ap (kindly provided by Prof. D.B. Johnson, Bangor University, UK) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.5 with  $H_2SO_4$ ) with 10 mM Fe<sup>2+</sup> and 0.02% (w/v) yeast extract. Flasks were incubated at 45°C, shaken at 150 rpm (G·BR-200, Taitec).

#### 2.2.5 Leptrospirillum ferriphilum strain P<sub>3</sub>A<sup>T</sup> (DSM 14647)

*Lp. ferriphilum*  $P_3A$  (Coram and Rowlings, 2002) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.7 with H<sub>2</sub>SO<sub>4</sub>) with 20 mM Fe<sup>2+</sup>, 0.01% (w/v) pyrite and trace element solution (×1). Flasks were incubated at 37°C, shaken at 150 rpm (G·BR-200, Taitec).

#### 2.2.5 Ferroplasma acidiphilum strain Y<sup>T</sup> (DSM 12658)

*Fp. acidiphilum* Y (Golyshina et al., 2000) was maintained in 300 ml Erlenmeyer flask containing 100 ml of HBS or ABS medium (pH 1.5 with H<sub>2</sub>SO<sub>4</sub>) with 10 mM Fe<sup>2+</sup> and 0.02% (w/v) yeast extract. Flasks were incubated at 35°C, shaken at 150 rpm (G·BR-200, Taitec).

#### 2.3 Mineral samples used in this study

#### Enargite (Cu<sub>3</sub>AsS<sub>4</sub>)

Enargite concentrate (produced in Peru) was kindly provided by JX Nippon Mining & Metals. For all the enargite bioleaching experiments, acid-washed enargite concentrate was used.

#### Pyrite (FeS<sub>2</sub>)

Pyrite concentrate (produced in Chile) was purchased by IWAMOTO mineral. Finely ground pyrite concentrate was used for the cultivation of microorganisms.

#### D3 concentrate

D3 concentrate (produced in Chile) was kindly by JOGMEC (Japan Oil, Gas and Metals National Corporation). D3 concentrate was directly used for the bioleaching experiment without washing.

# Acid wash treatment

The concentrates were washed with 1 M HNO<sub>3</sub> (5 min, 25°C), deionized water (5 min, 25°C), and finally with 100% ethanol (5 min, 25°C) in order to remove residual metals and surface oxide film on the concentrate. After that, the concentrate was freeze-dried overnight.

$\frac{1}{20}$
20
39
22
20
7.1
0.39
0.32
0.22
0.18
0.08
2.7
3.2
0.89
0.04
100 ppm
00 ppm

Table 2.1 Elemental composition of enargite concentrate.

Mineral	Chemical formula	wt% <sup>*</sup>
Enargite	Cu <sub>3</sub> AsS <sub>4</sub>	37.4
Pyrite	FeS <sub>2</sub>	47.3
Chalcopyrite	CuFeS <sub>2</sub>	
Tennantite	$(Cu,Fe)_{12}As_4S_{13}$	
Sphalerite	ZnS	
Stibnite	$Sb_2S_3$	
Quartz	SiO <sub>2</sub>	
Gibbsite	Al(OH) <sub>3</sub>	
Alunite	$KAl_3(SO_4)_2(OH)_6$	

Table 2.2 Mineralogical composition of enargite concentrate.

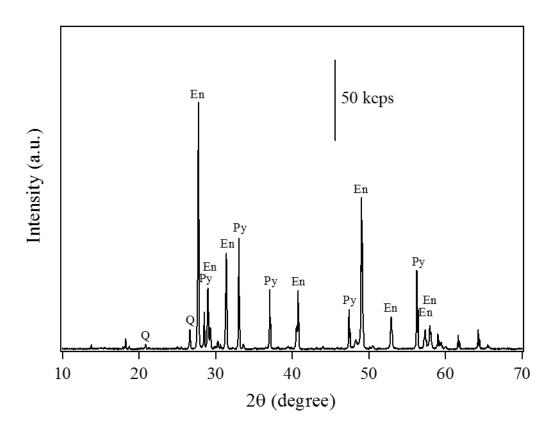


Fig. 2.1 X-ray diffraction patterns of original enargite concentrate. En: enargite  $(Cu_3AsS_4; PDF No. 00-035-0775)$ , Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>: PDF No. 01-070-3755).

Elemental composition of D3				
-	Elements	Ratio (%)		
-	As	4.16		
	Cu	29.6		
	Fe	17.65		
	Zn	4.08		
	Sb	0.31		
	S	31.7		
	Ag	0.04		
	Al	0.09		
	Ca	0.13		
	Mg	0.03		
	Na	0.02		
	Κ	0.1		
	Cd	268 ppm		
	Cr	10 ppm		
	Hg	4 ppm		
	Mo	309 ppm		
-	Pb	4290 ppm		

Table 2.3 Elemental composition of D3 concentrate.

Table 2.4 Mineralogical composition of D3 concentrate.

Mineral	Chemical formula	wt% <sup>*</sup>
Enargite	$Cu_3AsS_4$	21
Pyrite	FeS <sub>2</sub>	30
Chalcopyrite	CuFeS <sub>2</sub>	12
Tennantite	$(Cu,Fe)_{12}As_4S_{13}$	1.8
Bornite	Cu <sub>5</sub> FeS <sub>4</sub>	6.7
Chalcocite	Cu <sub>2</sub> S	14
Geerite	$Cu_8S_5$	3.8
Tetrahedrite	$(Cu,Fe,Zn,Ag)_{12}Sb_3S_4$	1.0
Other Cu suflde		1.3
Other sulfide		5.2
Gangue		3.1

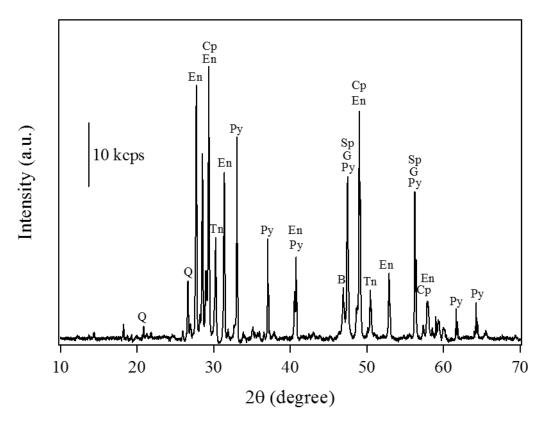


Fig. 2.2 X-ray diffraction patterns of original D3 concentrate. En: enargite (PDF No. 03-065-1097), Cp: chalcopyrite (PDF No. 01-075-6866), Py: pyrite (PDF No. 00-042-1340), Q: Quartz (PDF No. 01-086-1560), B: bornite (PDF No. 01-073-1667), Tn: tennantite (PDF No. 01-074-1027), Sp: sphalerite (PDF No. 01-077-8756), G: geerite (PDF No. 00-033-0491).

# 2.4 Sampling procedures

# 2.4.1 Liquid samples

Liquid samples were regularly taken from the experimental cultures after compensation of water evaporation with pure water, and then used for cell counting using a microscope, filtered using 0.2  $\mu$ m cartridge filters, and used for the determination of metal concentrations, pH values, and solution redox potential (*E*<sub>h</sub>) values.

# 2.4.2 Solid residues

At the end of the experiments, solid residues were collected by filtration using the vacuum pump, and freeze-dried overnight.

#### **2.5 pH and solution redox potential** $(E_h)$ measurements

Solution pH and redox potential values ( $E_h$ ; Ag/AgCl reference electrode) were measured using pH- $E_h$  meter (MM-60R, TOADKK). The measured  $E_h$  values were automatically converted to values vs. SHE as follows;

*E*<sub>h</sub> (mV vs. SHE)

$$= E_{\rm h} (\rm mV \ vs. \ Ag/AgCl) + 206 - 0.7 ("Solution Temp." - 25)$$
(Eq. 2-1)

#### 2.6 Spectrophotometry

# 2.6.1 *o*-phenanthroline method

*o*-phenanthroline method was used in this study as a  $Fe^{2+}$  assay. The procedures are described below (Caldwell and Adams, 1946).

1. Add 30  $\mu L$  of 1 M HCl to some wells of 96-well measuring plate.

2. Add 3  $\mu$ L of liquid samples to the wells. Note that all samples were filtered to remove all particles, and subsequently diluted (e.g., ×10) using 1 M HCl if needed. 3. Add 30  $\mu$ L of ascorbic acid solution to the wells for the determination of total soluble Fe. Note that ascorbic acid solution was made right before the measurement since the chemical is unstable in solution (one spoon of ascorbic acid powder (Wako pure chemicals) solubilized into 5 mL of distilled water).

4. Give 5 min to react to  $Fe^{3+}$  ions with ascorbic acid.

5. Add 30  $\mu$ L of 5 mM *o*-phenanthroline solution (solubilized in deionized water; Wako pure chemical) to the wells in order to form [Fe(phenanthoroline)<sub>3</sub>]<sup>2+</sup> complex.

6. Add 30  $\mu$ L of 2 M sodium acetate solution (solubilized in deionized water; Wako pure chemical) to the wells.

7. Add distilled water to make the volume up to 300  $\mu$ L.

8. Give 10 min for reaction time.

9. Measure the absorbance at 510 nm using spectrophotometer (Multiskan Go, Thermo Scientific).

A standard curve used is shown in Fig. 2.3. Note that the calibration curve was re-drawn every time new chemical reagents were made.

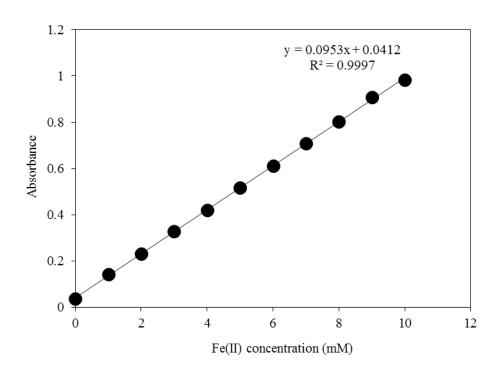


Fig. 2.3 Standard curve of Fe<sup>2+</sup> concentration determined by *o*-phenanthroline method.

# 2.6.2 Ferrozine method

For the determination of  $Fe^{2+}$  concentration during bioleaching As-bearing copper sulfide, Ferrozine method was used instead of *o*-phenanthroline method. The procedures are described below (Lovely and Phillips, 1987).

Ferrozine solution

1. Dissolve 0.59575 g HEPES in 40 mL deionized water and adjust pH to 7.0 with 1 M KOH.

2. Add 0.05 g ferrozine (3-(2-pyridyl)-5,6-bis(4-phenyl-sulfonic acid)-1,2,4-triazine; Wako pure chemical).

3. Make up to 50 mL with deionized water.

This ferrozine solution must be kept in a dark place for up to 1 month.

#### Procedure

1. Add 10  $\mu$ L of liquid samples to the wells of 96-well measuring plate. Note that all samples were filtered to remove all particles, and subsequently diluted (e.g.,  $\times$ 10) using 1 M H<sub>2</sub>SO<sub>4</sub> if needed.

2. Add 290  $\mu L$  of the mixed reagent of ferrozine solution to the wells.

3. Give 10 min to get stable.

4. Measure absorbance at 562 nm using spectrophotometer (Multiskan Go, Thermo Scientific).

A standard curve used is shown in Fig. 2.4. Note that calibration curve was re-drawn every time new chemical reagents were made.

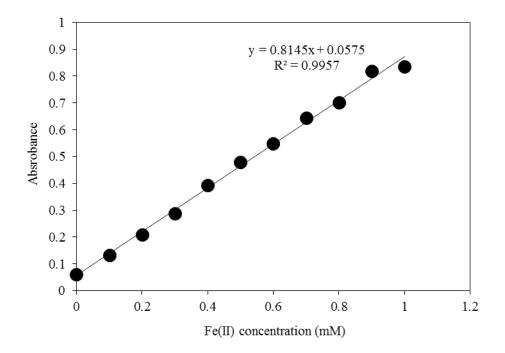


Fig. 2.4 Standard curve of  $Fe^{2+}$  concentration determined by ferrozine method.

# 2.6.3 Molybdenum blue method

Molybdenum blue method was used for the determination of As(III) concentration. The details are described in chapter 3.

#### 2.6.4 Turbidimetric method

Turbidimetic method was used in this study as a sulfate assay. The procedures are described below.

#### Conditioning reagent

1. Add 50 mL glycerol (Wako pure chemical), 30 mL concentrated HCl, 10 mL 95% ethanol (Wako pure chemical), and 75 g sodium chloride (Wako pure chemical) into 250 mL of deionized water.

2. Make up to 500 mL with deionized water.

#### Procedure

1. Add 100  $\mu$ L of liquid samples to the 1.5 mL tube. Note that all samples were filtered to remove all particles, and subsequently diluted (e.g., ×10) using 1 M HCl if needed.

2. Add 900 µL of conditioning reagent and mix thoroughly.

3. Add fine-grain barium chloride (ca. 60 mg; Wako pure chemical) and mix the solution with vortex for 1 min.

4. Transfer the solution into the wells of 96-well measuring plate and measure absorbance at 420 nm using spectrophotometer (Multiskan Go, Thermo Scientific).

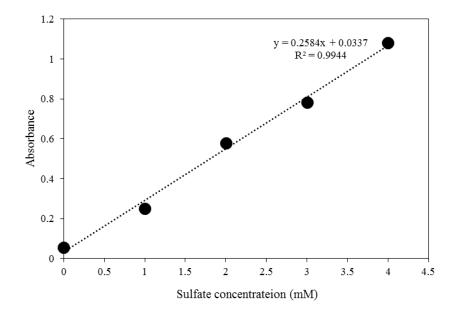


Fig. 2.5 Standard curve of sulfate concentration determined by turbidimetric method.

# 2.7 Inductively coupled plasma-optical emission spectrometry (ICP-OES)

Concentrations of total soluble metal ions (e.g., Fe, Cu, As) in acid solution samples were measured using ICP-OES (Optima 8300DV, PerkinElmer Japan Co., Ltd). After original liquid samples were taken from Erlenmeyer flasks, falcon tubes or serum bottles, they were filtered (0.20  $\mu$ m) or centrifuged (12,000 rpm, 8 min) using Minispin (Eppendolf) in order to separate solution and solid phases, and subsequently diluted depending on estimated concentrations of target metal ions in them (e.g., ×25, 100, 250) using 0.1 M HNO<sub>3</sub>. All the measurements using ICP-OES were carried out in duplicates: The average values were used for the results. Wavelengths measured for each metal are described as follows:

Fe: 238.204, 239.562, 259.939 nm

Cu: 327.393, 324.752, 224.700 nm

As: 188.979, 193.696, 197.197 nm

# 2.8 X-ray diffraction (XRD)

XRD measurement (Ultima IV, Rigaku) was performed with Cu-K $\alpha$  radiation as an X-ray source. The accelerating voltage and current were 40 kV and 40 mA, with a scanning speed of 2°/min and scanning step of 0.02°.

# 2.9 Electron probe micro analyzer (EPMA)

For the preparation of EPMA specimens, the freeze-dried samples were embedded in resin and polished to determine the chemical composition of constituent minerals by Electron Probe Micro Analyzer (EPMA; JEOL JXA-8530F; 6 nA, 20 kV). The incident electron beam was focused to 1 mm in diameter, and counting time was set to 20 seconds for each element. The acquired X-ray intensities were corrected by ZAF method to obtain element concentrations for quantitative analysis. (Boekestein et al., 1983).

# 2.10 Attenuated total reflection Fourier transform infrared spectroscopy (ATR-FT-IR)

For the analysis of surface functional groups of AC, attenuated total reflection Fourier transform infrared spectroscopy (ATR-FT-IR) was employed using FT/IR-670

(JASCO) with ZnSe crystal in the range of  $360-4000 \text{ cm}^{-1}$  (resolution:  $16 \text{ cm}^{-1}$ ).

#### 2.11 Raman spectroscopy

For the analysis of the structure of AC, Raman spectroscopy was employed using DXR Smart Raman (Thermo Scientific) with 532 nm laser (10 mW).

# 2.12 Microwave treatment

Hydrothermal pre-treatment was carried out as follows: Teflon vessels containing a known amount of solid samples and 60% HNO<sub>3</sub> solution or aqua regia (12M HCL and 60% HNO<sub>3</sub> are mixed in a volume ratio 3:1) were placed in the microwave digestion system (Ethos Plus, Milestone) and heated to 230°C with 7°C /min increments, kept for 15 min at 230°C, and finally allowed to cool to room temperature.

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Chapter 2 Methodology

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# Chapter 3

Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

# Abstract

The effect of co-existing metal ions such as copper (Cu) and iron (Fe) was studied for the application of modified molybdenum blue method (arsenic-antimony-molybdenum ternary chelation) to Cu sulfide leachate. While solo metal contamination (20 mM Fe<sup>2+</sup>, 20 mM Fe<sup>3+</sup>, or 25 mM Cu<sup>2+</sup>) showed no inhibitory effect on arsenic (As) determination, large amount of metal ions composed of 25 mM Fe<sup>2+</sup>, 25 mM Fe<sup>2+</sup>, and 50 mM Cu<sup>2+</sup> (100 mM in total) led to slight oxidation of As(III) to As(V) (4% in 15 min), resulting in the overestimation of As(V) (the underestimation of As(III)). Phosphate, which also chelates with molybdic acid, was also tested as a minor inhibitor of As(III) quantification usually contained in Cu sulfide leachate. While < 2.5 mM of phosphate was capable of chelating at the same ratio with As, more existence would completely consume molybdic acid, resulting in the unsuccessful standard curve. Applicability of this method to Cu sulfide leachate was indeed confirmed through the test using real Cu leachate obtained by bioleaching of enargite (Cu<sub>3</sub>AsS<sub>4</sub>) concentrate. Recommended procedure for As determination was finally summarized, which is specially modified for Cu sulfide leachate.

# **3.1 Introduction**

Along with the recent depletion of high-grade copper ore, the contamination of Asbearing minerals such as enargite ( $Cu_3AsS_4$ ) and tennantite ( $Cu_{13}AsS_{14}$ ) become increasingly serious problems. Since these minerals are also expected as one of the potential future copper resources, the novel approach for extraction of Cu from them has been therefore desperately required. For the exploitation of these minerals, the hydrometallurgical process has been thought appropriate since toxic As leached from the minerals remains in the solution phase in this process, while As in the minerals are volatilized to the air with unmanageable form in the pyrometallurgical process, resulting in the cause of air pollution. However, even after the hydrometallurgical process, dissolved As must be strictly managed not to leak them into the environment by using a physic-chemical treatment such as the adsorption and co-precipitation.

Dissolved As in the solution such as Cu sulfide leachate is predominantly present in the form of inorganic trivalent arsenic, As(III) (arsenite;  $H_2AsO_3^-$ ), and pentavalent arsenic, As(V) (arsenate;  $H_2AsO_4^{2^-}$ ), with the former being more toxic and mobile than the latter, especially at acidic pH (Matschullat, 2000; Hung et al., 2004). Since As(V) is more effectively immobilized than As(III), a pre-treatment is required to oxidize As(III) to As(V) by using strong oxidizing reagents before the immobilization step. Prior to pre-treatment, As(III) concentration needs to be determined to know the desired amount of the oxidant to accomplish As(III) oxidation for the economic process.

To determine the As(III) concentration, the various measurement techniques have been developed in the past several decades, such as Anodic Stripping Voltammetry (ASV) (Kopanica and Novotný, 1998), Hydride Generation–Atomic Absorption Spectrometry (HG-AAS) (Shraim et al., 1999), High Performance Liquid Chromatography (HPLC) (Raessler et al., 2000), and Inductively Coupled Plasma–Optical Emission Spectrometry (ICP-OES) (Amran et al., 1997). However, some of these measurements have following disadvantages: (i) necessity of expensive facilities and a large amount of chemicals, (ii) not applicable to in-situ measurement (Dasgupta et al., 2002), (iii) high dilution rate (around 10000 times), leading to the large dilution error. In terms of the last one, these measurement techniques are, in other words, susceptible to the tiny amount of As, which are assumed to be applied for the analysis of the drinking or ground water. In the case of the leachate containing a high concentration of As, however,

the sample needs to be diluted many times for the application to the above techniques, resulting in the seriously large dilution error. Therefore, an alternative method is desirable, which is capable of *in-situ* quick measurement with less dilution.

To overcome this problem, colorimetric molybdenum blue method is considered as one of the promising techniques, which has been proposed by Osmond (1887) and improved by a number of researchers (Bogdanova, 1984; Carvalho et al., 1998; Johnson and Pilson, 1972). Molybdenum blue method is based on the formation of the molybdic heteropoly-acid complex: Molybdenum blue is formed via the reduction of the complex composed of As and molybdic acid under acidic condition. However, color development has been known as a slow-step in this conventional method, requiring the heating for the time-reduction. To shorten this time-consuming process, the modified molybdenum blue method was developed by Murphy and Riley (1962), where ascorbic acid was used as a reducing reagent in the presence of trivalent antimony to form the arsenic-antimony-molybdenum ternary complex. Owing to this modification, reaction time was shortened to less than 15 minutes even at room temperature (Blomqvist et al., 1993).

Common contaminants in ground water, such as phosphate, fluoride, and silicate, have been recognized as the inhibitory elements of molybdenum blue method, which is also able to form the heteropoly-acid complex with molybdic acid (Blomqvist et al., 1993; Kitazume and Yagi, 1981). In order to eliminate their inhibitory effects, oxidation and/or reduction of As species have been tested (Lenoble et al., 2003; Tsang et al., 2007); only As(V) but not As(III) is detectable by molybdenum blue method, the oxidation and reduction of As species in samples enable to observe different As species separated from major inhibitory elements as mentioned above. However, the number of studies investigating the inhibitory effect of Fe and Cu on molybdenum blue method is limited. When Cu sulfide leachate is assumed the sample, the major contaminant is not phosphate, fluoride, and silicate but metal ions such as Cu and Fe, suggesting that the effect of these metal ions must be investigated. Therefore, the objective of this study was set to evaluate the inhibitory effect of metal ions on modified molybdenum blue method for application to Cu sulfide leachate.

# **3.2 Materials and methods**

# 3.2.1. Solution reagents for analysis

All solution reagents were prepared with deionized water. Ascorbic acid solution was prepared right before the measurement by dissolving 0.03 g L-ascorbic acid ( $C_6H_8O_6$ ; Wako pure chemical) in 5 mL deionized water to be 0.6% (w/v) in final concentration. The stock solution of 1 mM potassium permanganate (KMnO4; Wako pure chemical) was made as an oxidizing reagent for As(III) and stored in a dark plastic bottle. The stock solution of molybdenum-antimony reagent containing 1% (w/v) ammonium molybdate tetrahydrate ((NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>14</sub>•4H<sub>2</sub>O; Wako pure chemical) and 0.02% (w/v) potassium antimonyl tartrate (K<sub>2</sub>(SbO)<sub>2</sub>C<sub>8</sub>H<sub>4</sub>O<sub>10</sub>•3H<sub>2</sub>O; Sigma Aldrich) was also prepared. For acidification, 1M sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) was used.

# 3.2.2. Arsenic and phosphate standard solution

Each solution of 50 mM As(III) (arsenite) and As(V) (arsenate) were prepared by dissolving sodium meta-arsenite (NaAsO<sub>2</sub>; Wako pure chemical) and sodium arsenate heptahydrate (Na<sub>2</sub>HAsO<sub>4</sub>·7H<sub>2</sub>O; Junsei Chemical), which were diluted to 0.5, 1.0, 2.5, 5.0 with 0.1 mM H<sub>2</sub>SO<sub>4</sub> to draw the standard curve. The As standard solutions containing 20 mM Fe<sup>2+</sup> (as FeSO<sub>4</sub>·7H<sub>2</sub>O; Wako pure chemical), 20 mM Fe<sup>3+</sup> (as Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>·nH<sub>2</sub>O; Wako pure chemical), 25 mM Cu<sup>2+</sup> (as CuSO<sub>4</sub>·5H<sub>2</sub>O; Wako pure chemical), or mixture of 25 mM Fe<sup>2+</sup>, 25 mM Fe<sup>3+</sup>, and 50 mM Cu<sup>2+</sup> were also tested to evaluate the effect of co-existing metals. Separately, phosphate standard solution was prepared by dissolving potassium dihydrogen phosphate (KH<sub>2</sub>PO<sub>4</sub>; Wako pure chemical) with the same variety of concentration as As standard solution.

# 3.2.3. Analytical procedure

All absorbance measurements were carried out in 96-well plastic plate by Multiscan GO (Thermo Fisher Scientific). Three  $\mu$ L of sample solution was mixed with 30  $\mu$ L H<sub>2</sub>SO<sub>4</sub>, 30  $\mu$ L ascorbic acid, 30  $\mu$ L molybdenum-antimony stock solution, and 207  $\mu$ L deionized water to make the mixture up to 300  $\mu$ L for As(V) detection. In order to measure the total As concentration, 30  $\mu$ L potassium permanganate was further added prior to adding ascorbic acid and reduce the deionized water to 177  $\mu$ L; note that the order of the addition must not be changed. These mixtures were prepared in

quadruplicate. The time dependence of color development was investigated by changing the reaction time before the absorbance measurement from 15 min to 30 min with 5 min interval. Absorbance of the solution was read at 880 nm (Blomqvist et al., 1993).

# **3.2.4.** Application to real copper sulfide leachate

In order to evaluate the applicability of modified molybdenum blue method to copper sulfide leachate, bioleaching of enargite concentrate was carried out to obtain the real copper leachate used for the determination of As concentration. The detail of the bioleaching experiment was mentioned by Oyama et al. (2018). Enargite concentrate, mainly containing 7.1% As, 20% (w/w) Cu, 22% Fe, and 39% S, was added into the HBS media.(initial pH adjusted to 2.0; 200 mL in 500 mL Erlenmeyer flask), followed by the sterilization by autoclaving. Mixed culture of moderately thermophilic bacteria was inoculated. This flask was incubated and shaken at 45°C and 150 rpm. Solution sample was regularly withdrawn to monitor As concentration by molybdenum blue method. As concentration was also determined by ICP-OES to compare with the value obtained by molybdenum blue method.

# 3.3 Results and discussion

# 3.3.1 Check for the pure arsenic standard solution

At first, pure As standard solutions were tested for the absorbance measurements to obtain the ideal standard curve for the determination of As concentration. In the absence of any contaminants, standard curves were successfully drawn in the range from 0 to 5 mM (Fig. 3.1, Table 3.1; Eqs. 3-1 to 3-16). In addition to the complete As(III) oxidation by KMnO<sub>4</sub> (Fig. 3.1a,b, Table 3.1; Eqs. 3.1 to 3.8), the difference in the standard curve equation using As(V) standard solution between in the presence and absence of KMnO<sub>4</sub> was negligible (Fig. 3.1c,d, Table 3.1; Eqs. 3-9 to 3-16). This confirmed that KMnO<sub>4</sub> is appropriately applicable to this method as an oxidant for As(III). Since color-development was apparently visible until 15 min of reaction time, time-course color-development after 15 min was monitored by absorbance measurement with 5 min interval. The slope changes with time course were also negligibly small (< 0.05) in every case (Table 3.1; Eqs. 3.1 to 3.16). Based on these results, the optimal reaction time of this method was decided to be 15 min.

# Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

Standard solution	$KMnO_4$	Reaction time (min)	Stadard curve	$R^2$	Equation number	Referen
		15	y = -0.0003x + 0.0633	0.3958	3-1	
	-	20	y = -0.0004x + 0.0627	0.5521	3-2	Fig. 3.1
		25	y = -0.0003x + 0.0628	0.3260	3-3	8: -:-
As(III)		30	y = -0.0003x + 0.0627	0.4330	3-4	
		15	y = 0.1865x + 0.0648	0.9999	3-5	
	+	20	y = 0.1854x + 0.0646	0.9999	3-6	Fig. 3.1
		25	y = 0.1845x + 0.0654	0.9998	3-7	C
		30	y = 0.1839x + 0.0657	0.9998	3-8	
		15	y = 0.1711x + 0.0636	1.0000	3-9	
	-	20	y = 0.1697x + 0.0636	0.9999	3-10	Fig. 3.1
		25	y = 0.1692x + 0.0643	0.9999	3-11	e
As(V)		30	y = 0.1688x + 0.0646	0.9999	3-12	
		15	y = 0.1712x + 0.0631	1.0000	3-13	
	+	20	y = 0.1701x + 0.0628	1.0000	3-14	Fig. 3.
		25	y = 0.1696x + 0.0633	1.0000	3-15	e
		30	y = 0.1689x + 0.0638	1.0000	3-16	
		15	y = 0.197x + 0.0722	0.9976	3-17	
	-	20	y = 0.1973x + 0.0743	0.9967	3-18	Fig. 3.2
		25	y = 0.1978x + 0.0758	0.9960	3-19	U
$PO_4$		30	y = 0.1989x + 0.0778	0.9949	3-20	
-		15	y = 0.1909x + 0.0721	0.9985	3-21	
	+	20	y = 0.1908x + 0.0736	0.9979	3-22	Fig. 3.1
		25	y = 0.1916x + 0.0747	0.9977	3-23	U
		30	y = 0.1915x + 0.0755	0.9974	3-24	
		15	y = 0.0006x + 0.0614	0.7322	3-25	
	-	20	y = 0.0005x + 0.0614	0.7040	3-26	Fig. 3.1
		25	y = 0.0007x + 0.0608	0.8169	3-27	U
$As(III) + 20 \text{ mM Fe}^{2+}$		30	y = 0.0009x + 0.0611	0.8727	3-28	
15(111) + 20 11101 1 0		15	y = 0.1895x + 0.0654	1.0000	3-29	
	+	20	y = 0.1883x + 0.0663	0.9999	3-30	Fig. 3.1
		25	y = 0.1872x + 0.0672	0.9999	3-31	8
		30	y = 0.1864x + 0.0688	0.9999	3-32	
		15	y = 0.0008x + 0.0627	0.8200	3-33	
	-	20	y = 0.0009x + 0.0625	0.8971	3-34	Fig. 3.1
		25	y = 0.0011x + 0.0619	0.9396	3-35	0
$As(III) + 20 \text{ mM Fe}^{3+}$		30	y = 0.0012x + 0.0625	0.9546	3-36	
15(11) + 20 1101 1 0		15	y = 0.1907x + 0.0689	0.9992	3-37	
	+	20	y = 0.1895x + 0.0703	0.9991	3-38	Fig. 3.1
		25	y = 0.188x + 0.0709	0.9990	3-39	8
		30	y = 0.1878x + 0.072	0.9991	3-40	
		15	y = 0.0003x + 0.0691	0.7174	3-41	
	-	20	y = 0.0005x + 0.0693	0.7768	3-42	Fig. 3.
		25	y = 0.0004x + 0.0698	0.6891	3-43	8. 0.
$As(III) + 25 \text{ mM Cu}^{2+}$		30	y = 0.0005x + 0.0702	0.7824	3-44	
$As(III) + 25 \text{ mM Cu}^{-1}$		15	y = 0.1856x + 0.0756	0.9997	3-45	
	+	20	y = 0.1837x + 0.0777	0.9996	3-46	Fig. 3.
		25	y = 0.1826x + 0.0796	0.9995	3-47	- 15. 3.
		30	y = 0.1817x + 0.0808	0.9995	3-48	
		15	y = 0.0081x + 0.0681	0.9988	3-49	
A c(III)	-	20	y = 0.0098x + 0.068	0.9991	3-50	Fig. 3.4
As(III)	-	25	y = 0.0114x + 0.0676	0.9994	3-51	<b>.</b> њ. <i>Э</i> .
+ 25 mM Fe <sup>2+</sup>		30	y = 0.0132x + 0.0677	0.9991	3-52	
+ 25 mM Fe <sup>3+</sup>		15	y = 0.1852x + 0.0742	0.9999	3-53	
+ 50 mM Cu2+	+	20	y = 0.1834x + 0.0752	0.9999	3-54	Fig. 3.4
	т	25	y = 0.1828x + 0.0753	0.9999	3-55	1 1g. J.
	<u> </u>	30	y = 0.1823x + 0.0758	0.9999	3-56	
		15	y = 0.1725x + 0.0714	0.9992	3-57	
A (TT)	_	20	y = 0.1708x + 0.0715	0.9993	3-58	Fig. 3.4
As(V)	-	25	y = 0.1696x + 0.0719	0.9992	3-59	1'lg. 3.4
+ 25 mM Fe <sup>2+</sup>		30	y = 0.1696x + 0.0723	0.9993	3-60	
+ 25 mM Fe <sup>3+</sup>		15	y = 0.1733x + 0.0715	0.9994	3-61	
+ 50 mM Cu <sup>2+</sup>	1	20	y = 0.1718x + 0.0714	0.9995	3-62	Ein 2
1 50 may Cu	+	25	y = 0.171x + 0.0716	0.9994	3-63	Fig. 3.4

Table 3.1 List of the standard curve equations and  $R^2$  values.

Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

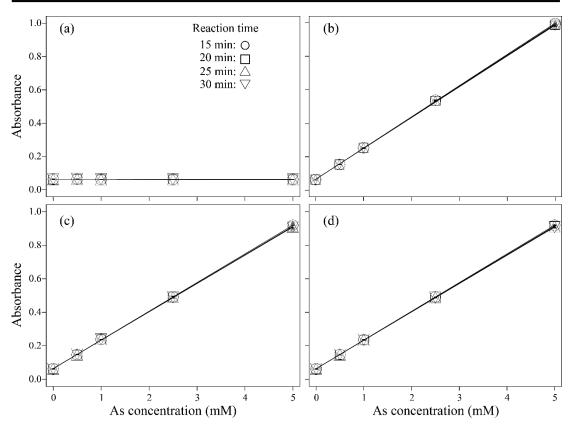


Fig. 3.1 Relationship between absorbance and As concentration with the reaction time of 15 min ( $\bigcirc$ ), 20 min ( $\square$ ), 25 min ( $\triangle$ ), and 30 min ( $\nabla$ ). As(III) (a,b) and As(V) (c, d) standard solution without (a, c) and with KMnO<sub>4</sub> (b, d) were used for the analysis. Markers, error bars, and standard curves were overlapped due to the high reproducibility.

# 3.3.2 Test of phosphate as a major inhibitor of As detection

Even though its concentration is low, phosphate might be dissolved from some gangues or clay minerals during the leaching process. Moreover, if the biological technique is employed to enhance the dissolution of Cu sulfides, acid basal salts medium must be used as a lixiviant for the microbial growth during the leaching process, which contains phosphate compounds as a component. Since this phosphate is also capable of chelating with molybdic acid and possibly inhibiting the detection of As, the effect of phosphate must be evaluated in the molybdenum blue method.

In the range of phosphate concentration from 0 to 2.5 mM, standard curve was successfully drawn, and time-course color-development was negligible even after 30 min of reaction time (Fig. 3.2, Table 3.1; Eqs. 3-17 to 3-24). While Blomqvist et al. (1993) reported that the reaction rate of phosphate differed from that of arsenate, similar reaction-rate (slope of the standard curve equation) was obtained in this study (see Eqs. 3-5 to 3-8 and Eqs. 3-21 to 3-24 in Table 3.1). However, with increase of phosphate concentration to 5.0 mM, slope and R<sup>2</sup> values suddenly dropped to around 0.15 and 0.98, respectively. This could attribute to the difference in the mechanism of chelating with molybdic acid; phosphate could require a larger amount of molybdic acid to form the complex than arsenate, possibly resulting in the complete consumption of molybdic acid and the unsuccessful standard curve. These observations suggest that phosphate concentration in the basal salt medium is basically around 0.2 mM (10 times lower than the above limit), Cu sulfide leachate would be directly applicable to this As detection method.

Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

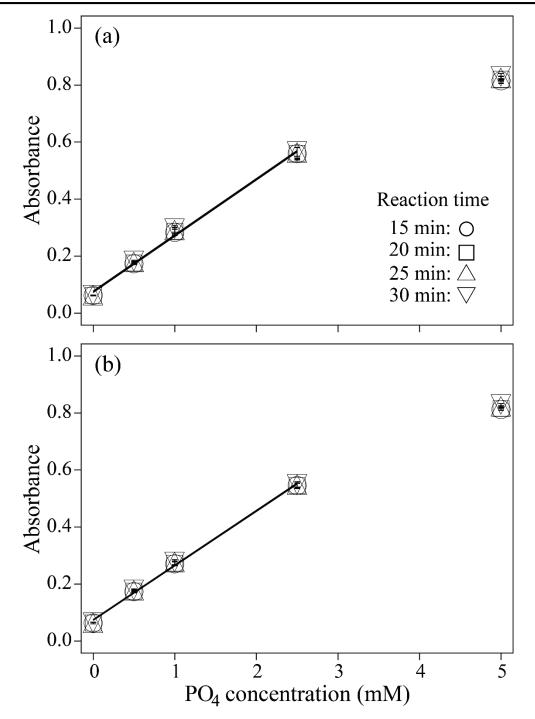


Fig. 3.2 Relationship between absorbance and PO<sub>4</sub> concentration with the reaction time of 15 min ( $\bigcirc$ ), 20 min ( $\square$ ), 25 min ( $\triangle$ ), and 30 min ( $\bigtriangledown$ ). PO<sub>4</sub> standard solution without (a) and with KMnO<sub>4</sub> (b) were used for the analysis. Markers, error bars, and standard curves were overlapped due to the high reproducibility.

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### 3.3.3. Evaluation of Fe<sup>2+</sup>, Fe<sup>3+</sup>, and/or Cu<sup>2+</sup> as the inhibitors for As detection

In order to evaluate the effect of possible inhibitory metals contained in Cu sulfide leachate, the As standard solutions mixed with Fe and/or Cu ware also tested. Solo metal contamination showed no inhibitory effect on the As detection by molybdenum blue method (Fig. 3.3). The standard curves hardly changed even in the presence of either 20 mM Fe<sup>2+</sup>, 20 mM Fe<sup>3+</sup>, or 25 mM Cu<sup>2+</sup> with high R<sup>2</sup> value (> 0.999; Table 3.1; Eqs. 3-25 to 3-48). These results indicate that the presence of Fe<sup>2+</sup>, Fe<sup>3+</sup>, or Cu<sup>2+</sup> solely did not affect on the chelating reaction between As and molybdic acid.

However, in the presence of all metal ions (25 mM  $Fe^{2+}$ , 25 mM  $Fe^{3+}$ , and 50 mM  $Cu^{2+}$ ) at the same time (100 mM in total), slight increase in absorbance with time was observed in the case using As(III) standard solution without KMnO<sub>4</sub> (Fig. 3.4a, Table 3.1; Eqs. 3-49 to 3-52). Additionally, obtained slopes of the standard equation (Eqs. 3-49 to 3-52) were 10 times higher than the others (e.g. Eqs. 3-1 to 3-4). Considering the time-course difference of As(V) standard curve was not observed (Fig. 3.4c,d, Table 3.1), it was assumed that small amount of As(III) was gradually oxidized, leading to the increase in the absorbance with time. Large amount of metal ions could change the ionic activity in the solution, possibly accelerating As(III) oxidation coupled with Fe<sup>3+</sup> reduction to  $Fe^{2+}$  (undetectable with the change in  $Fe^{2+}$  concentration due to its small difference). Even though this absorbance increase somewhat overestimate the As(V) concentration (in other words, As(III) is underestimated), the oxidized As(III) concentration was only 4% (roughly calculated by Eqs. 3-1, 3-5, and 3-49). Although it is desirable to remove Fe and Cu from the sample as much as possible, the Cu leaching solution, containing larger amount of Cu and Fe than that of As, is directly applicable to this method if slight oxidation of As(III) is acceptable.

Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

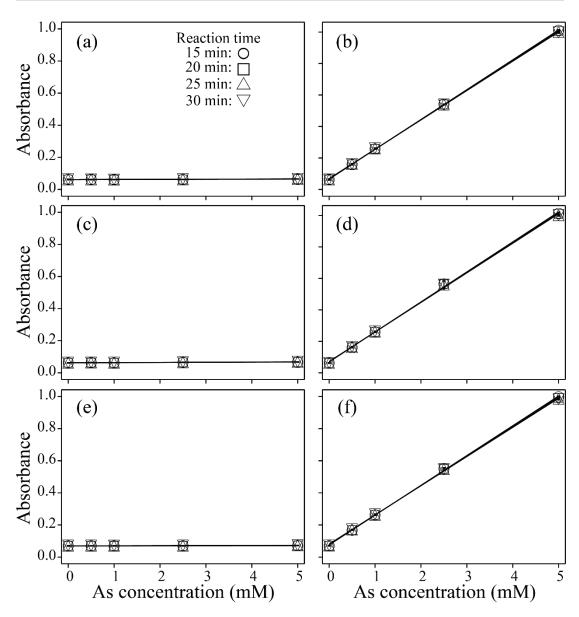


Fig. 3.3 Relationship between absorbance and As concentration with the reaction time of 15 min ( $\bigcirc$ ), 20 min ( $\square$ ), 25 min ( $\triangle$ ), and 30 min ( $\nabla$ ). As(III) standard solution containing 20 mM Fe<sup>2+</sup> (a,b), 20 mM Fe<sup>3+</sup> (c,d), or 25 mM Cu<sup>2+</sup> (e,f) without (a,c,e) and with KMnO<sub>4</sub> (b,d,f) were used for the analysis. Markers, error bars, and standard curves were overlapped due to the high reproducibility.

Chapter 3 Effect of co-existing metals on modified molybdenum blue method for the determination of As concentration in the copper sulfide leachate

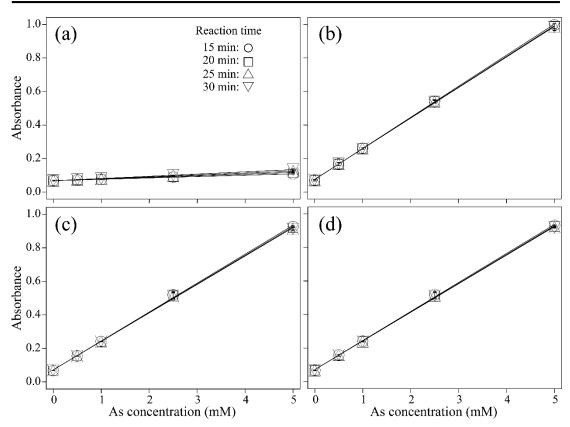


Fig. 3.4 Relationship between absorbance and As concentration with the reaction time of 15 min ( $\bigcirc$ ), 20 min ( $\square$ ), 25 min ( $\triangle$ ), and 30 min ( $\bigtriangledown$ ). As(III) (a,b) and As(V) (c,d) standard solution containing 25 mM Fe<sup>2+</sup>, 25 mM Fe<sup>3+</sup>, and 50 mM Cu<sup>2+</sup> without (a,c) and with KMnO<sub>4</sub> (b,d) were used for the analysis. Markers, error bars, and standard curves were overlapped due to the high reproducibility.

## **3.3.4** As detection in real copper leachate by molybdenum blue method compared with ICP-OES

Arsenic-containing Cu leachate was obtained by bioleaching of enargite concentration to ensure the accuracy of As qualification by modified molybdenum blue method via the comparison with ICP-OES. Fig. 3.5 shows the trends of As concentration leached from enargite during the bioleaching test. The total As concentration determined by modified molybdenum blue method showed a similar trend with that determined by ICP-OES, indicating that the accuracy of the former method is as competitively high as that of the latter. The maximum error in As concentration between two methods was only 0.4 mM, including 0.2 mM of phosphate derived from the ingredient of HBS media (actual error was only 0.2 mM) even though 23 mM of Cu and 80 mM of Fe ions were co-existed. This indicates that the molybdenum blue method is indeed applicable to Cu sulfide leachate with high performance as well as ICP-OES.

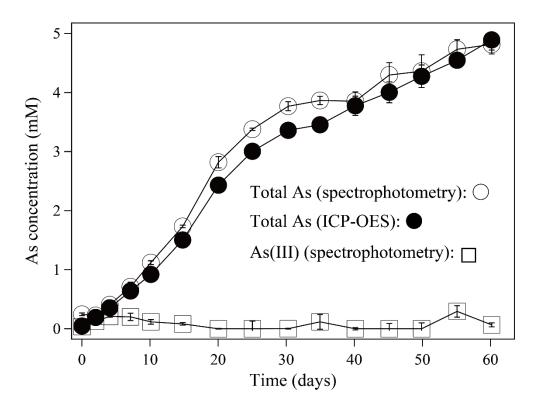


Fig. 3.5 Changes in As(III) ( $\Box$ ) and total As ( $\bigcirc$ ) during bioleaching of enargite concentrate. The concentration was determined by modified molybdenum blue method (open symbol) and ICP-OES (solid symbol).

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## **3.3.5** Summary of the procedure to determine As concentration in Cu sulfide leachate by modified molybdenum blue method

Sample containing negligibly small amount of phosphate should be applied to modified molybdenum blue method with the following procedure;

(i) For As(V) determination, 3  $\mu$ L of the sample solution is mixed with 30  $\mu$ L H<sub>2</sub>SO<sub>4</sub>, 30  $\mu$ L ascorbic acid, 30  $\mu$ L molybdenum-antimony stock solution, and 207  $\mu$ L deionized water to make the mixture up to 300  $\mu$ L.

(ii) For total As determination, 30  $\mu$ L potassium permanganate is further added prior to adding ascorbic acid and the deionized water decreased to 177  $\mu$ L.

(iii) After 15 min of reaction time, absorbance of the solution is read at 880 nm.

Since the difference between (i) and (ii) corresponded to the concentration of As(III), all As species (As(III), As(V) and total As) can be determined in this procedure. If the large amount of Cu and Fe are co-existed, metal-ion removal or sample dilution is recommended to prevent the As(III) oxidation.

It should be noted that if the sample is contaminated with phosphate, step (i) and (ii) determined the concentration of  $As(V) + PO_4$  and total  $As + PO_4$ , respectively. Therefore, the only As(III) concentration is able to be determined by subtracting the value obtained in step (i) from that obtained in step (ii). If the contamination of phosphate is higher than 2.5 mM, the sample must be diluted to be less than 2.5 mM of phosphate concentration.

### **3.4 Conclusions**

The effect of contamination such as Cu, Fe, and phosphate was investigated in the As(III) detection by modified molybdenum blue method. While solo metal contamination (20 mM Fe<sup>2+</sup>, 20 mM Fe<sup>3+</sup>, or 25 mM Cu<sup>2+</sup>) showed no inhibitory effect on As quantification, mixture of Fe<sup>2+</sup>, Fe<sup>3+</sup>, and Cu<sup>2+</sup> (100 mM metals ions in total) led to slight oxidation of As(III) with time, resulting in overestimation of As(V) (underestimation of As(III)). Since the amount of oxidized As(III) was correspond to 4% in 15 min, the sample containing large amount of Fe and Cu ions is directly applicable to this molybdenum blue method if the slight oxidation is acceptable; if not, Cu and Fe must be removed from the sample as much as possible. While phosphate could be inhibitory contamination, <2.5 mM of phosphate is capable of chelating with molybdic acid at the same ratio with arsenate. More phosphate concentration must be, or diluted to be, less than 2.5 mM.

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### **Chapter 4**

### Abstract

Effect of silver (Ag) catalyst in bioleaching of enargite (Cu<sub>3</sub>AsS<sub>4</sub>) concentrate was studied using mixed cultures of moderately thermophilic acidophilic microorganisms at 45°C. Addition of Ag<sub>2</sub>S enabled selective Cu dissolution from enargite while suppressing pyrite oxidation: At the highest Ag<sub>2</sub>S concentration of 0.04%, Cu recovery reached 96% while Fe dissolution was suppressed to reach only 29% by day 72. Overall results from thermodynamic calculation, liquid/solid analyses and kinetic study suggested that Ag-catalyzed bioleaching of enargite concentrate proceeds via formation of at least two types of secondary products (chalcocite, Cu<sub>2</sub>S; trisilver arsenic sulfide, Ag<sub>3</sub>AsS<sub>4</sub>): Addition of Ag<sub>2</sub>S as Ag catalyst thermodynamically and microbiologically contributed to lowering  $E_h$  during bioleaching, consequently satisfying  $E_{ox}$  (Cu<sub>2</sub>S) <  $E_h$  $< E_c$  (Ag<sup>+</sup>) to enhance enargite dissolution via formation of chalcocite intermediate. Formation of trisilver arsenic sulfide and its intermediate layer (Cu,Ag)<sub>3</sub>AsS<sub>4</sub> indicated that Cu ion in the enargite lattice is gradually substituted with Ag. Such secondary products did not impose a rate-limiting step, since the Ag-catalyzed bioleaching was shown to be controlled by a chemical surface reaction, rather than diffusion through product film which was the case in the absence of  $Ag_2S$ .

### 4.1 Introduction

Recent depletion of high-grade copper ores has been directing researchers' attention towards the utilization of low-grade and refractory copper sulfides such as chalcopyrite (CuFeS<sub>2</sub>) and enargite (Cu<sub>3</sub>AsS<sub>4</sub>). In order to improve dissolution efficiency of such minerals, different approaches have been investigated including pressure leaching (Ruiz et al., 2011; Padilla et al., 2015), chemical acid leaching (Safarzadeh and Miller, 2014) and biological leaching (Acevedo et al., 1998; Sasaki et al., 2009). Bioleaching is expected to be one of the most promising approaches in targeting such refractory ores/concentrates, and in fact, high-temperature bioleaching (60-70°C) generally resulted in high copper recoveries (52-91%; Escobar et al., 2000; Muñoz et al., 2006; Lee et al., 2011; Takatsugi et al., 2011; Sasaki et al., 2011). Whilst at low-temperatures (25-30°C), bioleaching still remains to be improved (< 30%; Escobar et al., 1997; Canales et al., 2002; Corkhill et al., 2008; Sasaki et al., 2010). These results suggest that the addition of reaction catalysts would be useful in low-temperature bioleaching to realize better copper recovery.

In the case of chalcopyrite bioleaching, the catalytic effect of different metal ions has been studied so far: Among those metals tested, silver ion was found to be effective in catalyzing chalcopyrite dissolution, whereas cobalt, manganese, antimony, bismuth, nickel and tin ions showed weak or no catalytic ability (Ballesster et al., 1990; Muñoz et al., 2007).

The mechanism of silver-catalyzed chalcopyrite leaching has been explained by different research groups based on abiotic leaching studies, such as via (i) improvement of electrical conductivity by formation of Ag<sub>2</sub>S inside S<sup>0</sup> layer on the chalcopyrite surface (Nazari et al., 2012), (ii) Ag atom diffusion into the metal-deficient sulfur-rich passive layer formed on the chalcopyrite surface (Ghahremaninezhad et al., 2015) and (iii) Ag<sub>2</sub>S formation which rapidly consumes H<sub>2</sub>S produced via intermediate chalcocite (Cu<sub>2</sub>S) formation from chalcopyrite, indirectly accelerating chalcopyrite dissolution (Hiroyoshi et al., 2000, 2001, 2002, 2007, 2008). The third theory was proposed by detailed electrochemical/chemical studies and thermodynamic calculations, revealing the correlation between the silver-catalyzed chalcopyrite dissolution behavior and solution redox potential (*E*<sub>h</sub>). Formation of intermediate Cu<sub>2</sub>S (Eq. 4-3; the sum of Eqs. 4-1 and 4-2) and its oxidation to yield Cu<sup>2+</sup> (Eq. 4-4) proceed simultaneously, when *E*<sub>h</sub>

satisfies the optimal range of  $E_{\rm ox} < E_{\rm h} < E_{\rm c}$ , where,

 $E_{\text{ox}}$  ("oxidation potential"); the equilibrium redox potential for the subsequent oxidation of chalcocite to Cu<sup>2+</sup>

 $E_c$  ("critical potential"); the equilibrium redox potential for the intermediate chalcocite formation from chalcopyrite.

$$2CuFeS_2 + 6H^+ + 2e^- \rightarrow Cu_2S + 2Fe^{2+} + 3H_2S$$
 (Eq. 4-1)

$$2Ag^{+} + H_2S \rightarrow Ag_2S + 2H^{+}$$
 (Eq. 4-2)

$$2CuFeS_2 + 6Ag^+ + 2e^- \rightarrow Cu_2S + 2Fe^{2+} + 3Ag_2S$$
 (Eq. 4-3)

$$Cu_2S \rightarrow 2Cu^{2+} + S^0 + 4e^-$$
 (Eq. 4-4)

As for enargite leaching, studies on the mechanism of silver catalyst is still very limited. An electrochemical study by Miki et al. (2016) suggested that the addition of silver expands the optimal  $E_h$  range, which allows enhanced enargite dissolution. However, the detailed mechanism is yet unclear, and its effect in bioleaching is largely unknown. Although the use of silver catalyst is considered unpractical for copper extraction, clarifying its catalytic mechanism would be beneficial in understanding how enargite leaching can be facilitated.

The objectives of this study were therefore set to evaluate the catalytic effect of silver on bioleaching of enargite concentrate and to elucidate its mechanism.

### 4.2 Materials and methods

# 4.2.1 Silver-catalyzed bioleaching of enargite concentrate using moderately thermophilic microorganisms

The cell of the three bacterial strains, Am. ferrooxidans ICP, Sb. sibiricus N1, At. caldus KU, and one archaeal strain, Fp. acidiphilum Y were pre-grown, as was described in chapter 2. Pre-grown cells were collected by centrifugation (9000 rpm, 10 min at 4°C) and washed twice with acidified water (pH 1.7), prior to inoculation into 200 mL HBS medium (pH 2.0; in 500 mL Erlenmeyer flasks) containing 2% (w/v) enargite concentrate and 5 mM Fe<sup>2+</sup> (so as to set the initial cell density of each strain at  $1.0 \times 10^7$ cells/mL; i.e.  $4.0 \times 10^7$  cells/mL in total). Silver sulfide (Ag<sub>2</sub>S) was added as silver catalyst into the medium at different concentrations: 0, 0.005, 0.01, 0.02, 0.03 and 0.04% (w/v). Flasks were incubated shaken at 45°C and 150 rpm for 72 days. Samples were regularly withdrawn to monitor pH, Eh, cell density and concentrations of Fe<sup>2+</sup> by the *o*-phenanthroline method, total Fe, As and Cu by inductively coupled plasma optical emission spectrometry (ICP-OES; Optima 8300DV; PerkinElmer). Leaching residues were collected after bioleaching and freeze-dried overnight for X-ray diffraction (XRD; Rigaku Ultima IV; CuKa 40 mA, 40 kV) analysis. For quantitative elemental composition analysis by electron probe micro analyzer (EPMA; JOEL JXA-8530F; 6 nA, 20 kV), the leaching residues were embedded into resin and polished. The incident electron beam was focused to 1 µm in diameter, and counting time was set to 20 sec for each element. The acquired results were collected by ZAF method (Boekestein et al., 1983).

# **4.2.2** Analysis of microbial population structure in silver-catalyzed bioleaching of enargite concentrate

In order to investigate the microbial population structure in bioleaching cultures, realtime PCR (MiniOpticon, Bio-Rad) was conducted according to the methods described by Tanaka et al. (2015) with some modifications as follows: The purified genomic DNA from each strain was used as the template to PCR amplify the 16S rRNA gene fragment (~1473 bp) using the universal primer set (27f and 1492r for bacteria or Arch 21f and 1492r for archaea: Table 4.1). The resultant PCR products derived from each strain were purified using ISOSPIN PCR Product (NIPPON GENE), quantified, and finally diluted to give a final concentration of  $1.0 \times 10^3$  to  $1.0 \times 10^9$  copies/µL, to be used as template DNA for real-time PCR. Once linearity in the standard curve was obtained within the range from  $1.0 \times 10^3$  to  $1.0 \times 10^9$  copies/µL for all species, synthetic DNA mixtures (composed of template DNA from each one of the four species at  $1.0 \times 10^3$  to  $1.0 \times 10^9$  copies/µL) was tested against each one of the four species-specific primer sets (Table 4.1) to ensure the accuracy in order to display the results as percentages in whole number. Genomic DNA extracted from the actual bioleaching mixed cultures were tested against the corresponding species-specific primer sets.

	PCR product size (bp)	1472	C/+I~	1451	1401	737	707	140	147	731	107	103	0/1
udy.	Target species PCR	Dootonio	DACICILA	A ******	AULIACA	Species-specific:	Am. ferrooxidans	Species-specific:	Sb. sibiricus	Species-specific:	At. caldus	Species-specific:	Fp. acidiphilum
Table 4.1 PCR and Real-Time PCR primer sets used in this study.	Primer sequence (5'-3')	AGAGTTTGATCMTGGCTCAG	TACGGYTACCTTGTTACGACTT	TTCCGGTTGATCCYGCCGGA		TCATTCGACGGGCTCCGTG	GAGCTGACGACARCCATGCA	TAGGTGTCGCCCGGGTCCAC	1	TAGGTGCTGAGTGTCGTAGCTAACG	1	GAAGCTTAACTCCAGAAAGTCTGAAGAGA	GGACTACCCGGGTATCTAATCCGGT
Та	Primer set	27f Universal	1492r Universal	Arch 21f	1492r Universal	Amferro-F1	Buniv-R1	Sbsib-F1	Buniv-R1	Acaldus-F3	Buniv-R1	Fpacidi-F2	Fpacidi-R1
	Purpose		משמ	ICN					Real-Time	PCR			

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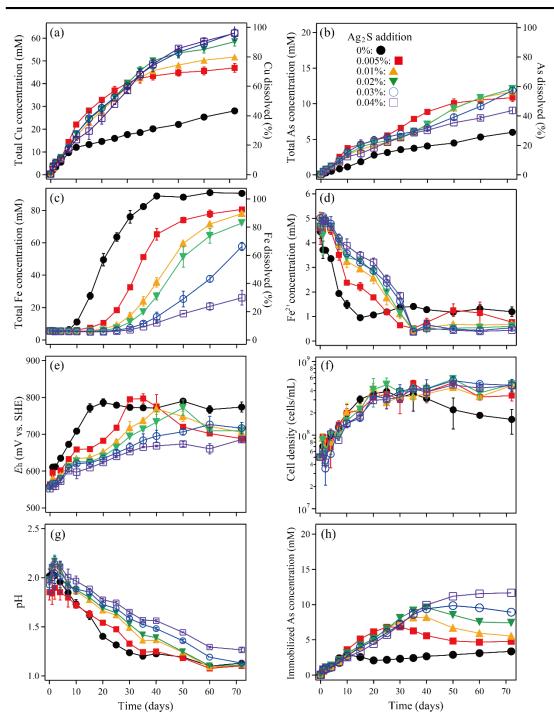
### 4.3 Results and discussion

# 4.3.1 Dissolution behavior of Cu, Fe, and As during bioleaching with and without Ag<sub>2</sub>S

In the absence of Ag<sub>2</sub>S, Cu recovery was 43% on day 72 (Fig. 4.1a), while Fe started to dissolve mainly from pyrite on day 10 to a rapid completion (100%) by day 40 (Fig. 4.1c), accompanied by the stably high  $E_h$  at around 770 mV (Fig. 4.1e). This high redox condition supported pyrite dissolution, whereas enargite oxidation was hindered due to the formation of the passivation layer such as jarosite (Muñoz et al., 2006; Takatsugi et al., 2011). Increasing addition of Ag<sub>2</sub>S (0.005–0.04%) led to consecutively greater Cu recoveries (Fig. 4.1a) and lower Fe dissolutions (Fig. 4.1c), with Fe<sup>2+</sup> oxidation seemingly being increasingly delayed (Fig. 4.1d) and thus  $E_{\rm h}$  values being increasingly suppressed (Fig. 4.1e). The results thus indicate that Ag<sub>2</sub>S addition improves Cu recovery by enabling selective Cu dissolution from enargite concentrate. Selective suppression of pyrite dissolution has also been reported in Ag-catalyzed chalcopyrite bioleaching studies (Ahonen and Tuovinen, 1990; Ballester et al., 1990). As for cell growth, active cell growth was seen despite the presence of the antibacterial effect of Ag<sup>+</sup> (Marambio-Jones and Hoek, 2010). Rather, the addition of Ag<sub>2</sub>S was found effective in maintaining high cell densities, which otherwise decreased towards the end of the stationary phase (Fig. 4.1f). At the highest  $Ag_2S$  concentration of 0.04%, Cu recovery reached 96% (Fig. 4.1a), while Fe dissolution was suppressed to reach only 29% by day 72 (Fig. 4.1c). Under this condition, 56% of dissolved As was calculated to be re-immobilized during bioleaching by day 72, compared with 36% As reimmobilization observed in the absence of Ag<sub>2</sub>S (Fig. 4.1b, h) (calculated based on the theoretical amount of As solubilized from enargite at the ratio of Cu:As=3:1).

XRD analysis of the original enargite concentrate (Fig. 4.2a) and bioleached residues (Fig. 4.2b–g) indeed showed the trend that enargite peaks selectively and progressively diminished, while leaving pyrite peaks increasingly unchanged at higher Ag<sub>2</sub>S concentrations. Jarosite (KFe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub>) peaks were found after bioleaching only in the absence of Ag<sub>2</sub>S (Fig. 4.2b), where pyrite was selectively and completely dissolved by day 40 (Fig. 4.1c). During bioleaching, fine red precipitates floating on the bioleaching liquors became increasingly visible at higher Ag<sub>2</sub>S concentrations. Although no XRD peaks attributing As secondary minerals were detected when bulk

bioleached residue samples were analyzed (Fig. 4.2), selective recovery of the red precipitates enabled their identification by XRD as trisilver arsenic sulfide (Ag<sub>3</sub>AsS<sub>4</sub>) (Fig. 4.3).



Chapter 4 Evaluating catalytic ability of silver in bioleaching of enargite concentrate and elucidating its catalytic mechanism

Fig. 4.1 Changes in the total soluble Cu concentration (a), total soluble As concentration (b), total soluble Fe concentration (c),  $Fe^{2+}$  concentration (d),  $E_h$  (e), cell density (f), pH (g), and immobilized As concentration (h) during bioleaching of enargite concentrate at 0% ( $\bigcirc$ ), 0.005% ( $\blacksquare$ ), 0.01% ( $\blacktriangle$ ), 0.02% ( $\checkmark$ ), 0.03% ( $\bigcirc$ ) or 0.04% ( $\Box$ ) of Ag<sub>2</sub>S. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

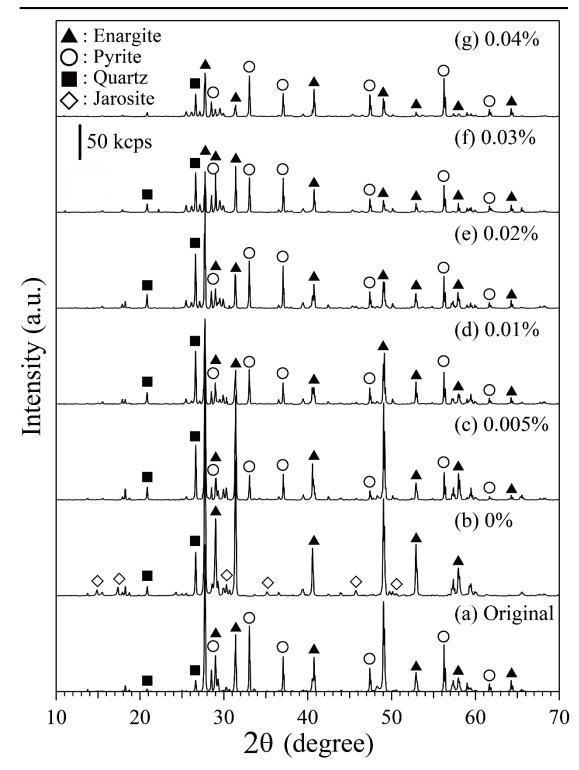


Fig. 4.2 X-ray diffraction patterns of original enargite concentrate (a) and bioleached residues (b-g) recovered on day 72 from cultures containing 0% (b), 0.005% (c), 0.01% (d), 0.02% (e), 0.03% (f) or 0.04% (g) of Ag<sub>2</sub>S.  $\blacktriangle$ : enargite (Cu<sub>3</sub>AsS<sub>4</sub>; PDF No. 00-035-0775),  $\bigcirc$ : pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340),  $\blacksquare$ : quartz (SiO<sub>2</sub>; PDF No. 01-070-3755),  $\diamondsuit$ : jarosite (K(Fe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub>); PDF No. 01-076-0629).

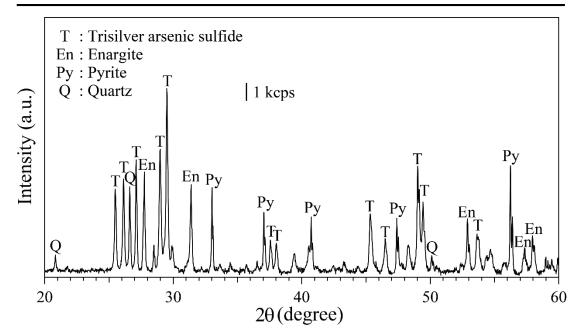


Fig. 4.3 X-ray diffraction patterns of red precipitates selectively collected from the bioleaching culture containing 0.04% Ag<sub>2</sub>S. T: trisilver arsenic sulfide (Ag<sub>3</sub>AsS<sub>4</sub>; PDF No. 01-089-1370), En: enargite (Cu<sub>3</sub>AsS<sub>4</sub>; PDF No. 00-035-0775), Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>; PDF No. 01-070-3755).

### 4.3.2 Suppression of pyrite dissolution by Ag<sub>2</sub>S

The effect of Ag<sub>2</sub>S in selective suppression of pyrite dissolution can be attributed to the following reasons; (i) the change in microbial population structure due to inhibitory effect of Cu<sup>2+</sup> and/or antibacterial Ag<sup>+</sup> ions, causing the low solution redox condition, (ii) the difference in rest potentials of co-existing minerals (enargite, pyrite and Ag<sub>2</sub>S) displaying different subjectivity to the oxidation. As for (i), the real-time PCR analysis found that Fe-oxidizing *Am. ferrooxidans* ICP was the dominant species in the absence of Ag<sub>2</sub>S (97–75% on day 15–30, Fig. 4.4). However, the addition of 0.04% Ag<sub>2</sub>S decreased its abundance to 57–31% whereas S-oxidizing *At. caldus* KU became the dominant species by increasing its ratio from 1–5% (0% Ag<sub>2</sub>S) to 42–53% (0.04% Ag<sub>2</sub>S) (on day 15–30; Fig. 4.4). The lower tolerance of *Am. ferrooxidans* ICP (9 mM) than *At. caldus* KU (24 mM) to Cu<sup>2+</sup> (Watkin et al., 2009) may be responsible for this observation, as Cu dissolution advanced steadily to reach 19–37mM on day 15–30 when 0.04% Ag<sub>2</sub>S was added (in contrast to 13–18mM at 0% Ag<sub>2</sub>S; Fig. 4.1a). The abundance of *Sb. sibiricus* N1 became noticeable at the later stage of bioleaching both at 0% and 0.04% Ag<sub>2</sub>S (Fig. 4.4), probably resulting from its extremely high tolerance

to  $Cu^{2+}$  (299 mM) and As (V) (100 mM) (Watling et al., 2008). The population of Fp. acidiphilum Y did not emerge throughout the experiment in both cases, probably due to its sensitivity to the temperature condition used here (Golyshina et al., 2000). There may also have been an antibacterial effect of Ag<sup>+</sup> to the microbes used, but their individual sensitivity to Ag<sup>+</sup> is unclear. This difference in microbial population structure resulted in deterioration of microbial  $Fe^{2+}$  oxidation in the presence of Ag<sub>2</sub>S, which may have partly caused the apparent delay of pyrite oxidation (Fig. 4.1c) and the suppression of  $E_{\rm h}$  values (Fig. 4.1e). As for (ii), rest potentials of the minerals were reported to be as follows: 164 mV vs. SCE (408 mV vs. SHE) for enargite, 398 mV vs. SCE (642 mV vs. SHE) for pyrite (Rivera-Vasquez and Dixon, 2015) and 280 mV (vs. SHE) for Ag<sub>2</sub>S (Majima, 1969). Therefore, consumption of the oxidant,  $Fe^{3+}$ , may have been more readily directed towards oxidation of Ag<sub>2</sub>S to release Ag<sup>+</sup> ions, rather than to oxidation of pyrite. Due to the low solubility product of Ag<sub>2</sub>S (Goates et al., 1951; Hseu and Rechnitz, 1968), solubilized Ag<sup>+</sup> ions would have been immediately transformed back to Ag<sub>2</sub>S, which is then re-oxidized by Fe<sup>3+</sup>. This continuous Ag<sub>2</sub>Soxidation coupled with Fe<sup>3+</sup>-reduction may have caused the apparent lag-time of Fe<sup>2+</sup> oxidation (Fig. 4.1d) and the suppression of  $E_h$  values (Fig. 4.1e). Since pyrite bioleaching favors high  $E_{\rm h}$  conditions, the above effects would likely have contributed to the suppression of pyrite bioleaching.

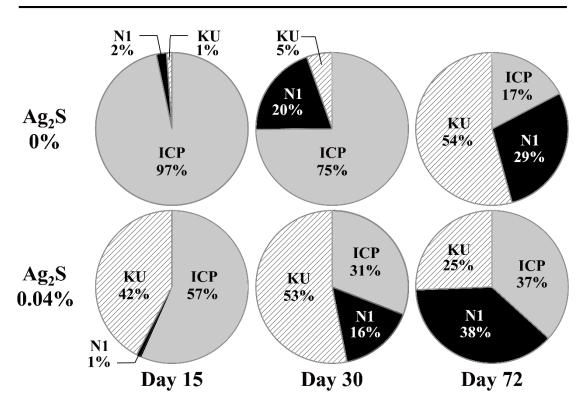


Fig. 4.4 Microbial population structure on day 15, 30, and 72 in bioleaching cultures of enargite concentrate at 0% and 0.04% of Ag<sub>2</sub>S. N1, ICP, and KU indicate *Am. ferrooxidans* ICP, *Sb. sibiricus* N1, and *At. caldus* KU, respectively.

#### 4.3.3 Promotion of enargite dissolution by Ag<sub>2</sub>S

The theory of Ag-catalyzed chalcopyrite leaching (Hiroyoshi et al., 2002) was applied to that of Ag-catalyzed electrochemical enargite leaching by Miki et al. (2016), suggesting the existence of the optimal  $E_h$  range for enhanced enargite dissolution as follows: In the absence of Ag, when  $E_h$  is within the optimal range, enargite dissolution proceeds via formation of intermediate Cu<sub>2</sub>S (Eq. 4-5) and H<sub>2</sub>S generated by Eq. 4-5 is consumed by Cu<sup>2+</sup> to form Cu<sub>2</sub>S (Eq. 4-6). The overall reaction of Eqs. 4-5 and 4-6 can be summarized as Eq. 4-7, and the resultant Cu<sub>2</sub>S is amenable to oxidation to produce Cu<sup>2+</sup> (Eq. 4-8). However, this optimal range is narrow and exists at the relatively lower redox potential level (0.501–0.503 V; Miki et al., 2016), implying that Eqs. 4-7 and 4-8 hardly occur simultaneously in general bioleaching cultures. If Ag is present, however, H<sub>2</sub>S generated by Eq. 4-5 is immediately removed by Ag<sup>+</sup> to form Ag<sub>2</sub>S (Eq. 4-9) to result in Eq. 4-10 (the sum of Eq. 4-5 and Eq. 4-9), leading to the expansion of the optimal  $E_h$  range (0.501–1.020V in the presence of 10<sup>-5</sup> M Ag<sup>+</sup>, Miki et al., 2016).

$$2Cu_{3}AsS_{4} + 6H_{2}O + 4H^{+} + 4e^{-} \rightarrow 3Cu_{2}S + 5H_{2}S + 2H_{3}AsO_{3}$$
 (Eq. 4-5)

$$2Cu^{2+} + H_2S + 2e^- \rightarrow Cu_2S + 2H^+$$
 (Eq. 4-6)

$$2Cu_{3}AsS_{4} + 6H_{2}O + 10Cu^{2+} + 14e^{-} \rightarrow 8Cu_{2}S + 2H_{3}AsO_{3} + 6H^{+}$$
(Eq. 4-7)

$$Cu_2S \rightarrow 2Cu^{2+} + S^0 + 4e^-$$
 (Eq. 4-8)

$$2Ag^{+} + H_2S \rightarrow Ag_2S + 2H^{+}$$
 (Eq. 4-9)

$$2Cu_{3}AsS_{4} + 6H_{2}O + 10Ag^{+} + 4e^{-} \rightarrow 3Cu_{2}S + 5Ag_{2}S + 2H_{3}AsO_{3} + 6H^{+}$$
(Eq. 4-10)

The optimal  $E_h$  ranges in the absence and presence of Ag are expressed as Eqs. 4-11 and 4-12, respectively.

$$E_{\rm ox}({\rm Cu}_2{\rm S}) < E_{\rm h} < E_{\rm c}({\rm Cu}^{2+})$$
 (Eq. 4-11)

$$E_{\rm ox}({\rm Cu}_2{\rm S}) < E_{\rm h} < E_{\rm c}({\rm Ag}^+)$$
 (Eq. 4-12)

 $E_{\rm c}({\rm Cu}^{2+})$  and  $E_{\rm c}({\rm Ag}^+)$  ("critical potential"): the equilibrium redox potential for the intermediate Cu<sub>2</sub>S formation from enargite in the absence (Eq. 4-7) and presence (Eq. 4-10) of Ag, respectively.

 $E_{\text{ox}}(\text{Cu}_2\text{S})$  ("oxidation potential"): the equilibrium redox potential for the subsequent oxidation of Cu<sub>2</sub>S to Cu<sup>2+</sup> (Eq. 4-8).

 $E_{\rm c}({\rm Cu}^{2+})$ ,  $E_{\rm c}({\rm Ag}^+)$  and  $E_{\rm ox}({\rm Cu}_2{\rm S})$  were calculated by using Eq. 4-13, 4-14 and 4-15, respectively:

$$E_{\rm c}({\rm Cu}^{2+}) = E_{\rm c}^{0}({\rm Cu}^{2+}) + \frac{RT}{14F} \ln \frac{(\alpha_{Cu^{2+}})^{10}}{(\alpha_{H_3ASO_3})^2(\alpha_{H^+})^6}$$
(Eq. 4-13)

$$E_{\rm c}({\rm Ag}^{+}) = E_{\rm c}^{0}({\rm Ag}^{+}) + \frac{RT}{4F} \ln \frac{\left(\alpha_{Ag^{+}}\right)^{10}}{\left(\alpha_{H_{3}AsO_{3}}\right)^{2}\left(\alpha_{H^{+}}\right)^{6}}$$
(Eq. 4-14)

$$E_{\rm ox}({\rm Cu}_2{\rm S}) = E_{\rm ox}^0({\rm Cu}_2{\rm S}) + \frac{RT}{4F} \ln (\alpha_{Cu^{2+}})^2$$
(Eq. 4-15)

R, T, F, and  $\alpha_i$  are gas constant (J/Kmol), temperature (K), Faraday constant (C/mol), and activities of species i, respectively.

Here,  $E_c^0(Cu^{2+})$ ,  $E_c^0(Ag^+)$  and  $E_{ox}^0(Cu_2S)$  indicate the standard redox potentials (V) of Eq. 4-7, 4-10 and 4-8 calculated by Eq. 4-16, 4-17 and 4-18, respectively:

$$E_{c}^{0}(Cu^{2+}) = -\frac{1}{14F}(8\Delta G_{Cu_{2}S}^{0} + 2\Delta G_{H_{3}ASO_{3}}^{0} + 6\Delta G_{H^{+}}^{0} - 2\Delta G_{Cu_{3}ASS_{4}}^{0} - 6\Delta G_{H_{2}O}^{0} - 10\Delta G_{Cu^{2+}}^{0})$$
(Eq. 4-16)

$$E_{c}^{0}(Ag^{+}) = -\frac{1}{4F}(3\Delta G_{Cu_{2}S}^{0} + 5\Delta G_{Ag_{2}S}^{0} + 2\Delta G_{H_{3}ASO_{3}}^{0} + 6\Delta G_{H^{+}}^{0} - 2\Delta G_{Cu_{3}ASS_{4}}^{0} - 6\Delta G_{H_{2}O}^{0} - 10\Delta G_{Ag^{+}}^{0})$$
(Eq. 4-17)

$$E_{\rm ox}^{0}({\rm Cu}_{2}{\rm S}) = -\frac{1}{4F} (\Delta G_{Cu_{2}S}^{0} - 2\Delta G_{Cu^{2+}}^{0} - \Delta G_{S^{0}}^{0})$$
(Eq. 4-18)

 $\Delta G_i^0$  indicates the standard Gibbs free energy of species i and those used for calculation are listed in Table 4.2. The values of  $E_c^0(Cu^{2+})$ ,  $E_c^0(Ag^+)$ , and  $E_{ox}^0(Cu_2S)$  were thus calculated to be 0.628, 1.867, and 0.561 V, respectively.

Since Ag concentrations in leachates were below the detection limit of ICP-OES, they were thermodynamically calculated as follows and listed in Tables 4.3 and 4.4. Dissolution of  $Ag_2S$  in bioleaching culture (Eq. 4-19) and the equilibrium potential of Eq. 4-19 (Eq. 4-20) are expressed as below (Miki et al., 2016):

$$Ag_2S \rightarrow 2Ag^+ + S^0 + 2e^-$$
 (Eq. 4-19)

$$E_{ox}(Ag_2S) = E_{ox}^0(Ag_2S) + \frac{RT}{F}\ln(\alpha_{Ag^+})$$
(Eq. 4-20)

 $E_{\text{ox}}(\text{Ag}_2\text{S})$  ("oxidation potential") indicates the equilibrium redox potential for oxidation of Ag<sub>2</sub>S to Ag<sup>+</sup> (Eq. 4-19).

 $E_{\text{ox}}^{0}(\text{Ag}_2\text{S})$  indicates the standard redox potential of Eq. 4-19, as calculated by Eq. 4-21.

$$E_{0x}^{0}(Ag_{2}S) = -\frac{1}{2F} (\Delta G_{Ag_{2}S}^{0} - 2\Delta G_{Ag^{+}}^{0} - \Delta G_{S^{0}}^{0})$$
(Eq. 4-21)

Based on Eq. 4-20, when the activity coefficient is defined as 1, the Ag concentration was calculated by the function of  $E_{ox}(Ag_2S)$  as shown in Fig. 4.5.

In order to estimate whether or not the above Cu<sub>2</sub>S intermediate reaction contributed to enargite bioleaching in this study, actual measured values were evaluated if they satisfy Eq. 4-11 and/or Eq. 4-12. Actual As(III) concentrations were not measured in this study. Therefore, calculations for  $E_c(Cu^{2+})$ ,  $E_c(Ag^+)$  and  $E_{ox}(Cu_2S)$  values were conducted based on both assumptions that (i) total As concentrations equal to As(III) concentrations (Table 4.3) and (ii) As(III) concentrations are negligible (10<sup>-5</sup> M) (Table 4.4), in order to ensure that the results are similar in both cases. Copper extraction rates and  $E_{have}$  values were calculated using Eqs. 4-13 and 4-14, respectively, and listed in Tables 4.3 and 4.4.

Cu extraction rate = 
$$(X_n - X_{n-1}) / (t_n - t_{n-1})$$
 (Fig. 4-13)

$$E_{\text{have}} = (E_{\text{hn}} + E_{\text{hn-1}}) / 2$$
 (Fig. 4-14)

t<sub>n</sub>: the sampling time (day)

X<sub>n</sub>: total dissolved Cu concentration on day t<sub>n</sub> (M)

 $E_{hn}$ :  $E_h$  value on day  $t_n$  (V vs. SHE)

The calculated  $E_c(Cu^{2+})$  values in all cultures were 0.588–0.607 V and 0.607–0.633 V as shown in Tables 4.3 and 4.4, respectively. These values were only about maximum of 0.1 V higher than the  $E_{ox}(Cu_2S)$  values (0.501–0.524 V; Tables 4.3 and 4.4).

Measured  $E_{\text{have}}$  values could hardly locate within this < 0.1 V-wide optimal range, indicating that enargite dissolution was hardly contributed by the Cu<sub>2</sub>S intermediate reaction in the absence of Ag.

In the presence of Ag, this optimal range was greatly expanded due to the higher redox potential of  $E_c(Ag^+)$ : 1.044–1.500 V and 1.120–1.590 V (Tables 4.3 and 4.4, respectively). The correlation between  $E_{have}$  values and Cu extraction rates was plotted in Fig. 4.6, by employing the maximum  $E_{ox}(Cu_2S)$  value of 0.524 V and the minimum value of  $E_c(Ag^+)$  (1.044 V) as the strictest evaluation (Tables 4.3 and 4.4). All plots were within the optimal range satisfying  $E_{ox}(Cu_2S) < E_h < E_c(Ag^+)$  (Eq. 4-12), with generally higher Cu extraction rates at elevated Ag<sub>2</sub>S concentrations (Fig. 4.6). The results suggest that the Cu<sub>2</sub>S intermediate reaction was involved in enargite bioleaching in the presence of Ag<sub>2</sub>S.

Table 4.2 Standard Gibbs free energy of each species used for thermodynamic calculation in Tables 4.3 and 4.4 (Padilla et al. (2013); Outokumpu (HSC Chemistry 5 software)).

species	$Cu_3AsS_4$	$Cu_2S$	Cu <sup>2+</sup>	H <sub>3</sub> AsO <sub>3</sub>	$Ag_2S$	$\mathrm{Ag}^{+}$	$H_2S$	$H_2O$	$\mathrm{H}^{+}$
$\Delta  G_{i}^{\ 0}$	-178.9	-86.7	65.1	-632.6	-40.9	75.2	-34.2	-233.9	0.0

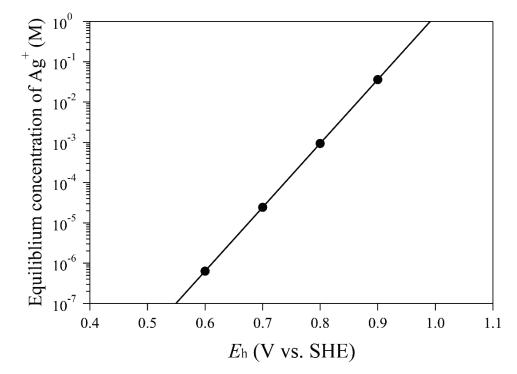


Fig. 4.5 Relationship between solution redox potential ( $E_h$ ) and thermodynamically calculated equilibrium concentration of Ag<sup>+</sup>.

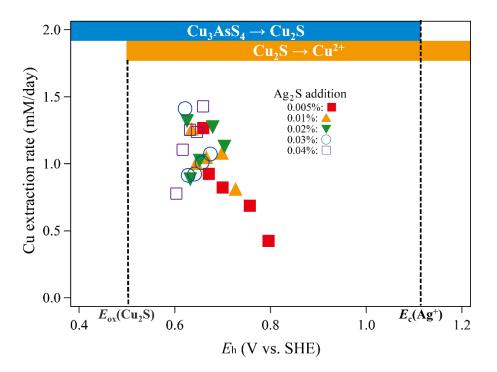


Fig. 4.6 Relationship between the Cu leaching rate and  $E_h$  value in bioleaching of enargite concentrate at 0.005% ( $\blacksquare$ ), 0.01% ( $\triangle$ ), 0.02% ( $\bigtriangledown$ ), 0.03% ( $\bigcirc$ ), and 0.04% ( $\Box$ ) of Ag<sub>2</sub>S. Data sets obtained from day 15 to 35 were employed.

$Ag_2S$	Day	Hq	[H <sup>+</sup> ] (M)	$[H_3AsO_3]$ (M)	[Ag <sup>+</sup> ] (M)	[Cu <sup>2+</sup> ] (M)	Cu extraction rate (M/day)	Eh (V)	Eh <sub>ave</sub> (V)	$E_c(Cu^{2+})$ (V)	$E_{c}(Ag^{+})\;(V)$	$E_{ox}(Cu_2S)$ (V)
	10	1.733	0.177	$1.123  imes 10^3$		$12.02 \times 10^{-3}$	$0.733 imes 10^3$	0.709	0.691	0.588		0.501
	15	1.618	0.198	$1.850\times 10^3$		$13.27 imes10^3$	$0.257 imes 10^3$	0.772	0.740	0.587		0.502
	20	1.403	0.246	$2.781  imes 10^3$	·	$14.62\times 10^3$	$0.267 imes 10^3$	0.786	0.779	0.585		0.504
	25	1.316	0.268	$3.144 \times 10^3$		$15.97  imes 10^3$	$0.270  imes 10^3$	0.779	0.783	0.585		0.505
òò	30	1.238	0.290	$3.552 imes 10^3$		$17.65  imes 10^3$	$0.345 imes 10^3$	0.773	0.776	0.585	,	0.506
%0	35	1.202	0.301	$3.738\times 10^3$		$18.52\times 10^3$	$0.179 imes 10^3$	0.772	0.772	0.586		0.507
	40	1.226	0.294	$4.055 imes 10^3$		$20.17  imes 10^3$	$0.331  imes 10^3$	0.771	0.772	0.587		0.508
	50	1.192	0.304	$4.476  imes 10^3$	ı	$22.10\times 10^3$	$0.189 imes 10^3$	0.790	0.781	0.588		0.509
	60	1.101	0.333	$5.319 imes10^3$		$25.34\times10^3$	$0.330  imes 10^3$	0.767	0.778	0.589		0.511
	72	1.130	0.323	$5.983 imes10^3$		$28.07 \times 10^3$	$0.227 imes 10^3$	0.774	0.770	0.591		0.513
	10	1.721	0.179	$3.771 imes10^3$	$0.545  imes 10^{-5}$	$22.09 \times 10^3$	$2.409  imes 10^3$	0.659	0.646	0.595	1.183	0.509
	15	1.631	0.196	$4.288 \times 10^3$	$0.563  imes 10^{-5}$	$28.23\times 10^3$	$1.265 imes 10^3$	0.660	0.659	0.598	1.180	0.513
	20	1.541	0.214	$4.820 imes 10^3$	$1.285  imes 10^{-5}$	$32.89  imes 10^3$	$0.925  imes 10^3$	0.682	0.671	0.600	1.231	0.515
	25	1.475	0.229	$5.560 imes10^3$	$4.668\times10^{-5}$	$37.02  imes 10^3$	$0.823 imes 10^3$	0.718	0.700	0.601	1.315	0.517
0.0050/	30	1.329	0.265	$6.609 imes10^3$	$78.67  imes 10^{-5}$	$40.36\times10^3$	$0.688  imes 10^3$	0.795	0.757	0.600	1.500	0.518
% con.r	35	1.243	0.289	$7.858  imes 10^3$	$84.32\times10^{-5}$	$42.44\times10^3$	$0.425 imes 10^3$	0.797	0.796	0.600	1.499	0.518
	40	1.249	0.287	$8.867 imes10^{-3}$	$38.13\times10^{-5}$	$43.40\times10^3$	$0.193 imes 10^3$	0.775	0.786	0.600	1.443	0.519
	50	1.183	0.307	$10.10 imes10^3$	$5.040  imes 10^{-5}$	$44.84\times10^3$	$0.142 imes 10^3$	0.720	0.748	0.599	1.300	0.519
	09	1.077	0.341	$10.52 imes10^3$	$2.632\times10^{-5}$	$45.59\times10^3$	$0.076 imes 10^3$	0.702	0.711	0.598	1.251	0.519
	72	1.103	0.332	$10.85 imes 10^3$	$1.585\times10^{-5}$	$46.95 \times 10^3$	$0.113 imes 10^3$	0.688	0.695	0.599	1.217	0.520
	10	1.863	0.155	$2.820 imes 10^{-3}$	$0.214\times10^{-5}$	$16.90  imes 10^3$	$1.767 imes10^3$	0.633	0.624	0.593	1.129	0.506
	15	1.771	0.170	$3.590 imes 10^3$	$0.246\times10^{-5}$	$23.02\times 10^3$	$1.261 imes 10^3$	0.637	0.635	0.597	1.132	0.510
	20	1.664	0.189	$4.137 \times 10^3$	$0.424\times10^{-5}$	$28.09\times 10^3$	$1.005 imes 10^3$	0.652	0.645	0.599	1.163	0.513
	25	1.618	0.198	$4.578  imes 10^3$	$1.154  imes 10^{-5}$	$33.36  imes 10^3$	$1.049 imes 10^3$	0.680	0.666	0.601	1.228	0.515
0.010/0	30	1.490	0.225	$5.182 imes 10^3$	$4.584\times10^{-5}$	$38.61\times 10^3$	$1.082 imes 10^3$	0.717	0.698	0.602	1.315	0.517
% TO O	35	1.360	0.257	$6.025 imes 10^3$	$9.287  imes 10^{-5}$	$42.57  imes 10^3$	$0.812\times 10^3$	0.737	0.727	0.602	1.356	0.518
	40	1.363	0.256	$7.024  imes 10^3$	$29.64\times10^{-5}$	$45.73\times10^3$	$0.634 imes 10^3$	0.768	0.753	0.603	1.434	0.519
	50	1.239	0.290	$9.379 imes10^3$	$14.18\times10^{-5}$	$48.23\times10^3$	$0.246 imes 10^3$	0.748	0.758	0.601	1.374	0.520
	09	1.087	0.337	$10.832 imes 10^3$	$5.392  imes 10^{-5}$	$50.33 imes10^3$	$0.214 imes 10^3$	0.722	0.735	0.600	1.300	0.521

A523	Day	Hq	(H <sup>+</sup> ] (M)	$[H_3AsO_3]$ (M)	$[Ag^{+}](M)$	[Cu <sup>2+</sup> ] (M)	Cu extraction rate (M/day)	Eh (V)	$Eh_{ave}\left(V ight)$	$E_{c}(Cu^{2+})$ (V)	$E_{c}(Ag^{+})(V)$	$E_{ox}(Cu_2S)$ (V)
	10	1.877	0.153	$2.908  imes 10^3$	$0.166  imes 10^{-5}$	$18.00  imes 10^3$	$1.877 imes10^3$	0.626	0.619	0.594	1.112	0.507
	15	1.799	0.166	$3.933  imes 10^3$	$0.156\times 10^{-5}$	$24.40  imes 10^{-3}$	$1.318  imes 10^3$	0.625	0.626	0.598	1.100	0.511
	20	1.692	0.184	$4.477  imes 10^3$	$0.271 \times 10^{-5}$	$28.85\times 10^{-3}$	$0.883  imes 10^3$	0.640	0.632	0.599	1.132	0.513
	25	1.642	0.194	$4.809 imes 10^3$	$0.653\times 10^{-5}$	$33.99  imes 10^3$	$1.023  imes 10^3$	0.664	0.652	0.602	1.189	0.515
	30	1.528	0.217	$5.287 imes 10^3$	$1.966\times 10^{-5}$	$40.17  imes 10^3$	$1.273  imes 10^3$	0.694	0.679	0.603	1.259	0.518
0.02%	35	1.417	0.243	$6.083  imes 10^3$	$3.976  imes 10^{-5}$	$45.66  imes 10^{-3}$	$1.127 imes10^3$	0.713	0.704	0.604	1.301	0.519
	40	1.390	0.249	$7.092  imes 10^3$	$8.129\times 10^{-5}$	$50.01  imes 10^3$	$0.874 imes10^3$	0.733	0.723	0.605	1.346	0.521
	50	1.247	0.287	$9.317 imes 10^3$	$33.56\times10^{-5}$	$53.52  imes 10^3$	$0.344  imes 10^3$	0.772	0.752	0.603	1.434	0.522
	60	1.104	0.332	$10.82 imes 10^3$	$3.448\times 10^{-5}$	$55.10\times 10^3$	$0.161  imes 10^3$	0.710	0.741	0.602	1.270	0.522
	72	1.105	0.331	$12.10\times 10^{-3}$	$3.436  imes 10^{-5}$	$58.49  imes 10^3$	$0.282 imes10^3$	0.709	0.709	0.602	1.268	0.523
	10	1.885	0.152	$3.241 \times 10^3$	$0.134 \times 10^{-5}$	$17.88  imes 10^{-3}$	$1.973  imes 10^3$	0.620	0.614	0.594	1.096	0.507
	15	1.854	0.157	$4.278 \times 10^3$	$0.143 \times 10^{-5}$	$24.73  imes 10^{-3}$	$1.412  imes 10^3$	0.622	0.621	0.598	1.095	0.511
	20	1.726	0.178	$4.861\times 10^3$	$0.217  imes 10^{-5}$	$29.34  imes 10^{-3}$	$0.914  imes 10^3$	0.634	0.628	0.600	1.117	0.513
	25	1.687	0.185	$5.318 imes10^3$	$0.385 \times 10^{-5}$	$33.97  imes 10^{-3}$	$0.923  imes 10^3$	0.649	0.642	0.602	1.154	0.515
0.02.07	30	1.585	0.205	$5.738  imes 10^3$	$0.677 imes 10^{-5}$	$38.87  imes 10^{-3}$	$1.009  imes 10^3$	0.665	0.657	0.603	1.187	0.517
% cn.n	35	1.525	0.218	$6.106  imes 10^3$	$1.333 \times 10^{-5}$	$44.10\times10^{-3}$	$1.073  imes 10^3$	0.683	0.674	0.605	1.230	0.519
	40	1.482	0.227	$6.594  imes 10^3$	$2.039 imes 10^{-5}$	$48.02\times10^{-3}$	$0.788  imes 10^3$	0.695	0.689	0.605	1.256	0.520
	50	1.358	0.257	$8.100\times 10^3$	$3.119\times 10^{-5}$	$53.86\times10^{-3}$	$0.573  imes 10^3$	0.707	0.701	0.605	1.278	0.522
	60	1.192	0.304	$9.642  imes 10^3$	$6.389 \times 10^{-5}$	$57.55 imes 10^3$	$0.376  imes 10^3$	0.726	0.717	0.604	1.317	0.523
	72	1.131	0.323	$11.86\times 10^3$	$4.460\times10^{-5}$	$62.37  imes 10^{-3}$	$0.402  imes 10^3$	0.717	0.721	0.604	1.288	0.524
	10	1.967	0.140	$2.571 imes10^3$	$0.057 imes 10^{-5}$	$15.39  imes 10^3$	$1.336  imes 10^3$	0.597	0.599	0.593	1.044	0.504
	15	1.887	0.152	$3.024  imes 10^3$	$0.089 imes 10^{-5}$	$19.16\times 10^{-3}$	$0.777 imes 10^3$	0.609	0.603	0.595	1.069	0.507
	20	1.777	0.169	$3.799  imes 10^3$	$0.148\times 10^{-5}$	$24.74  imes 10^{-3}$	$1.106  imes 10^3$	0.623	0.616	0.598	1.096	0.511
	25	1.745	0.175	$4.602  imes 10^3$	$0.271  imes 10^{-5}$	$31.03 imes10^{-3}$	$1.254  imes 10^3$	0.640	0.631	0.601	1.134	0.514
/010/0	30	1.650	0.192	$5.260 imes10^3$	$0.437 imes 10^{-5}$	$37.04  imes 10^{-3}$	$1.238  imes 10^3$	0.653	0.646	0.603	1.161	0.517
0.400	35	1.569	0.208	$5.915 imes 10^3$	$0.676  imes 10^{-5}$	$44.01\times10^{-3}$	$1.429  imes 10^3$	0.665	0.659	0.605	1.186	0.519
	40	1.563	0.210	$6.271 \times 10^3$	$0.767 imes10^{-5}$	$48.64\times10^{-3}$	$0.931  imes 10^3$	0.668	0.667	0.607	1.193	0.520
	50	1.444	0.236	$7.319  imes 10^3$	$0.934 \times 10^{-5}$	$55.50 imes 10^{-3}$	$0.674  imes 10^3$	0.674	0.671	0.607	1.200	0.522
	60	1.294	0.274	$7.997 \times 10^3$	$0.581 \times 10^{-5}$	$58.66  imes 10^{-3}$	$0.321 imes 10^3$	0.661	0.667	0.606	1.160	0.523
	<i>CL</i>	1 266	0.282	$9.051 \times 10^{-3}$	$1.452 \times 10^{-5}$	$62.18 \times 10^{-3}$	$0.293 \times 10^{-3}$	0.686	0.673	0.607	1 220	0 574

$Ag_2S$	Day	Hq	(W) [+H]	$[H_3AsO_3]$ (M)	[Ag <sup>+</sup> ] (M)	[Cu <sup>2+</sup> ] (M)	Cu extraction rate (M/day)	Eh (V)	Eh <sub>ave</sub> (V)	E <sub>c</sub> (Cu <sup>2+</sup> ) (V)	$E_{c}(Ag^{+})(V)$	E <sub>ox</sub> (Cu <sub>2</sub> S) (V)
	10	1.733	0.177	10-5	1	$12.02  imes 10^{-3}$	$0.733  imes 10^3$	0.709	0.691	0.607		0.501
	15	1.618	0.198	$10^{-5}$		$13.27 imes10^3$	$0.257 imes10^3$	0.772	0.740	0.607		0.502
	20	1.403	0.246	$10^{-5}$		$14.62  imes 10^{-3}$	$0.267  imes 10^3$	0.786	0.779	0.607		0.504
	25	1.316	0.268	$10^{-5}$		$15.97 imes10^{-3}$	$0.270  imes 10^3$	0.779	0.783	0.607	·	0.505
)00	30	1.238	0.290	$10^{-5}$		$17.65  imes 10^{-3}$	$0.345  imes 10^3$	0.773	0.776	0.608	ı	0.506
%0	35	1.202	0.301	$10^{-5}$		$18.52 imes10^3$	$0.179  imes 10^3$	0.772	0.772	0.609	ı	0.507
	40	1.226	0.294	$10^{-5}$		$20.17 imes10^3$	$0.331  imes 10^3$	0.771	0.772	0.611		0.508
	50	1.192	0.304	$10^{-5}$	·	$22.10\times10^{-3}$	$0.189  imes 10^3$	0.790	0.781	0.612		0.509
	60	1.101	0.333	$10^{-5}$		$25.34  imes 10^{-3}$	$0.330  imes 10^3$	0.767	0.778	0.614		0.511
	72	1.130	0.323	$10^{-5}$		$28.07 imes10^{-3}$	$0.227  imes 10^3$	0.774	0.770	0.616		0.513
	10	1.721	0.179	$10^{-5}$	$0.545  imes 10^{-5}$	$22.09  imes 10^{-3}$	$2.409 \times 10^3$	0.659	0.646	0.618	1.265	0.509
	15	1.631	0.196	$10^{-5}$	$0.563 imes 10^{-5}$	$28.23  imes 10^{-3}$	$1.265  imes 10^3$	0.660	0.659	0.622	1.263	0.513
	20	1.541	0.214	$10^{-5}$	$1.285\times 10^{-5}$	$32.89  imes 10^3$	$0.925  imes 10^3$	0.682	0.671	0.624	1.316	0.515
	25	1.475	0.229	$10^{-5}$	$4.668\times10^{5}$	$37.02  imes 10^{-3}$	$0.823  imes 10^3$	0.718	0.700	0.626	1.402	0.517
	30	1.329	0.265	$10^{-5}$	$78.67 imes10^{-5}$	$40.36 \times 10^{-3}$	$0.688  imes 10^3$	0.795	0.757	0.626	1.589	0.518
0/ CON.	35	1.243	0.289	$10^{-5}$	$84.32\times10^{-5}$	$42.44 \times 10^{-3}$	$0.425  imes 10^3$	0.797	0.796	0.626	1.590	0.518
	40	1.249	0.287	$10^{-5}$	$38.13\times 10^{5}$	$43.40 \times 10^{-3}$	$0.193  imes 10^3$	0.775	0.786	0.626	1.536	0.519
	50	1.183	0.307	$10^{-5}$	$5.040 imes 10^{-5}$	$44.84 \times 10^{-3}$	$0.142  imes 10^3$	0.720	0.748	0.626	1.395	0.519
	09	1.077	0.341	$10^{-5}$	$2.632\times 10^{-5}$	$45.59 imes10^3$	$0.076  imes 10^3$	0.702	0.711	0.625	1.346	0.519
	72	1.103	0.332	$10^{-5}$	$1.585\times 10^{-5}$	$46.95 \times 10^{-3}$	$0.113  imes 10^3$	0.688	0.695	0.626	1.312	0.520
	10	1.863	0.155	$10^{-5}$	$0.214\times 10^{-5}$	$16.90  imes 10^{-3}$	$1.767  imes 10^3$	0.633	0.624	0.615	1.206	0.506
	15	1.771	0.170	$10^{-5}$	$0.246\times 10^{-5}$	$23.02  imes 10^{-3}$	$1.261  imes 10^3$	0.637	0.635	0.620	1.212	0.510
	20	1.664	0.189	$10^{-5}$	$0.424\times 10^{-5}$	$28.09 imes10^{-3}$	$1.005  imes 10^3$	0.652	0.645	0.622	1.245	0.513
	25	1.618	0.198	$10^{-5}$	$1.154\times 10^{-5}$	$33.36 \times 10^{-3}$	$1.049  imes 10^3$	0.680	0.666	0.625	1.312	0.515
0.010	30	1.490	0.225	$10^{-5}$	$4.584\times10^{5}$	$38.61 \times 10^{-3}$	$1.082  imes 10^3$	0.717	0.698	0.627	1.401	0.517
N 10.0	35	1.360	0.257	$10^{-5}$	$9.287 \times 10^{-5}$	$42.57  imes 10^3$	$0.812  imes 10^3$	0.737	0.727	0.627	1.444	0.518
	40	1.363	0.256	$10^{-5}$	$29.64\times 10^{-5}$	$45.73  imes 10^{-3}$	$0.634  imes 10^3$	0.768	0.753	0.628	1.524	0.519
	50	1.239	0.290	$10^{-5}$	$14.18\times 10^{-5}$	$48.23\times10^{-3}$	$0.246  imes 10^3$	0.748	0.758	0.628	1.468	0.520
	60	1.087	0.337	$10^{-5}$	$5.392 imes 10^{-5}$	$50.33 imes10^{-3}$	$0.214  imes 10^3$	0.722	0.735	0.627	1.396	0.521
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$Ag_2S$	Day	Hq	(M) [ <sup>+</sup> H]	[H <sub>3</sub> AsO <sub>3</sub> ] (M)	[Ag <sup>+</sup> ] (M)	[Cu <sup>2+</sup> ] (M)	Cu extraction rate (M/day)	Eh (V)	$Eh_{ave}\left(V ight)$	$E_{c}(Cu^{2+})$ (V)	$E_{c}(Ag^{+})\left(V\right)$	$E_{ox}(Cu_2S)(V)$
	10	1.877	0.153	10 <sup>-5</sup>	$0.166  imes 10^{-5}$	$18.00  imes 10^{-3}$	$1.877 imes10^3$	0.626	0.619	0.616	1.190	0.507
	15	1.799	0.166	$10^{-5}$	$0.156\times 10^{-5}$	$24.40 imes10^{-3}$	$1.318\times 10^3$	0.625	0.626	0.621	1.182	0.511
	20	1.692	0.184	$10^{-5}$	$0.271 imes 10^{-5}$	$28.85 \times 10^{-3}$	$0.883  imes 10^3$	0.640	0.632	0.623	1.216	0.513
	25	1.642	0.194	$10^{-5}$	$0.653 imes 10^{-5}$	$33.99 imes10^3$	$1.023  imes 10^3$	0.664	0.652	0.626	1.274	0.515
2000	30	1.528	0.217	$10^{-5}$	$1.966  imes 10^{-5}$	$40.17 \times 10^{-3}$	$1.273  imes 10^3$	0.694	0.679	0.628	1.345	0.518
0.02%	35	1.417	0.243	$10^{-5}$	$3.976 imes 10^{-5}$	$45.66  imes 10^3$	$1.127  imes 10^3$	0.713	0.704	0.629	1.388	0.519
	40	1.390	0.249	$10^{-5}$	$8.129 \times 10^{-5}$	$50.01 imes10^{-3}$	$0.874  imes 10^3$	0.733	0.723	0.631	1.436	0.521
	50	1.247	0.287	$10^{-5}$	$33.56  imes 10^{-5}$	$53.52 imes10^{-3}$	$0.344  imes 10^3$	0.772	0.752	0.630	1.528	0.522
	60	1.104	0.332	$10^{-5}$	$3.448  imes 10^{-5}$	$55.10 imes10^3$	$0.161  imes 10^3$	0.710	0.741	0.629	1.366	0.522
	72	1.105	0.331	$10^{-5}$	$3.436  imes 10^{-5}$	$58.49 imes10^3$	$0.282  imes 10^3$	0.709	0.709	0.630	1.366	0.523
	10	1.885	0.152	$10^{-5}$	$0.134  imes 10^{-5}$	$17.88  imes 10^{-3}$	$1.973  imes 10^3$	0.620	0.614	0.616	1.175	0.507
	15	1.854	0.157	$10^{-5}$	$0.143 \times 10^{-5}$	$24.73 imes10^{-3}$	$1.412  imes 10^3$	0.622	0.621	0.622	1.178	0.511
	20	1.726	0.178	$10^{-5}$	$0.217 imes 10^{-5}$	$29.34  imes 10^{-3}$	$0.914  imes 10^3$	0.634	0.628	0.624	1.202	0.513
	25	1.687	0.185	$10^{-5}$	$0.385 \times 10^{-5}$	$33.97  imes 10^3$	$0.923  imes 10^3$	0.649	0.642	0.626	1.240	0.515
/0000	30	1.585	0.205	$10^{-5}$	$0.677 imes 10^{-5}$	$38.87  imes 10^{-3}$	$1.009  imes 10^3$	0.665	0.657	0.628	1.274	0.517
0% CU.L	35	1.525	0.218	$10^{-5}$	$1.333 imes 10^{-5}$	$44.10\times10^{-3}$	$1.073  imes 10^3$	0.683	0.674	0.630	1.318	0.519
	40	1.482	0.227	$10^{-5}$	$2.039 imes 10^{-5}$	$48.02 \times 10^{-3}$	$0.788  imes 10^3$	0.695	0.689	0.631	1.345	0.520
	50	1.358	0.257	$10^{-5}$	$3.119 imes 10^{-5}$	$53.86  imes 10^{-3}$	$0.573  imes 10^3$	0.707	0.701	0.632	1.369	0.522
	60	1.192	0.304	$10^{-5}$	$6.389 imes 10^{-5}$	$57.55 imes10^{-3}$	$0.376  imes 10^3$	0.726	0.717	0.631	1.412	0.523
	72	1.131	0.323	$10^{-5}$	$4.460\times 10^{-5}$	$62.37  imes 10^{-3}$	$0.402  imes 10^3$	0.717	0.721	0.632	1.384	0.524
	10	1.967	0.140	10 <sup>-5</sup>	$0.057 imes 10^{-5}$	$15.39  imes 10^{-3}$	$1.336  imes 10^3$	0.597	0.599	0.614	1.120	0.504
	15	1.887	0.152	$10^{-5}$	$0.089 imes 10^{-5}$	$19.16  imes 10^{-3}$	$0.777 imes10^3$	0.609	0.603	0.618	1.148	0.507
	20	1.777	0.169	$10^{-5}$	$0.148 \times 10^{-5}$	$24.74  imes 10^{-3}$	$1.106  imes 10^3$	0.623	0.616	0.621	1.178	0.511
	25	1.745	0.175	$10^{-5}$	$0.271\times 10^{-5}$	$31.03 imes10^{-3}$	$1.254  imes 10^3$	0.640	0.631	0.625	1.218	0.514
0.040/	30	1.650	0.192	$10^{-5}$	$0.437 imes 10^{-5}$	$37.04 \times 10^{-3}$	$1.238\times 10^3$	0.653	0.646	0.628	1.247	0.517
J.U4%	35	1.569	0.208	$10^{-5}$	$0.676  imes 10^{-5}$	$44.01\times10^{-3}$	$1.429  imes 10^3$	0.665	0.659	0.630	1.273	0.519
	40	1.563	0.210	$10^{-5}$	$0.767 imes10^{-5}$	$48.64 \times 10^{-3}$	$0.931  imes 10^3$	0.668	0.667	0.632	1.282	0.520
	50	1.444	0.236	$10^{-5}$	$0.934 imes 10^{-5}$	$55.50 imes10^{-3}$	$0.674  imes 10^3$	0.674	0.671	0.633	1.290	0.522
	60	1.294	0.274	$10^{-5}$	$0.581 \times 10^{-5}$	$58.66  imes 10^{-3}$	$0.321  imes 10^3$	0.661	0.667	0.633	1.252	0.523
	<i>CL</i>	1 266	0.787	10 <sup>-5</sup>	$1.452 \times 10^{-5}$	$62.18 \times 10^{-3}$	$0.293 \times 10^{-3}$	0.686	0.673	0 633	1 313	0 504

### 4.3.4 Copper substitution on enargite surface with silver

Following identification of trisilver arsenic sulfide by XRD (Fig. 4.3), EPMA elemental mapping was performed in order to confirm the formation of Ag-containing passivation layers around the enargite surface after bioleaching with 0.04% Ag<sub>2</sub>S (Fig. 4.7). Emergence of bright white areas on the enargite surface indicated the formation of secondary minerals consisting of heavier metals than Cu, such as Ag (Fig. 4.7a). The enargite grain was indeed covered with a thick but porous secondary layer (Fig. 4.7a; solid arrow), consisting of Ag, As, and S (Fig. 4.7b, d, e), onto which another partial layer (Fig. 4.7a; broken arrow) of ferric arsenate (Fig. 4.7d, f) was observed. To further analyze the formation of Ag-containing passivation layers, EPMA quantitative analysis was conducted on different locations of the particle (Fig. 4.8): Spot 1, the core of enargite grain (grey); Spot 4, the passivation layer around the enargite surface (white); Spots 2 and 3, the interface between Spots 1 and 4 (light grey). Spots 1–4 shared the approximate atomic ratio of (Cu+Ag):As:S=3:1:4, with different Ag:Cu ratios (Table 4.5). An increasing dominance of Ag relative to Cu, from the core to surface of the enargite particle indicated that Cu was dissolved from enargite (Cu<sub>3</sub>AsS<sub>4</sub>; Spot 1) possibly by substitution with Ag ((Cu,Ag)<sub>3</sub>AsS<sub>4</sub>; Spots 2 and 3), eventually leaving the passivation layer of trisilver arsenic sulfide (Ag<sub>3</sub>AsS<sub>4</sub>; Spot 4) (Fig. 4.8).

In chemical/electrochemical studies for chalcopyrite, metal-deficient sulfur-rich layers  $(Cu_{1-x}Fe_{1-y}S_2 \text{ or } Cu_{1-x}Fe_{1-y}S_{2-z})$  were reported to passivate the mineral surface (Warren et al., 1982; Hackl et al., 1995; Ghahremaninezhad et al., 2010, 2013). Ghahremaninezhad et al. (2015) explained the mechanism of Ag-catalyzed chalcopyrite dissolution by Ag diffusion into such metal-deficient sulfur-rich layers, eventually producing Ag<sub>2</sub>S passivation. Likewise, trisilver arsenic sulfide detected in this study might have been formed via Ag ion diffusion into enargite-type metal-deficient sulfur-rich layers (Cu<sub>3-x</sub>AsS<sub>4</sub>; Córdova et al., 1997; Fantauzzi et al., 2007, 2009).

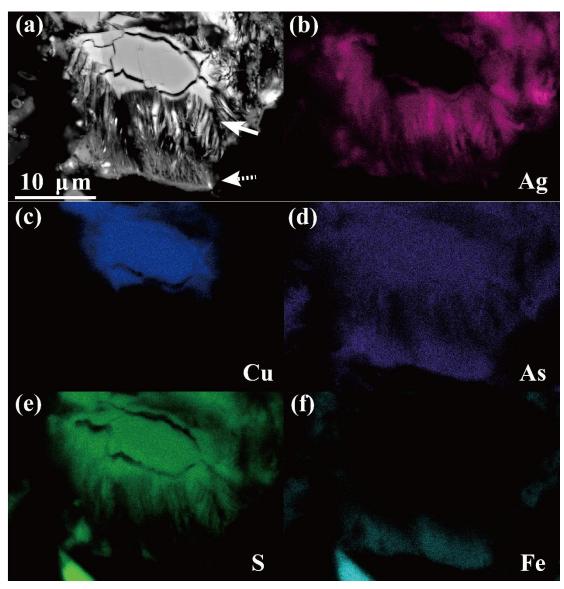


Fig. 4.7 EPMA elemental mapping of enargite concentrate residue bioleached for 72 days with 0.04%  $Ag_2S$ : The backscattered electron image at 2000-fold magnification (a) was mapped for Ag (b), Cu (c), As (d), S (e) and Fe (f). The surface of an enargite grain is covered with Ag-containing secondary mineral (solid arrow), on which deposition of ferric arsenate is observed (broken arrow).

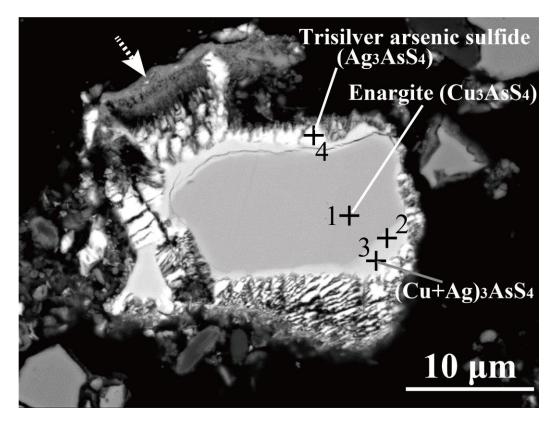


Fig. 4.8 Backscattered electron image of an enargite grain bioleached for 72 days with 0.04% Ag<sub>2</sub>S at the 2000-fold magnification. Cross points 1–4 indicate the beam spot positions for quantitative analysis (results summarized in Table 4.5).

surface after bioleaching: Numbers 1-4 indicate the cross points 1-5 in Fig. 4.8,
respectively.

(Cu+Ag) 2 49.15 12.02 11.63 0.91 26.29 Cu (Cu+Ag)	A tomaio motio
(Cu+Ag) 2 49.15 12.02 11.63 0.91 26.29 Cu (Cu+Ag)	Atomic ratio
(Cu+Ag)	: Ag = 40.4 : 1.0 As : S = 3.3 : 1.0 : 4.3
	: Ag = 2.2 : 1.0 As : S = 3.3 : 1.0 : 4.2
	: Ag = 1.0 : 2.0 As : S = 3.4 : 1.0 : 3.8
	: Ag = 1.0 : 7.6 As : S = 2.7 : 1.0 : 3.5
5 0.78 0.04 6.20 6.05 0.09 Fe : As	: O = 1.0 : 1.0 : 3.9

### 4.3.5 Kinetic study on Ag-catalyzed bioleaching of enargite concentrate

The shrinking core model is frequently utilized to model the mineral dissolution process. Based on this model, the dissolution reaction proceeds either via diffusion through the liquid film (Eq. 4-22), diffusion through product film (Eq. 4-23) or surface chemical reaction (Eq. 4-24), one of which may become the rate-limiting step under certain conditions (Wadsworth and Sohn, 1979).

$$\mathbf{X} = k_l \mathbf{t} \tag{Eq. 4-22}$$

$$1 - 3(1 - X)^{2/3} + 2(1 - X) = k_d t$$
 (Eq. 4-23)

$$1 - (1 - X)^{1/3} = k_r t \tag{Eq. 4-24}$$

X: the fraction of dissolved Cu

t: the reaction time

k: the rate constant

In order to investigate which process rate-limits Cu dissolution during bioleaching of enargite concentrate with and without Ag<sub>2</sub>S, measured values from Fig. 4.1a were fitted to Eqs. 4-23 and 4-24 (Fig. 4.9). The fluid film resistance was considered negligible relative to other effects, and in fact no linear relationships between X against t were found. The *k* and  $R^2$  values were calculated from the fitting results and listed in Table 4.6. Linear lines were drawn where  $R^2$  values of regression analyses were > 0.99 (Table. 4.6).

In the absence of Ag<sub>2</sub>S, rapid Fe dissolution (Fig. 4.1c) caused precipitation of jarosite (as confirmed by XRD; Fig. 4.2), resulting in the reaction being fitted to diffusion through product film throughout the bioleaching period (Fig. 4.9a; Table 4.6). At higher Ag<sub>2</sub>S concentration of 0.03 and 0.04%, on the other hand, surface chemical reaction was likely the rate-limiting step until the end (Fig. 4.9e, f; Table 4.6), suggesting that formation of trisilver arsenic sulfide layer (as well as ferric arsenate "outer" layer) around the enargite surface did not rate-limit the enargite dissolution. Rather, the formation of trisilver arsenic sulfide was likely involved in the mechanism of facilitated enargite dissolution. At 0.005–0.02% Ag<sub>2</sub>S concentrations, enargite dissolution was

controlled by surface chemical reaction but only at the early stage (0–20 days at 0.005% and 0–40 days at 0.01–0.02%; Fig. 4.9b–d; Table 4.6) due to depletion of Ag.

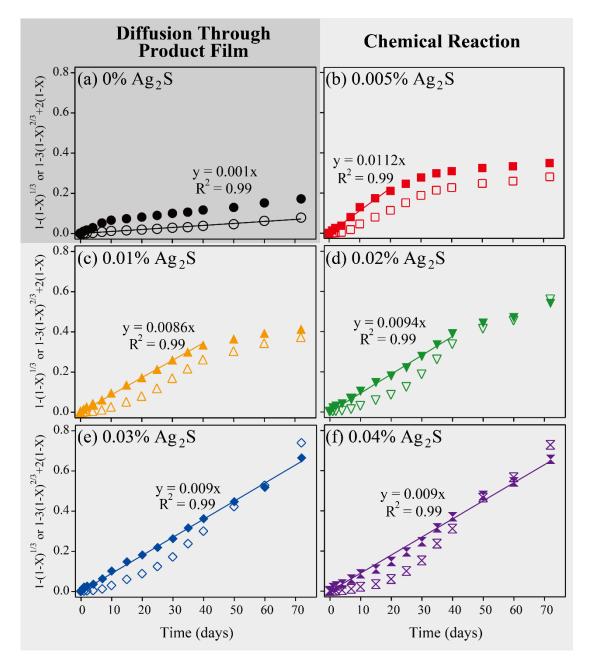


Fig. 4.9 Kinetic modeling on bioleaching of enargite concentrate at different Ag<sub>2</sub>S concentrations: (a) 0%, (b) 0.005%, (c) 0.01%, (d) 0.02%, (e) 0.03% and (f) 0.04%. Solid and open symbols indicate the fitting data to surface chemical reaction  $(1-(1-X)^{1/3}=k_rt)$  and diffusion through product film  $(1-3(1-X)^{2/3}+2(1-X)=k_dt)$ , respectively. Linear lines were drawn where R<sup>2</sup> values were calculated to be > 0.99.

Table 4.6  $R^2$  and *k* values calculated using the kinetic model of surface chemical reaction and diffusion through product film. Shadowed cells ( $R^2 > 0.99$ ) indicate which one of the two models fits the experimental data.

	× 1 1		Reactio	on model	
Ag <sub>2</sub> S addition (%)	Leaching period (day)	Surface chem	nical reaction	Diffusion throug	gh product film
(70)	(day)	k <sub>r</sub>	$\mathbb{R}^2$	k <sub>d</sub>	$\mathbb{R}^2$
0	0 - 72	0.0028	0.82	0.0010	0.99
0.005	0 - 20	0.0112	0.99	0.0051	0.94
0.005	25 - 72	0.0019	0.88	0.0025	0.90
0.01	0 - 40	0.0086	0.99	0.0056	0.93
0.01	50 - 72	0.0022	0.98	0.0031	0.98
0.02	0 - 40	0.0094	0.99	0.0066	0.89
0.02	50 - 72	0.0045	0.96	0.0068	0.96
0.03	0 - 72	0.0090	0.99	0.0084	0.92
0.04	0 - 72	0.0090	0.99	0.0085	0.90

# 4.4 Conclusions

Based on the overall results obtained in this study, a proposed mechanism for Agcatalyzed bioleaching of enargite concentrate was summarized in Fig. 4.10. The mechanism includes the formation of at least two types of secondary products (chalcocite and trisilver arsenic sulfide).

Chalcocite intermediate: Due to the low rest potential of Ag<sub>2</sub>S (compared to those of enargite and pyrite), consumption of Fe<sup>3+</sup> is more likely directed towards oxidation of Ag<sub>2</sub>S to produce Fe<sup>2+</sup> and Ag<sup>+</sup>. Instead, oxidation of pyrite by Fe<sup>3+</sup> is suppressed (I). Addition of Ag<sub>2</sub>S may also partially inhibit the activity of Fe-oxidizing microorganisms (II). Due to (I) and (II), Fe<sup>2+</sup> becomes more abundant than Fe<sup>3+</sup> to maintain lower  $E_h$  to satisfy  $E_{ox}$  (Cu<sub>2</sub>S) <  $E_h$  < Ec (Ag<sup>+</sup>). Consequently, enargite dissolution was enhanced via the formation of Cu<sub>2</sub>S intermediate, accompanied by the production of H<sub>2</sub>S which is rapidly removed by Ag<sup>+</sup> to re-form Ag<sub>2</sub>S (III). The resultant Cu<sub>2</sub>S is amenable to oxidation by Fe<sup>3+</sup> to solubilize Cu<sup>2+</sup> (IV).

Trisilver arsenic sulfide: Cu ion in the enargite structure is gradually substituted with  $Ag^+$  solubilized from  $Ag_2S$  to form an intermediate layer of  $(Cu,Ag)_3AsS_4$ . Eventually, trisilver arsenic sulfide  $(Ag_3AsS_4)$  covers the surface of enargite (V). The formation of this product film, however, does not impose a rate-limiting step.

The combination of the above reactions contributes to enhanced enargite bioleaching in the presence of  $Ag_2S$  as an effective Ag catalyst.

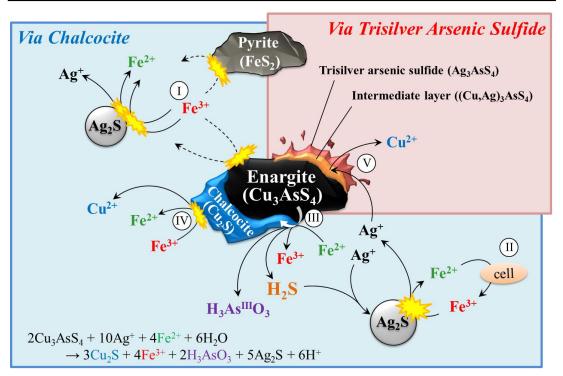


Fig. 4.10 Schematic image illustrating the proposed mechanism of Ag-catalyzed bioleaching of enargite concentrate.

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Data shown in this chapter are partially included in the paper submitted to Hydrometallurgy (2018, 177, 197-204) entitled "Silver-catalyzed bioleaching of enargite concentrate using moderately thermophilic microorganisms".

# **Chapter 5**

Evaluating catalytic ability of activated carbon in bioleaching of enargite concentrate and elucidating its catalytic mechanism

#### Abstract

The catalytic effect of activated carbon (AC) on bioleaching of enargite (Cu<sub>3</sub>AsS<sub>4</sub>) concentrate was studied to evaluate its catalytic capability in copper (Cu) and iron (Fe) solubilization, arsenic (As) immobilization, and solution redox potential,  $E_h$  control. In the absence of AC, co-existing pyrite (FeS<sub>2</sub>) in the concentrate began to rapidly solubilize at day 7, which was increasingly delayed by the addition of 0.1% and 0.2% AC to day 25 and 35, respectively. Suppression of pyrite dissolution was the result of the lowered  $E_h$  level via  $Fe^{3+}$ -reduction coupled with reduced inorganic sulfur compounds (RISCs)-oxidation on the AC surface acting as an electron-mediator. Realtime PCR analysis found that the abundance of S-oxidizing bacteria dropped in the presence of AC, proving that RISCs as an energy source for S-oxidizing bacteria were indeed consumed via the coupling reaction. While final Cu recovery was improved from 36% (0% AC) to 46% (0.1%) and 53% (0.2%), electrochemical study suggested that this was not much contributed by the galvanic interaction between enargite and AC. A kinetic study using the shrinking core model revealed that AC addition let Cu solubilize slowly but steadily and continuously at lower  $E_{\rm h}$  under the suppression of pyrite dissolution, consequently improving the final Cu recovery. Addition of AC also facilitated the As immobilization from 3.1 mM (0% AC at day 10) to 5.2 mM (0.1% AC at day 30), 7.0 mM (0.2% AC at day 40), and 6.9 mM (0.3% AC at day 60). EPMA analysis found that As was immobilized as ferric arsenate selectively on the enargite surface, while its re-solubilization was observed coincided with rapid pyrite dissolution. This observation implied that high dissolved sulfate concentration from pyrite might have the effect of triggering re-solubilization of As-precipitates. Based on the results obtained above, the overall mechanism of AC-catalyzed bioleaching of enargite concentrate was proposed.

# 5.1 Introduction

Arsenic contamination in copper mine has been increasingly recognized as a serious problem in the copper mining industry in decades. Although enargite (Cu<sub>3</sub>AsS<sub>4</sub>) is wellknown as one of the As-bearing sulfides, it also has a potential for future Cu resource. Hence, the installation of environmental-friendly and economical technique, by which Cu is selectively extracted rather than As from enargite, has been desperately awaited. Conventional pyrometallurgical process is inapplicable to these As-bearing copper sulfides from the environmental point of view (Takatsugi et al., 2011); the smelting let As volatilize into the air in the unmanageable gaseous form. Hydrometallurgical process has been therefore thought appropriate for the exploitation of As-bearing sulfides such as pressure leaching (Ruiz et al., 2011; Padilla et al., 2015), acid leaching (Safarzadeh et al., 2014), and alkaline leaching (Li et al., 2018). Bioleaching is also considered as one of the most promising hydrometallurgical processes due to its environmental and economic advantages, and high-temperature bioleaching of enargite have indeed succeeded to exclusively extract Cu rather than As; > 90% Cu solubilized into the solution while < 90% As remained in the solid phase (Sasaki et al., 2011). Likewise, other tests of high-temperature (65-70°C) bioleaching have achieved high Cu recovery (52-91%; Escobar et al., 2000; Muñoz et al., 2006; Lee et al., 2011; Takatsugi et al., 2011; Sasaki et al., 2011), whereas those of low-temperature (25-30°C) bioleaching still need to be improved (< 15%; Escobar et al., 1997; Sasaki et al., 2010). These investigations suggest the necessity of the additive such as a catalyst to further promote the Cu dissolution under lower-temperature condition.

Although the number is limited, some studies have investigated the effect of the catalysts on enargite dissolution: silver (Ag; Miki et al., 2016; Oyama et al., 2018) and carbon materials (Olvera et al., 2013; Jahromi et al., 2016, 2017, 2018, 2019). The former has long been recognized as the most effective catalyst on the dissolution of refractory copper sulfides, especially for chalcopyrite (CuFeS<sub>2</sub>; Ahonen and Tuovinen et al., 1990; Ballester et al., 1990; Hiroyoshi et al., 2002; Muñoz et al., 2007; Nazari et al., 2012a and 2012b; Ghahremaninezhad et al., 2015). Miki et al. (2016) reported that even enargite dissolution was dramatically enhanced in the presence of Ag by promoting the transformation from enargite into more amenable intermediate, chalcocite, at the specific  $E_h$  range. Moreover, Oyama et al. (2018) concluded that

bioleaching of enargite concentrate was also catalyzed by the addition of Ag<sub>2</sub>S based on the collaborative two different mechanisms: (i) Miki's theory and (ii) Ag atom diffusion into enargite structure via the replacement with Cu atom. Although its catalytic capability is outstanding among possible catalysts, there are some drawbacks to its difficulty in recycling use. Nazari et al. (2011) employed silver-doped pyrite for enabling the easier silver-recycling system, while the loss of silver was inevitable, resulting in the prolonged leaching period in the recycled experiment. It indicates that an alternative catalyst, which is much cheaper and certainly consumable, needs to be sought for the more practical process.

The latter has recently attracted researchers' attention due to its electrochemically catalytic effect on the dissolution of refractory copper sulfides. Originally, the utility of AC as one of the carbon materials has been reported in the chalcopyrite bioleaching experiment (Nakazawa et al., 1998; Zhang et al., 2007; Liang et al., 2010). In these studies, chalcopyrite dissolution was thought to be enhanced basically through galvanic interaction between electrically nobler AC and electrically poorer chalcopyrite. Olvera et al. (2013) tested its catalytic effect in enargite leaching by electrochemical study, suggesting its potential for the enhancement of enargite dissolution by causing galvanic effect as well as modifying semi-conductive surface property of enargite. Jahromi et al. (2016) indeed confirmed the effectiveness of AC in enargite leaching, where enargite dissolution was promoted based on (i) the oxidation of Fe<sup>2+</sup> to Fe<sup>3+</sup> (oxidant regeneration) and (ii) direct enargite oxidation by in-situ hydrogen peroxide production. These mechanisms were proposed by Ahumada et al. (2002), where the oxidation reactions occur on the surface of AC as follows;

$$2C_{red}^{*} + O_2 + 2H_2O = 2H_2O_2 + 2C_{ox}^{*}$$
 (Eq. 7-1)

$$2Fe^{2+} + H_2O_2 + 2H^+ = 2Fe^{3+} + 2H_2O$$
 (Eq. 7-2)

 $C_{red}$  and  $C_{ox}$  indicate that surface functional groups on the surface of AC. Eq. 7-1 shows the generation of hydrogen peroxide occurring on the surface of AC through the reaction of quinone or other oxidative functional groups such as carboxylic acid, anhydrides, hydroxyls, lactol groups, lactone groups, and phenol groups. This hydrogen peroxide is subsequently (i) consumed to directly oxidize enargite or (ii) used for the oxidation of  $Fe^{2+}$  to  $Fe^{3+}$  (Eq. 7-2), followed by enargite oxidation by produced  $Fe^{3+}$ . Modification of functional groups on the surface of AC with sulfuric acid, hydrochloric acid, or nitric acid was tested, confirming that the oxidation ability of AC was indeed varied with different acid treatments even in the leaching process (Jahromi et al., 2019).

On the other hand, it has been reported that the presence of AC suppress  $E_h$  rise during bioleaching process, implying that AC would also catalyze the Fe<sup>3+</sup>-reduction (Nakazawa et al., 1998; Zhang et al., 2007; Ma et al., 2017; Hao et al., 2018). This adverse catalytic effect of AC was confirmed in the chemical experiment conducted by Vargas et al. (2009), where Fe<sup>3+</sup>-reduction to Fe<sup>2+</sup> was able to be catalyzed by the AC. Liang et al. (2010) observed the decrease in Fe<sup>3+</sup>/Fe<sup>2+</sup> ratio with the addition of AC during chalcopyrite bioleaching, ensuring that Fe<sup>3+</sup> was indeed catalytically reduced to Fe<sup>2+</sup> by AC even in the presence of microorganisms. Although the reduction mechanism has yet been well-described, not only Fe<sup>2+</sup>-oxidation but also Fe<sup>3+</sup>-reduction have to be considered as the catalytic reaction caused by AC during the bioleaching process.

The addition of AC also shows a positive effect on the formation of scorodite (FeAsO<sub>4</sub>·2H<sub>2</sub>O) as an immobilized form of once-dissolved As from enargite (Jahromi et al., 2018). This would attribute to the catalytic reaction on the surface of AC; As-oxidation was greatly enhanced in the presence of AC, possibly by hydrogen peroxide generated (Radzinski et al., 2016). The enhanced As-oxidation on the AC surface led to the As(V) supply for the in-situ formation of scorodite during enargite leaching, consequently promoting the immobilization of As in the solid phase (Jahromi et al., 2018).

Although the catalytic mechanism of AC in the leaching process is roughly summarized as (i) electrochemical reaction to accelerate the electron transfer (e.g. galvanic interaction and other redox reaction) and (ii) chemical reaction by surface functional groups to produce the oxidant (e.g.  $Fe^{3+}$  and hydrogen peroxide), further discussion is still necessary to reach a consensus among researchers. Moreover, the number of studies investigating the effect of AC on enargite bioleaching is still limited, while the addition of AC in chemical enargite leaching is shown effective in enhanced Cu dissolution and As immobilization. This study, therefore, aimed to evaluate the catalytic capability of AC in Cu and Fe solubilization, As immobilization, and  $E_h$  control during enargite bioleaching. The electrochemical study, kinetic model fitting, microbiological population structure analysis were also carried out to clarify the underlying catalytic mechanism in the presence of AC.

# 5.2 Materials and methods

# 5.2.1 Activated carbon (AC)

AC (Wako) used in this study was granular shape with an average particle size of around 5 mm. The BET specific surface area and average pore diameter of AC were determined as was described by Konadu et al. (2017). The sample was pre-treated in two steps: vacuum degassing for 90 min at 150°C and finally vacuum pre-treatment for 15 h at 150°C. The measurement was conducted by N<sub>2</sub> (99.99%) adsorption using BELSORP-max porosimeter (JAPAN BELL). The obtained data were analyzed by BEL master software in version 6.3.0.0 (JAPAN BELL) based on the non-local density functional theory (Lastoskie et al., 1993). The obtained specific surface area and average pore diameter were 1212 m<sup>2</sup>/g and 1.77 nm, respectively.

# **5.2.2 Bioleaching experiments**

Pre-grown culture of each of three strains (*Am. ferrooxidans* ICP, *Sb. sibiricus* N1, and *At. caldus* KU) was centrifuged (9000 rpm, 10 min at 4°C) to collect cells and washed twice with acidified water (pH 1.7), prior to inoculation into 200 mL HBS medium (pH 2.0; in 500 mL Erlenmeyer flasks) containing 2% (w/v) enargite concentrate and 5 mM Fe<sup>2+</sup> (to set the initial cell density of each strain at  $1.0 \times 10^7$  cells/mL; i.e.  $3.0 \times 10^7$  cells/mL in total). AC was added into the medium at different concentrations; 0, 0.1, 0.2, 0.3% (w/v). Flasks were incubated shaken at 45°C and 150 rpm for 60 days. Samples were regularly withdrawn to monitor pH, *E*<sub>h</sub>, cell density, and concentrations of Fe<sup>2+</sup> (*o*-phenanthroline method), As(III) (molybdenum blue method), and total Fe, As and Cu (ICP-OES). Solid residue was collected and freeze-dried overnight for the analysis by EPMA.

# 5.2.3 Abiotic evaluation of catalytic ability of AC

As for the abiotic experiment, AC (0.1% (w/v)) was added with 100 mL of ABS medium (pH adjusted to 2.0 with 1 M H<sub>2</sub>SO<sub>4</sub>) into the 300 mL of Erlenmeyer flask. For the series of experiments, 10 mM Fe<sup>2+</sup> or Fe<sup>3+</sup>, 5 mM of sodium tetrathionate and/or 0.02% yeast extract were solely or simultaneously added into the medium. As for the biotic experiment, heterotrophic basal salts media (200 ml in 500 ml Erlenmeyer flasks; pH adjusted to 2.0 with 1 M H<sub>2</sub>SO<sub>4</sub>) containing 5 mM of sodium tetrathionate or 5 mM

of As(III) as NaAsO<sub>2</sub> were prepared and sterilized by autoclaving. Fe-oxidizing bacterium without S- and As-oxidizing ability, *Am. ferrooxidans* ICP, was inoculated into the sterilized medium to set the initial cell density to  $1.0 \times 10^7$  cells/mL. Five mM Fe<sup>2+</sup> and 0.02% (w/v) yeast extract were also supplemented for bacterial growth at the initial stage of the bioleaching experiments. Inoculated cultures with and without the addition of 0.2% (w/v) AC were prepared in duplicate. These flasks were incubated and shaken at 45°C and 150 rpm. Solution samples were regularly withdrawn to monitor pH,  $E_h$ , Fe<sup>2+</sup> and total Fe concentration (*o*-phenanthroline method), As(III) concentration (molybdenum blue method), and sulfate concentration (turbidimetric method).

#### 5.2.4 Real-time PCR

In order to investigate the microbial population structure in bioleaching cultures, Real-Time PCR (MiniOpticon, Bio-Rad) was conducted according to the methods described by Oyama et al. (2018) as follows. The purified genomic DNA from each strain was used as the template to PCR amplify the 16S rRNA gene fragment (~1473 bp) using the universal primer set (27f and 1492r: Table 5.1). The resultant PCR products derived from each strain were purified using ISOSPIN PCR Product (NIPPON GENE), quantified, and finally diluted to give a final concentration of  $1.0 \times 10^3$  to  $1.0 \times 10^9$ copies/µL, to be used as template DNA for Real-Time PCR. Once linearity in the standard curve was obtained within the range from  $1.0 \times 10^3$  to  $1.0 \times 10^9$  copies/µL for all species, synthetic DNA mixtures (composed of template DNA from each one of the four species at  $1.0 \times 10^3$  to  $1.0 \times 10^9$  copies/µL) was tested against each one of the four species-specific primer sets (Table 5.1) to ensure the accuracy in order to display the results as percentages in whole number. Genomic DNA extracted from the actual bioleaching mixed cultures were tested against the corresponding species-specific primer sets.

	Primer set	Primer sequence (5'-3')	Target species	PCR product size (bp)
aya	27f Universal	AGAGTTTGATCMTGGCTCAG		62 V 1
FUN	1492r Universal	TACGGYTACCTTGTTACGACTT	DACIETA	C/+I~
	Amferro-F1	TCATTCGACGGGCTCCGTG	Species-specific:	737
	Buniv-R1	GAGCTGACGACARCCATGCA	Am. ferrooxidans	707
Parl Time DCD	Sbsib-F1	TAGGTGTCGCCCGGGTCCAC	Species-specific:	140
NCAF LILLE FUN	Buniv-R1	1	Sb. sibiricus	147
	Acaldus-F3	TAGGTGCTGAGTGTCGTAGCTAACG	Species-specific:	731
	Buniv-R1		At. caldus	107

#### 5.2.5 Electrochemical analysis for the detection of galvanic reaction

In order to obtain the evidence of galvanic reaction occurring thought the contact between enargite and AC, electrochemical analysis was carried out. The mineral electrodes were prepared from the pure massive enargite, pyrite, and AC samples by cutting them into cubes (around 1 cm<sup>3</sup>). One side of the massive samples was used as the electrode surface, and the other side was connected to a copper wire using silver conductive paste. This was embedded into the resin for the fixation. The surface of each mineral electrode was polished by emery-paper to provide a flat surface and rinsed with pure water. Before each measurement, the polishing was conducted again to ensure that the pure mineral surface is properly exposed.

To obtain the solutions with varied  $E_h$ , 0.1 M H<sub>2</sub>SO<sub>4</sub> solution was prepared containing 0.1 M Fe with varied Fe<sup>2+</sup>/Fe<sup>3+</sup> ratio to adjust the  $E_h$  to 0.5, 0.53, 0.6, 0.68, 0.74, 0.8, 0.86, 0.9 V (vs. SHE).

Electrochemical analysis was carried out with the three-electrode method by using the electrochemical instrument (Solartron Analytical 1280 C, TOYO Corporation). Firstly, the  $E_h$  were measured by Ag/AgCl reference electrode and platinum working electrode. After that, mineral electrode potential at certain  $E_h$  was measured by replacing from platinum electrode to each one of the mineral electrode (enargite, pyrite, AC). Measurement time of solution  $E_h$  and electrode potential was set to 300 sec to reach the stationary phase. After the measurement, copper wire of two of mineral electrodes (enargite-pyrite or enargite-AC) were contacted together, which was further connected to the working electrode to measure the "minerals-contacted electrode potential". This electrode potential is assumed to be the actual potential when two minerals are contacted and the galvanic reaction occurs. Measurement time for this step was set to 60 sec.

For the galvanic current measurement, both reference and counter electrode were connected to one of AC or pyrite electrode, while the working electrode was connected to enargite electrode. In this condition, each mineral electrode was indirectly connected through electrochemical instrument; each electrode potential is independent but not the potential when two mineral electrodes were directly connected. In order to shift this mineral electrode potential to galvanic potential for artificially causing galvanic interaction, the difference between electrode potential and "minerals-contacted electrode potential" was intentionally applied to enargite electrode. The current value observed here was postulated as the galvanic current. The measurement time was set to 300 sec to reach the stationary phase.

# 5.3 Results and discussion

# **5.3.1** Dissolution behavior of Cu and Fe during bioleaching with and without AC addition

In the absence of AC without inoculation, Cu recovery at day 60 was only 11%, which increased to 23% by the addition of 0.3% AC (Fig. 5.1a). Meanwhile, Fe solubilization was also enhanced from 9% (0% AC) to 16% (0.3% AC) (Fig. 5.1b). This slightly facilitated Cu and Fe solubilization in AC-catalyzed abiotic leaching would result from the slight increase in  $E_h$ ; The  $E_h$  in the presence of AC was slightly higher (20-30 mV) throughout the experiment than that in the absence of AC (Fig. 5.1c). The oxidant generation (i.e. Fe<sup>3+</sup>), by AC-catalyzed Fe<sup>2+</sup>-oxidation could be the reason of this difference in  $E_h$ , suggesting that AC shows the Fe<sup>2+</sup>-oxidizing ability as was observed by the previous study (Jahromi et al., 2019).

Bioleaching without AC addition achieved higher Cu recovery than AC-catalyzed abiotic leaching, reaching 36% of final Cu recovery at day 60 (Fig. 5.1a). Similarly with sterile cultures, the addition of 0.1% and 0.2% AC further improved the Cu recovery to 46% and 53%, respectively (Fig. 5.1a), which show stronger catalyzing effect with less amount of AC addition (0.1% and 0.2%) than sterile cultures with 0.3% AC addition, implying the existence of synergistic effect between microbiologically catalyzing and AC-catalyzing effects on the enhanced Cu dissolution. However, excess amount of AC addition (0.3%) adversely affected on the Cu dissolution (35% of final Cu recovery at day 60; Fig. 5.1a), thus necessitating the strict optimization of the AC addition. It was reported that there is no specific  $E_h$  range where enargite dissolution is dramatically enhanced, and strongly oxidative condition (e.g. higher  $E_h$ ) is favorable for the faster enargite dissolution (Lattanzi et al., 2008). Excessively lowered  $E_h$  by the addition of 0.3% AC less than 700 mV throughout the experiment could be the reason of suppressed enargite dissolution (Fig. 5.1c).

Contrary to the enhancement of Cu dissolution, the addition of AC in the bioleaching cultures showed a suppressive effect on Fe solubilization. In the absence of AC, the rapid dissolution of Fe from pyrite began at day 7, readily reaching >80% Fe solubilization by day 40 (Fig. 5.1b). Addition of 0.1 and 0.2% AC increasingly delayed Fe dissolution to day 25 and 35, respectively, and at 0.3% AC, Fe dissolution was suppressed almost completely until day 60 (Fig. 5.1b). Pyrite is the only Fe source in

this concentrate, suppressed Fe dissolution was thus derived from selective suppression of pyrite dissolution. This trend was accompanied by lowered  $E_h$  levels during bioleaching; it took 7 (0% AC), 25 (0.1% AC), and 35 days (0.2% AC) to reach 700 mV, and < 700 mV was kept throughout the experiment in the presence of 0.3% AC (Fig. 5.1c). Lowered  $E_h$  level by the addition of AC was likely the result of Fe<sup>3+</sup> reduction to Fe<sup>2+</sup>, which is confirmed by the behavior of Fe<sup>2+</sup> concentration; the decrease in Fe<sup>2+</sup> concentration was deteriorated with the addition of AC (Fig. 5.1d). Since it has been reported that  $E_h$  rise to around 700 mV led to the initiation of the rapid pyrite dissolution in bioleaching cultures (Gu et al., 2012), AC likely played a key role to maintain the lower  $E_h$  level by reducing Fe<sup>3+</sup> to Fe<sup>2+</sup> to delay unwanted pyrite solubilization. Based on the above results, it was assumed that enargite dissolution could be indirectly catalyzed by the addition of AC via lowering  $E_h$  level to < 700 mV, followed by suppressing pyrite dissolution to prevent passivation of enargite surface with Fe precipitates.

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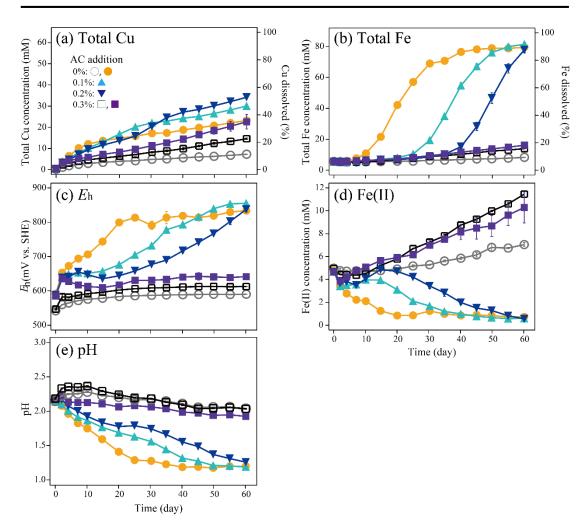
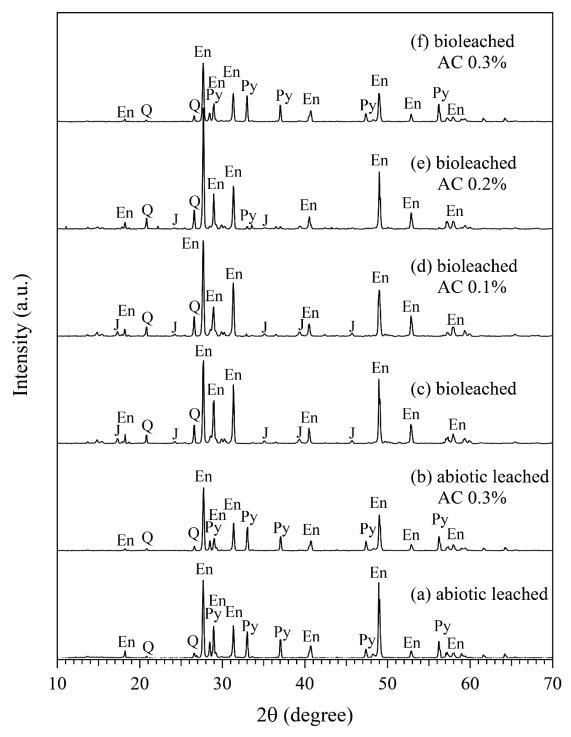


Fig. 5.1 Changes in the total soluble Cu concentration (a), total soluble Fe concentration (b),  $E_h$  (c), Fe<sup>2+</sup> concentration (d), and pH (e) during abiotic leaching (open symbol) or bioleaching (closed symbol) of enargite concentrate at 0% ( $\bigcirc$ ,  $\bigcirc$ ), 0.1% ( $\blacktriangle$ ), 0.2% ( $\checkmark$ ), or 0.3% (w/v) ( $\Box$ ,  $\blacksquare$ ) of AC. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



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Fig. 5.2 X-ray diffraction patterns of abiotic leached (a, b) and bioleached residues (cf) recovered on day 60 from cultures containing 0% (a, c), 0.1% (d), 0.2% (e), or 0.3% (b, f) of AC. En: enargite (Cu<sub>3</sub>AsS<sub>4</sub>; PDF No. 00-035-0775), Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>; PDF No. 01 - 070-3755), J: jarosite (K(Fe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub>); PDF No. 01-076-0629).

# 5.3.2 Catalytic mechanism of AC in the $E_h$ control

Above results indicate that  $\text{Fe}^{3+}$  could be reduced by the catalytic effect of AC, possibly via (i) the reaction with surface functional groups of AC and/or (ii) the electrochemical redox reaction on the surface of AC. To clearly understand this catalytic mechanism of AC in the *E*<sub>h</sub> control, the separate abiotic experiment was performed with the conditions as follows;

- (a) 10 mM Fe<sup>3+</sup> + 0.1% AC
- (b) 10 mM  $\mathrm{Fe}^{2+}$  + 0.1% AC
- (c) 5 mM tetrathionate + 0.1% AC
- (d) 10 mM  $Fe^{3+}$  + 5 mM tetrathionate
- (e) 10 mM Fe<sup>3+</sup> + 5 mM tetrathionate + 0.1% AC
- (f) 10 mM Fe<sup>3+</sup> + 0.02% yeast extract + 0.1% AC

Condition (a), (b), and (c) aimed to evaluate the oxidative/reductive ability of AC against solely present  $Fe^{3+}$ ,  $Fe^{2+}$ , tetrathionate. Condition (d), (e), and (f) were set to investigate the redox reaction electrochemically catalyzed by AC and find the suitable electron donor for strongly promoting  $Fe^{3+}$  reduction. Tetrathionate and yeast extract were employed as the model material of reduced inorganic sulfur compounds (RISCs) generated via the dissolution of sulfide minerals and organic metabolites produced by microorganisms, respectively. These materials were thought sufficiently present in the bioleaching culture throughout the experiment to act as the electron donor for  $Fe^{3+}$  reduction.

In the presence of AC with Fe<sup>3+</sup> (Fig. 5.3), a slight reduction of Fe<sup>3+</sup> to Fe<sup>2+</sup> (0.6 mM; Fig. 5.3a) was observed and thus  $E_h$  dropped from 829 mV to 741 mV in 4 h right after the experiment began (Fig. 5.3b; condition (a)). Subsequently, Fe<sup>2+</sup> concentration and  $E_h$  kept constant until the end of the experiment, suggesting that slight and rapid reduction of Fe<sup>3+</sup> to Fe<sup>2+</sup> at the beginning of the experiment was likely derived from the interaction with surface functional groups of AC. This result also indicates that functional groups on the AC surface would be insufficient to keep lowering the  $E_h$ throughout the leaching experiment. In the presence of AC with Fe<sup>2+</sup> or tetrathionate solely (conditions (b) and (c)), Fe<sup>2+</sup> and tetrathionate were constantly oxidized (Fig.

5.3); Fe<sup>2+</sup> concentration decreased from 9.4 mM (day 0) to 6.0 mM (day 6; Fig. 5.3a) and sulfate production increased from 0 (day 0) to 2.3 mM (day 6; Fig. 5.3c). These oxidations were catalyzed by AC, possibly via either (i) the oxidation by hydrogen peroxide produced by oxidative functional groups on the AC surface as was described by Ahumada et al. (2002) or (ii) the direct oxidation by O<sub>2</sub> supplied from the air. In summary, AC was shown effective in (i) continuously oxidizing Fe<sup>2+</sup> to increase  $E_h$  and (ii) weakly reducing Fe<sup>3+</sup> to decrease  $E_h$ , which is contradictory to the  $E_h$  trend observed in bioleaching experiment. It, therefore, indicates that the suppressed  $E_h$  increase during the bioleaching experiment could be the result of Fe<sup>3+</sup>-reduction probably via some redox reaction electrochemically catalyzed by AC, but not the interaction with surface functional groups of AC.

While Fe<sup>3+</sup> and tetrathionate did not react each other (only 0.37 mM Fe<sup>3+</sup> reduction; condition (d); Fig. 5.3a), addition of AC strongly enhanced both the reduction of Fe<sup>3+</sup> (9.2 mM in 6 days; Fig. 5.3a) and oxidation of tetrathionate (10.5 mM sulfate production; in Fig. 5.3c); thus  $E_{\rm h}$  continuously decreased from 826 mV (day 0) to 621 mV (day 6) (condition (e); Fig. 5.3b). Considering the weak Fe<sup>3+</sup>-reduction capability of AC, the presence of tetrathionate played the key role to reduce Fe<sup>3+</sup> to Fe<sup>2+</sup>, proving that electrochemical redox reaction catalyzed by AC resulted in the suppressed  $E_{\rm h}$  increase. Additionally, Fe<sup>3+</sup> was not greatly reduced in the presence of yeast extract as an electron donor (condition (f); Fig. 5.3a), suggesting that RISCs must be the major electron donor for the coupling reaction.

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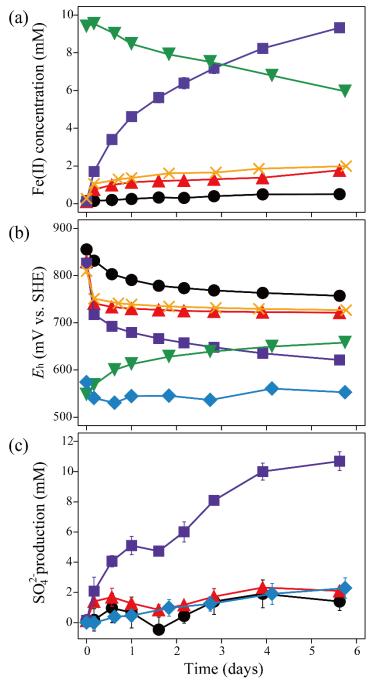


Fig. 5.3 Changes in the Fe<sup>2+</sup> concentration (a),  $E_h$  (b), and sulfate production (c) during abiotic experiment for evaluation of catalytic capability of AC. Cultures containing 0.1% (w/v) AC + Fe<sup>3+</sup> ( $\bigstar$ ; condition (a)), 0.1% AC + Fe<sup>2+</sup> ( $\blacktriangledown$ ; condition (b)), 0.1% AC + tetrathionate ( $\diamondsuit$ ; condition (c)), Fe<sup>3+</sup> + tetrathionate (O; condition (d)), 0.1% AC + Fe<sup>3+</sup> + tetrathionate ( $\blacksquare$ ; condition (e)), or 0.1% AC + Fe<sup>3+</sup> + yeast extract ( $\times$ ; condition (f)) were tested. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

This hypothesis was also checked in the biotic experiment using Fe-oxidizing microorganism without As-oxidizing and S-oxidizing capability, Am. ferrooxidans ICP. Although the concentration is thought insufficient to keep lowering  $E_{\rm h}$  during bioleaching, As(III) was also tested as an electron donor to evaluate the possibility of AC-catalyzed As(III)-oxidation for the enhancement of As immobilization. In the absence of AC, both tetrathionate and As(III) were little oxidized by  $Fe^{3+}$  (less than 5%) of oxidation ratio in both cases), whereas the presence of 0.2% AC greatly facilitate their oxidations, achieving 78% (tetrathionate) and 24% (As(III)) at day 4 (Fig. 5.4). Even though suppressed  $E_{\rm h}$  increase was hardly visible due to the robust and continuous Fe<sup>2+</sup>-oxidation by Am. ferrooxidans ICP (data not shown), the facilitated oxidations proved that the coupling reaction on the AC surface indeed occurs even in the presence of microorganisms. Moreover, it was confirmed that As-oxidation could be the counterpart of the coupling reaction on the AC surface, likely contributing to As immobilization during bioleaching. Consequently, the catalytic mechanism of AC in the  $E_h$  control was summarized as follows; (i) the short-term oxidation by surface functional groups ( $E_h$  rising), (ii) continuous oxidation of Fe<sup>2+</sup>, RISCs, As(III) by hydrogen peroxide or  $O_2$  ( $E_h$  rising), and (iii) Fe<sup>3+</sup> reduction coupled with As(III) and, especially, RISCs oxidation ( $E_h$  lowering). It was thus concluded that Fe<sup>3+</sup>-reduction coupled with tetrathionate oxidation is much favorable than Fe<sup>2+</sup>-oxidation by above reactions (i) and (ii), thus  $E_h$  increase was suppressed in the presence of AC during bioleaching.

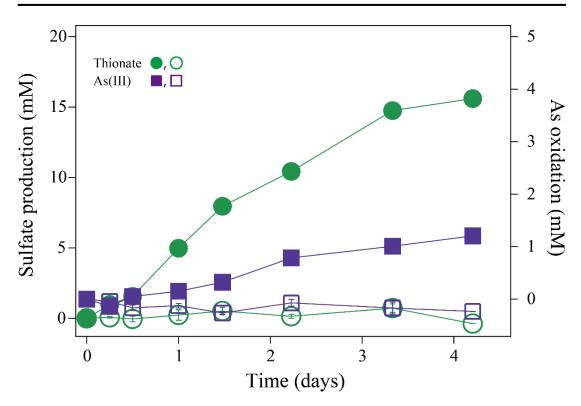
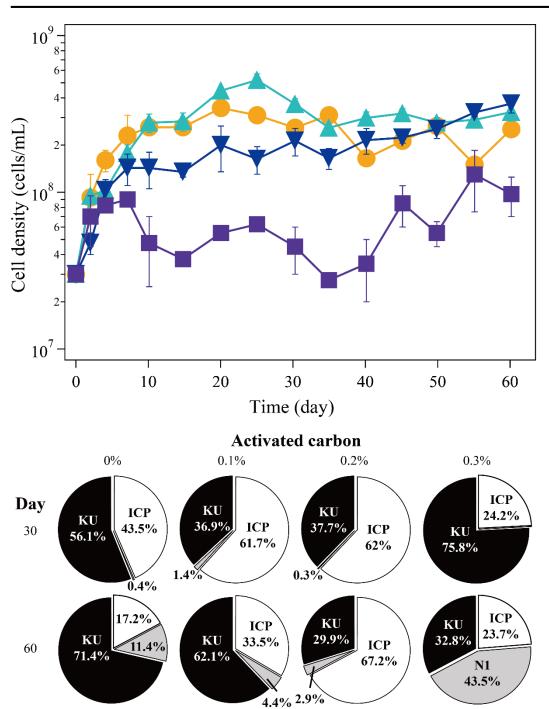


Fig. 5.4 Changes in oxidation ratio of tetrathionate  $(\bigcirc, \bullet)$  and As(III)  $(\Box, \bullet)$  during the biotic experiment for evaluation of catalytic ability of AC in the absence (open symbol) or presence (closed symbol) of 0.2% AC (closed symbol). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

#### 5.3.3 Modification of microbiological population structure by AC addition

It was found that planktonic cell density gradually decreased with the addition of AC (Fig. 5.5), implying that the presence of AC could show some inhibitory effect on cell growth. In order to clarify its effect, Real-Time PCR analysis was carried out to trace the chronological change in the microbiological population structure in the absence and presence of AC. In the absence of AC, the abundance of S-oxidizing At caldus KU and Fe-oxidizing Am. ferrooxidans ICP were competitive at day 30 (56.1% and 43.5%, respectively), which changed into 71.4% (KU) and 17.2% (ICP) at day 60 (Fig. 5.5). At the same time, the abundance of Fe- and S-oxidizing Sb. sibiricus N1 became noticeable by increasing its ratio from 0.4% (day 30) to 11.4% (day 60; Fig. 5.5), implying that S-oxidizing bacteria actively grew in the middle to end stage of the experiment. However, the addition of AC suppressed the growth of S-oxidizer; 0.1% and 0.2% AC dropped the abundance of At caldus KU into 36.9% and 37.7%, respectively (day 30). Especially at 0.2% AC, At caldus KU was not the dominant species even at day 60 (only 29.9%), whereas Fe-oxidizing Am. ferrooxidans ICP possessed the largest population (67.2%). RISCs-consumption by coupling reaction (Fe<sup>3+</sup>-reduction coupled with RISCs-oxidation) on the AC surface attributed to the lack of energy source for the growth of S-oxidizer, which might be the reason of decrease in the abundance of At caldus KU. This modification of the microbial population structure also proved that the coupling reaction certainly occurred during bioleaching of enargite.

Since cell growth was strictly inhibited in the presence of 0.3% AC (Fig. 5.5), the result of Real-Time PCR analysis was not consistence with that obtained in the other cultures.



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Fig. 5.5 Changes in planktonic cell density during bioleaching of enargite concentrate in the presence of 0% ( $\bigcirc$ ), 0.1% ( $\blacktriangle$ ), 0.2% ( $\checkmark$ ), and 0.3% (w/v) AC ( $\blacksquare$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols. Microbial population structure on day 30 and 60 in bioleaching cultures of enargite concentrate at 0%, 0.1%, 0.2%, and 0.3% (w/v) of AC are also depicted.

# 5.3.4 Contribution of galvanic interaction to enargite dissolution

Galvanic interaction is well-known as the electrochemically catalytic effect of carbon material on the dissolution of refractory copper sulfides. While its catalytic capability has been recognized, especially in the AC-catalyzed chalcopyrite bioleaching (Nakazawa et al., 1998; Zhang et al., 2007; Liang et al., 2010), no study has indeed confirmed the existence of catalytic galvanic current. In this study, electrochemical analysis was therefore carried out with the aim to indirectly observe the galvanic current and evaluate its catalytic capability.

Fig. 5.6a shows the electrode potential of each mineral electrode in various potential solutions. Every electrode potential constantly increases accompanied with the  $E_h$  increase in the range from 0.5 V to 0.7 V. However, once  $E_h$  becomes higher than 0.75 V, electrode potentials of enargite and AC were not able to keep up with the increase in  $E_h$ , while pyrite electrode still shows the same potential with  $E_h$ . At around 0.8 V, each electrode potential finally reached almost stationary value of 0.72 V (enargite), 0.74 V (AC), and 0.81 V (pyrite), followed by slight increase in electrode potential at further higher  $E_h$  (> 0.8 V). Since the difference in electrode potential of each mineral corresponds to the galvanic electromotive force, it is expected that the higher  $E_h$  range (> 0.75 V) is favorable to facilitate the galvanic reaction. Furthermore, pyrite showed the highest electrode potential, followed by AC and enargite, in the range of  $E_h$  being achievable during bioleaching, suggesting that pyrite-enargite system would cause a stronger galvanic effect than AC-enargite system.

Galvanic current measurement confirmed that the pyrite-enargite system indeed showed higher current value than AC-enargite system in the bioleaching  $E_h$  range (0.6 – 0.85 V; Fig. 5.6b). Moreover, the galvanic current of AC-enargite system was negligibly small (< 1mA) at the lower  $E_h$  range (< 0.7 V) than the higher  $E_h$  range (> 0.7 V), where enargite dissolution was promoted during bioleaching. Conclusively, enargite dissolution is unlikely catalyzed by galvanic interaction between enargite and AC at which Cu steadily solubilized during the bioleaching experiment.

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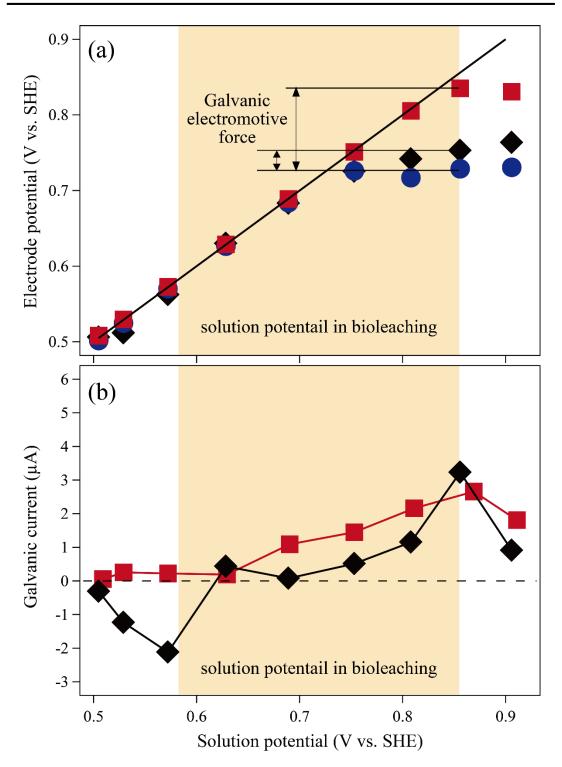


Fig. 5.6 Relationship between solution potential ( $E_h$ ) and electrode potential (a) of enargite ( $\bigcirc$ ), pyrite ( $\blacksquare$ ), and AC ( $\blacklozenge$ ), or galvanic current (b) in enargite-pyrite ( $\blacksquare$ ) or enargite-AC ( $\diamondsuit$ ) system. Difference in the electrode potential between minerals corresponds to the galvanic electromotive force.

#### 5.3.5 Kinetic study in AC-catalyzed bioleaching of enargite concentrate

The shrinking core model is frequently utilized to model the mineral dissolution process. This has been indeed used in the chalcopyrite and enargite bioleaching by Masaki et al. (2018) and Oyama et al. (2018), confirming its applicability even to bioleaching. Since it was found that enargite dissolution was negligibly enhanced by the galvanic interaction between AC and enargite, shrinking core model was employed in this study for modeling the dissolution behavior to disclose the factors affecting on the improved final Cu recovery.

In the abiotic cultures, Cu dissolution behavior in the absence of AC was well-fit to diffusion through production film model, while that in the presence of 0.3% AC showed slightly better fitting to the surface chemical reaction model, known as faster dissolution model than the other, throughout the experiment (Fig. 5.7). Kinetic constant, k, greatly increased from 0.00007 (without AC) to 0.0014 (0.3% AC; Table 5.2), indicating that AC addition indeed accelerated the enargite dissolution by modifying the dissolution mechanism; facilitated oxidation by Fe<sup>3+</sup> produced via AC-catalyzing Fe<sup>2+</sup> oxidation to Fe<sup>3+</sup> as was described in section 5.3.1.

On the other hand, all biotic cultures were rate-limited by surface chemical reaction model but not diffusion through product film model, implying that the fundamental reaction mechanism would be scarcely changed by the addition of AC (Fig. 5.7a). Contrary to abiotic cultures, kinetic constant became gradually smaller with the addition of AC from 0.0081 (0% AC) to 0.049 (0.1%), 0.04% (0.2% AC), and 0.0021 (0.3% AC) (Table 5.2); enargite dissolution was not, in fact, accelerated by the addition of AC. This could be due to the lowered  $E_h$  with the addition of AC, while higher  $E_h$  is favorable for faster enargite dissolution (Lattanzi et al., 2008 37). However, the fitting durations were prolonged with the addition of AC from 7 days (0% AC) to 25 days (0.1%), 35 days (0.2%), and 60 days (0.3%); Fig. 5.7a); the fitting was halted at which the correlation factor, R<sup>2</sup>, start to decrease. Since these timings are almost consistent with the initiation of rapid Fe solubilization, deteriorated pyrite solubilization by AC addition would enable to prolong the duration being fit with faster reaction model, surface chemical reaction model. Consequently, improved Cu recovery was resulted from the slower but long and stable Cu solubilization from enargite via the  $E_{\rm h}$ modification by AC.

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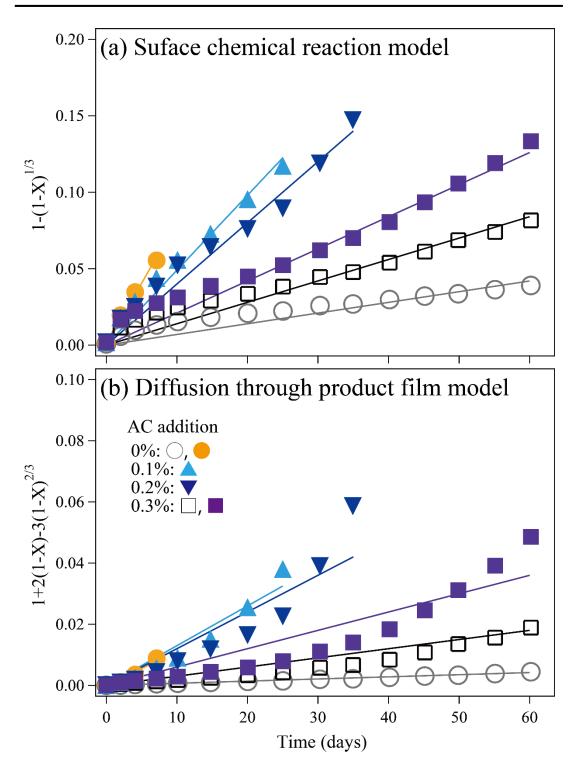


Fig. 5.7 Kinetic modeling on abiotic leaching (open symbol) or bioleaching (closed symbol) of enargite concentrate in the presence of 0% ( $\bigcirc$ ,  $\bigcirc$ ), 0.1% ( $\blacktriangle$ ), 0.2% ( $\checkmark$ ), and 0.3% (w/v) ( $\Box$ ,  $\blacksquare$ ) AC; (a) surface chemical reaction (1 - (1-X)<sup>1/3</sup> =  $k_r$ t) and (b) diffusion through product film (1 + 2(1-X) - 3(1-X)<sup>2/3</sup> =  $k_d$ t). Linear lines were drawn until where R<sup>2</sup> values increase.

Table 5.2 Correlation factor R         diffusion through product film.	ion factor R <sup>2</sup> a product film.	und kinetic constant	k values calculated	using the kinetic r	Table 5.2 Correlation factor $\mathbb{R}^2$ and kinetic constant k values calculated using the kinetic model of surface chemical reaction and diffusion through product film.	mical reaction and
				Reactio	Reaction model	
	AC addition	F1UIT	Surface chemical reaction	ical reaction	Diffusion through product film	gh product film
	(0/)	(uay)	$k_{r}$	$\mathbb{R}^2$	$k_{d}$	$\mathbb{R}^2$
chistic locatine	0	0 - 60	0.0007	0.800	0.00007	0.990
ablouc reactillity	0.3	0 - 60	0.0014	0.928	0.0003	0.923
	0	0 - 7	0.0081	0.987	0.0011	0.932
	0.1	0 - 25	0.0049	0.974	0.0013	0.930
UNICACIIIIS	0.2	0 - 35	0.0040	0.969	0.0012	0.855
	0.3	0 - 60	0.0021	0.967	0.0006	0.860

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# 5.3.6 Arsenic solubilization and immobilization during bioleaching with and without AC

The behavior of As (dissolution and immobilization) is also one of the most important factors in enargite leaching. In the abiotic cultures, As solubilization was negligible (< 3% in the absence and presence of AC; Fig. 5.8a) and the majority of once-dissolved As was immediately immobilized throughout the experiment (75% and 94% As immobilized in the absence and presence of AC, respectively; Fig. 5.8a and 5.8b). Slow dissolution of enargite resulted in the small amount of As supplied into the solution, which could be successively immobilized via the co-precipitation with Fe. On the other hand, As solubilization was visible in the biotic cultures (except for the culture in the presence of 0.3% AC) due to the faster dissolution of enargite than abiotic cultures, reaching 24%, 29%, 35%, 3% As dissolution at day 60 in the a presence of 0, 0.1, 0.2, and 0.3% AC, respectively (Fig. 5.8a). However, the addition of AC enables to delay the initiation of As dissolution from day 10 (0% AC) to 30 (0.1%) and 40 (0.2%), and almost no As solubilization was observed until the end of the experiment at 0.3% AC (Fig. 5.8a).

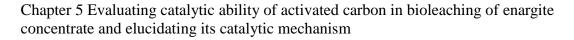
Fig. 5.8b shows the immobilized As concentration in each culture calculated by the following equation;

As immobilized (mM) = Total Cu dissolved (mM) / 3 - Total As dissolved (mM) (Eq. 7-3)

Regardless of the absence or presence of AC, the amount of As immobilized once increased with time to reach the highest amount of 3.1 mM (0% AC at day 10), 5.2 mM (0.1% at day 30), 7.0 mM (0.2% at day 40), and 6.9 mM (0.3% at day 60), corresponding to 77%, 70%, 77%, and 92% of immobilization ratio, respectively (Fig. 5.8b). However, it later started to decrease at day 10 (0%), 30 (0.1%), and 40 (0.2%), resulting in < 40% As immobilization at day 60 in each case; in the presence of 0.3% AC, As immobilization constantly increased throughout the experiment. The initiation of the decrease in As immobilization was consistent with that of the As solubilization into the solution (Fig 5.8a and 5.8b), suggesting that the once-immobilized As was likely re-solubilized.

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EPMA analysis was carried out to understand the As immobilization form and its resolubilization mechanism. Bioleaching residues of 0.2% AC culture at day 30 and day 60 were collected to obtain the "before As re-solubilization" and "after As resolubilization" samples (indicated in Fig. 5.8b), respectively. In the former sample, enargite grains covered with some thin layer  $(1-3 \mu m)$  were uniformly found (Fig. 5.8b), which completely disappeared in the latter sample (Fig. 5.8c), alternatively forming jarosite (KFe<sub>3</sub>(OH)<sub>6</sub>(SO<sub>4</sub>)<sub>2</sub>) as a major secondary mineral. Elemental mapping analysis revealed that the thin layer was composed of Fe, As, and O, corresponding to ferric arsenate (FeAsO<sub>4</sub>; Fig. 5.9). This observation suggests that dissolved As successively co-precipitates with Fe on the surface of enargite to form amorphous ferric arsenate layer, which was later re-solubilized to release As and Fe into the solution again, thus resulting in the decrease in As immobilization. It was expected that some As would be still immobilized by co-precipitating with jarosite, which was observed as the majority of secondary mineral in "after As re-solubilization" sample. The re-solubilization could be triggered by the dissolution of pyrite, since the initiation of As re-solubilization was almost accompanied by that of rapid Fe dissolution (Fig. 5.1b). It has been reported that sulfate ion is likely involved in the dissolution-recrystallization process of Asbearing precursor to finally form highly crystalline scorodite (FeAsO<sub>4</sub>·2H<sub>2</sub>O; Tanaka et al., 2018). Large amount of sulfate ion supplied by rapid pyrite dissolution would thus hinder the stabilization of once-immobilized ferric arsenate by transferring the chemical equilibrium toward the formation of ferric sulfate such as jarosite. Stabilization of ferric arsenate and its transformation into highly crystalline scorodite might be achievable by the optimization of AC addition to maintain the  $E_h$  level to <700 mV throughout the experiment for completely suppressing the sulfate solubilization from pyrite.



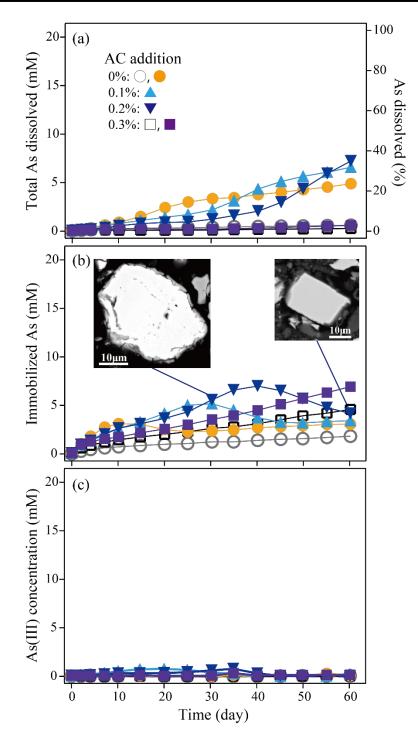
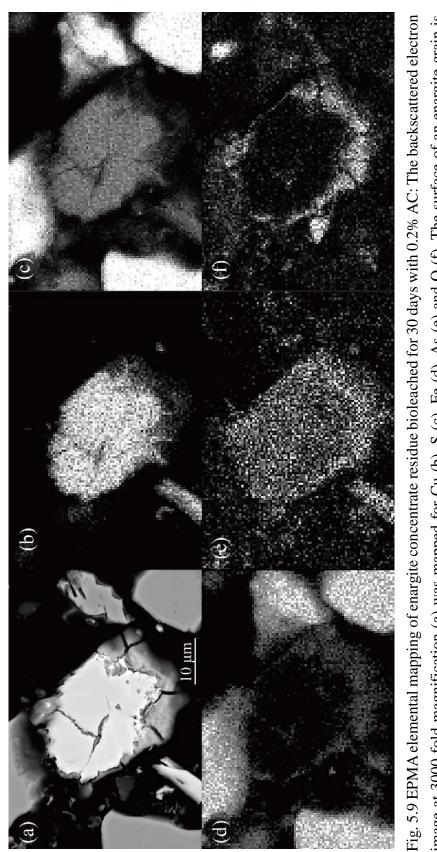


Fig. 5.8 Changes in the concentration of total soluble As (a), immobilized As (b), and soluble As (III) (c) during abiotic leaching (open symbol) or bioleaching (closed symbol) of enargite concentrate at 0% ( $\bigcirc$ ,  $\bigcirc$ ), 0.1% ( $\blacktriangle$ ), 0.2% ( $\checkmark$ ), or 0.3% (w/v) ( $\Box$ ,  $\blacksquare$ ) of AC. Backscattered electron image of an enargite grain bioleached for 30 or 60 days with 0.2% (w/v) AC at the 2700-fold or 1000-fold magnification was also depicted, respectively. White brighter grain (enargite) was covered with gray layer at day 30, which disappeared at day 60.



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image at 3000-fold magnification (a) was mapped for Cu (b), S (c), Fe (d), As (e) and O (f). The surface of an enargite grain is covered with Fe-, As-, O-containing secondary mineral, ferric arsenate.

#### **5.4 Conclusions**

Based on the overall findings, the mechanism of AC-catalyzed bioleaching of enargite concentrates is proposed in Fig. 5.10.

The presence of AC suppresses the  $E_h$  increase via the coupling reaction (Fe<sup>3+</sup>reduction and RISCs-oxidation) on the AC surface acting as an electron mediator (i). This  $E_h$  lowering effect by AC deteriorates the initiation of pyrite dissolution (ii), which starts to dissolve when  $E_h$  reaches to 700 mV. At the same time, enargite dissolution is also slightly slowed down according to the addition of AC, since high  $E_h$  is favorable for the faster dissolution. The galvanic interaction between enargite and AC negligibly contributes to Cu solubilization at the lower  $E_h$  level. However, suppressed pyrite dissolution results in the less passivation of enargite with Fe precipitates such as jarosite, consequently leading to the steady and long Cu solubilization (iii).

Once dissolved As from enargite is successively and immediately immobilized as ferric arsenate selectively on the enargite surface (iv). However, large amount of sulfate supplied from rapid pyrite dissolution would destabilize the ferric arsenate by shifting the chemical equilibrium toward the formation of ferric sulfate such as jarosite. As a result, As re-solubilization occurs to release As into the solution again, and some of them co-precipitates with jarosite (v).

This proposed mechanism suggests that completely suppressed pyrite dissolution is a key point to realize much longer Cu solubilization and the stabilized As immobilization. Therefore, further investigation on the catalytic ability of AC will be beneficial to completely prevent pyrite dissolution by maintaining the  $E_h$  less than 700 mV.

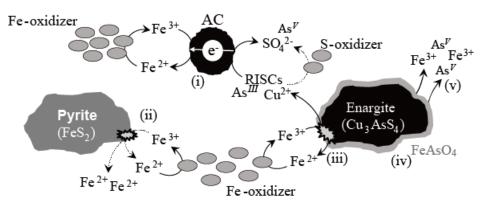


Fig. 5.10 The schematic image of overall mechanism of AC-catalyzed bioleaching of enargite concentrate.

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### Chapter 6

# Physicochemical properties determining the catalytic ability of activated carbon

#### Abstract

To clarify the property determining the  $E_{\rm h}$ -control ability of AC, 8 types of AC (Apowder, B-granular, B-powder, C-powder, D-powder, E-powder, F-powder, and Gpowder) with the variety of surface property were compared in the abiotic experiment. Three AC (A-powder, B-granular, and B-powder) were also used in the bioleaching experiment for further understanding of AC-catalyzing mechanism. Series of the test revealed that Fe<sup>3+</sup>-reduction coupled with the oxidation of tetrathionate was greatly facilitated by using chemical-activated carbon (A-powder and G-powder), rather than steam-activated carbon. Raman spectroscopy analysis revealed that the well-developed graphene structure in the former type of AC was likely the reason of its superiority as an electron mediator, leading to the strongest  $E_{\rm h}$ -reducing ability. Other parameters such as specific surface area, total pore volume, size, activation degree, and raw material were found negligibly influential in E<sub>h</sub>-control ability. Even in the bioleaching experiment, the utility of chemical-activated carbon (A-powder) was confirmed as an  $E_{\rm h}$ -controlling catalyst. Moreover, faster dissolution behavior of enargite was retained by using powder AC, while it was slowed down when granular AC was used. High contact frequency of the former AC would facilitate enargite dissolution, likely canceling out the slowed enargite dissolution due to the AC-catalyzed  $E_{\rm h}$ -reduction. In summary, powder AC produced by chemical activation was found the most suitable for AC-catalyzing bioleaching of enargite concentrate.

#### 6.1 Introduction

In order to accelerate the dissolution of refractory copper sulfides such as chalcopyrite (CuFeS<sub>2</sub>) and enargite (Cu<sub>3</sub>AsS<sub>4</sub>), a promising catalyst which is applicable to the bioleaching process has been sought in decades. Silver is one of the candidates, actively studied by a number of researcher's so far especially in the chalcopyrite bioleaching system (Ahonen et al., 1990; Ballester et al., 1990; Gómez et al., 1999; Sato et al., 2000; Yuehua et al., 2002; Muñoz et al., 2007; Johnson et al., 2008; Feng et al., 2013; Abdollahi et al., 2015; Xia et al., 2018). Regardless of its strong catalytic ability, however, other possibilities must be found due to the economic infeasibility of silver-utilization in real operation.

As an alternative, carbon materials such as graphite or AC are considered useful (Hao et al., 2018). Possible utility of AC was indeed confirmed in previous chapter 5 in this thesis, where the final Cu recovery was improved with AC addition during bioleaching of enargite concentrate based on the indirect catalysis mechanism; AC act as an  $E_{\rm h}$ -controlling catalyst to prevent unwanted pyrite dissolution, enabling slower but steady dissolution of enargite without Fe passivation. Although Fe<sup>3+</sup> reduction coupled with RISCs oxidation on the AC surface was found the key reaction of AC-catalyzed  $E_{\rm h}$ -control, the property determining the  $E_{\rm h}$ -controlling ability of AC is still unclear.

The effected of specific surface area have been tested by comparing graphite and AC with various specific surface area (Hao et al., 2018). Even though electrical conductivity of graphite (0.6 S/m) is rather higher than that of the others (0.1 S/m), AC with the highest specific surface (1200 m<sup>2</sup>/g) performed the strongest  $E_h$ -reduction in bioleaching of complex copper ores, proving the importance of the specific surface area. Jahromi et al. (2018) modified the surface functional groups on the AC surface with sulfuric acid, hydrochloric acid, and nitric acid to investigate the effect of varied surface functional groups on abiotic enargite leaching. It clarified that the modification with different acid changed the abundance of oxidative functional groups on the AC surface such as quinone and carboxyl groups. These oxidative functional groups are catalytically capable of producing H<sub>2</sub>O<sub>2</sub> via the following equations, proposed by Ahumada et al., (2002);

Chapter 6 Physicochemical properties determining the catalytic ability of activated carbon

$$2C_{red} + O_2 + 2H_2O = 2H_2O_2 + 2C_{ox}$$
(Eq. 6-1)

$$2Fe^{2+} + H_2O_2 + 2H^+ = 2Fe^{3+} + 2H_2O$$
 (Eq. 6-2)

 $C_{red}$  and  $C_{ox}$  indicate that surface functional groups on the surface of AC. This H<sub>2</sub>O<sub>2</sub> formed in Eq. 6-1 could be consumed to oxidize the Fe<sup>2+</sup> to Fe<sup>3+</sup> (Eq. 6-2), possibly shifting  $E_h$  to the higher level. Therefore, surface functional groups must also be considered as one of the properties determining the  $E_h$ -controlling ability of AC.

Moreover, the properties of AC significantly affected on the dissolution kinetics of minerals during the leaching process. Nakazawa et al. (1998) found the necessity of contact with AC to enhance the chalcopyrite dissolution; almost no catalytic ability was noticeable without contact between AC and chalcopyrite. This suggests that the particle size (or shape) of AC must be finer to maximize the catalytic ability of AC by increasing the contact frequency. Besides this, other parameters such as pore size, pore volume, raw material, and activation method would determine the catalytic ability of AC.

This chapter, therefore, aimed to find the most crucial property determining the catalytic ability of activated carbon. Series of abiotic and biotic tests were carried out to compare the various AC with varied surface and structural properties. The obtained information would be summarized for a further comprehensive understanding of AC-catalyzed bioleaching of enargite concentrate.

#### 6.2 Materials and methods

#### 6.2.1 Comparison of granular and powder AC

In order to evaluate the effect of AC-shape (granular or powder) on redox reactions occurring on the surface of AC, three AC, powder AC, granular AC (used in chapter 5), and crushed granular AC (hereinafter, referred to as A-powder, B-granular, B-powder, respectively; purchased from Wako) were employed; B-powder was prepared by crushing the B-granular so as to set its particle size to be similar with A-powder. Material property and pore size distribution of each AC were summarized in Table 6.1 and Fig. 6.1. A-powder and B-powder were also used for the analyses by Raman spectroscopy and ATR-FT-IR.

ABS medium (100 mL; pH adjusted to 2.0 by using 1 M H<sub>2</sub>SO<sub>4</sub>) was added into the 300 mL of Erlenmeyer flask. Each type of AC at the pulp density of 0.1% (w/v), 10 mM Fe<sup>2+</sup> or Fe<sup>3+</sup>, and/or 5 mM of tetrathionate were respectively added into the medium to prepare the experimental cultures listed below. These flasks were incubated and shaken at 45°C and 150 rpm, respectively. Solution samples were regularly withdrawn to monitor pH,  $E_h$ , Fe<sup>2+</sup> and total Fe concentration (*o*-phenanthroline method), and SO<sub>4</sub><sup>2-</sup> concentration (turbidimetric method).

1	10 mM Fe <sup>3+</sup> + 5 mM tetrathionate	+ 0.1% A-powder
		+ 0.1% B-granular
		+ 0.1% B-powder
2		+ 0.1% A-powder
	10 mM Fe <sup>3+</sup>	+ 0.1% B-granular
		+ 0.1% B-powder
3		+ 0.1% A-powder
	10 mM Fe <sup>2+</sup>	+ 0.1% B-granular
		+ 0.1% B-powder
4		+ 0.1% A-powder
	5 mM tetrathionate	+ 0.1% B-granular
		+ 0.1% B-powder

Chapter 6 Physicochemical properties determining the catalytic ability of activated carbon

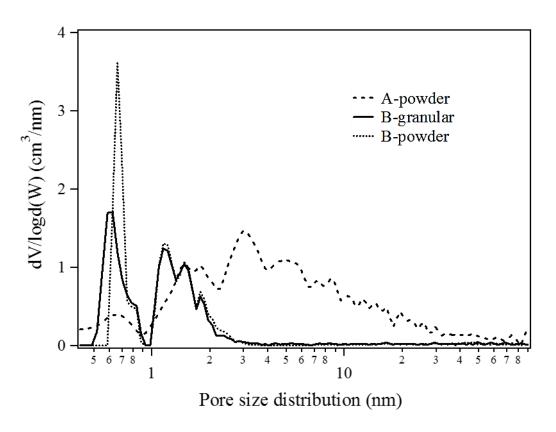


Fig. 6.1 Pore size distribution of A-powder, B-granular, and B-powder.

	A-powder	B-granular	B-powder
Specific surface Area (m <sup>2</sup> /g)	1429	1212	1261
Total pore volume (cm <sup>3</sup> /g)	1.33	0.54	0.57
Average pore diameter (nm)	3.71	1.77	1.81
Average particle size (µm)	42.2	5000	237.8
Raw material	Woody chip	Coconut shell	Coconut shell
Activation	Chemical-activated	Steam-activated	Steam-activated

Table 6.1. Material properties of A-powder, B-granular, and B-powder.

#### 6.2.2 Comparison of other AC with various properties

For further discussion, other types of powder AC (C-powder, D-powder, E-powder, Fpowder, and G-powder) were also tested in the abiotic condition. Material properties of each AC were summarized in Table 6.2. These were also used for the analyses by Raman spectroscopy and ATR-FT-IR.

ABS medium (100 mL; pH adjusted to 2.0 by using 1 M H<sub>2</sub>SO<sub>4</sub>) was added into the 300 mL of Erlenmeyer flask. Each type of AC at the pulp density of 0.1% (w/v), 10 mM Fe<sup>3+</sup>, and 5 mM of tetrathionate were also added into the medium. These flasks were incubated and shaken at 45°C and 150 rpm, respectively. Solution sample were regularly withdrawn to monitor pH,  $E_h$ , Fe<sup>2+</sup> and total Fe concentration (*o*-phenanthroline method), SO<sub>4</sub><sup>2-</sup> concentration (turbidimetric method).

Table 6.2. Material properties of other types of AC (C-powder, D-powder, E-powder, F-powder, and G-powder).

AC	Raw material	Activation	Specific surface area (m <sup>2</sup> /g)	Total pore volume (mL/g)	Average pore diameter (nm)
C-powder	Coconut shell	Steam-activated	1683	0.807	1.9
D-powder	Coconut shell	Steam-activated	1075	0.483	1.8
E-powder	Woody chip	Steam-activated	959	0.554	2.3
F-powder	Coal	Steam-activated	916	0.454	2.0
G-powder	Woody chip	Chemical-activated	1395	1.243	3.6

#### 6.2.3 Comparison of AC in enargite bioleaching system

Bioleaching of enargite concentrate using A-powder or B-powder were carried out to compare their catalytic ability in biotic condition. HBS media (200 ml in 500 ml flasks; pH adjusted to 2.0 with 1 M H<sub>2</sub>SO<sub>4</sub>) containing 2.0% (4.0 g) enargite concentrate (average particle size: 46.5  $\mu$ m) and 0, 0.02, 0.04, 0.06 and 0.08% (w/v) A-powder or B-powder were prepared and sterilized by autoclaving. Pre-grown culture of each of three strains (*Am. ferrooxidans* ICP, *Sb. sibiricus* N1, and *At. caldus* KU) was centrifuged (9000 rpm, 10 min at 4°C) to collect cells and washed twice with acidified

water (pH 1.7), prior to inoculation. Initial cell density in total was set to  $3.0 \times 10^7$  cells /mL ( $1.0 \times 10^7$  cells /mL for each strain) and 5 mM FeSO<sub>4</sub>·7H<sub>2</sub>O was supplemented for initial cell growth. These flasks were incubated and shaken at 45°C and 150 rpm. Samples were regularly withdrawn to monitor pH,  $E_h$ , cell density, and concentrations of Fe<sup>2+</sup> (*o*-phenanthroline method), As(III) (molybdenum blue method), and total Fe, As, and Cu (ICP-OES). Finally, the obtained data in this bioleaching experiment was compared with that obtained in chapter 5, bioleaching of enargite concentrate using B-granular as an AC catalyst.

#### 6.3 Results and discussion

#### 6.3.1 Catalytic reaction affected by the shape of AC

In this abiotic experiment, three different AC were employed to compare the difference in physical property: (i) A-powder is a powder AC (average size: 42  $\mu$ m) made from woody chip by chemical-activation, (ii) B-granular is a granular AC (average size: around 5000  $\mu$ m) made from coconut shell by steam-activation, (iii) B-powder is a powder AC (average size: 238  $\mu$ m) obtained by crushing the B-granular. Even though the raw material of each AC are different, the comparison among these AC would enable to evaluate the effect of shape (granular or powder) on AC-catalyzed redox reaction, especially for *E*<sub>h</sub>-controlling effect.

In the presence of Fe<sup>3+</sup> and tetrathionate with any AC, rapid decrease in  $E_h$  occurred at the beginning of the experiment (Fig. 6.2b). This must be due to the coupling reaction confirmed in chapter 5; Fe<sup>3+</sup>-reduction coupled with tetrathionate-oxidation on the AC surface acting as an electron mediator. The other trends, decrease in pH, increase in SO<sub>4</sub> production, and increase in acid production, also proved that tetrathionate indeed plays a role as an electron donor for Fe<sup>3+</sup>-reduction (Fig. 6.2a,e,f) regardless of AC type. In the culture with B-granular, relatively slower kinetics was observed compared to the other two powder AC (Fig. 6.2a,b,c,e,f), suggesting that granular AC inferior to powder AC, possibly in terms of ion-capturing capability; in other words, granular AC is more susceptible to the diffusion of ionic species than the others. However,  $E_h$  in the presence of B-granular was consequently lowered to 620 mV at the end of the experiment, which is as low as that in the presence of B-powder, indicating that long-term  $E_h$ -reduction ability of AC could not be determined by the shape(granular and powder).

Interestingly, the stronger  $E_h$ -reduction ability of A-powder became noticeable in the later stage of the experiment after day 3 (Fig. 6.2b).  $E_h$  reached to significantly low level (557 mV) at the end of the experiment (day 6), accompanied with complete Fe<sup>3+</sup> reduction to Fe<sup>2+</sup> (Fig. 6.2c,d). Based on this fact, A-powder was found the most effective in  $E_h$ -reduction among these three AC. This different  $E_h$  trend between A-powder and B-powder is also evidence that the shape of AC is not the predominant property determining its  $E_h$ -controlling ability.

On the other hand, larger amount of SO<sub>4</sub> was continuously produced in the presence of B-powder throughout the experiment than other cultures, even though smaller amount

of tetrathionate was assumed to be used for the  $Fe^{3+}$ -reduction in this culture. This implies that the surface property of B-powder would be suitable for the oxidative reaction rather than that of A-powder.

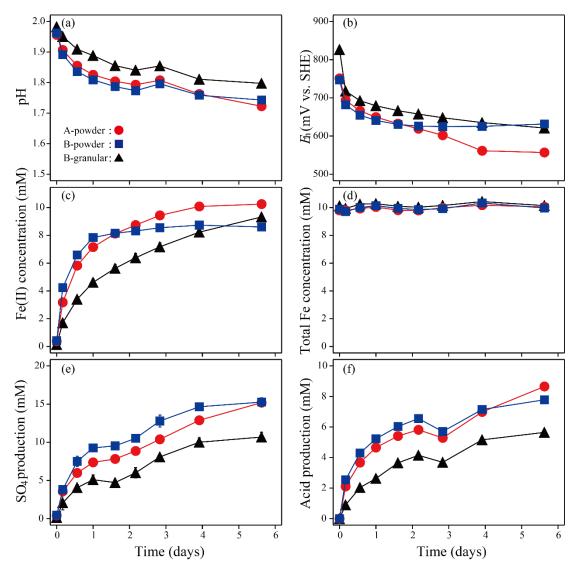
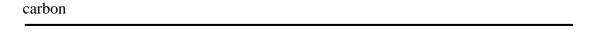


Fig. 6.2 Changes in pH (a),  $E_h$  (b), Fe<sup>2+</sup> concentration (c), total Fe concentration (d), sulfate production (e), and acid production (f) during the abiotic experiment in the presence of 10 mM Fe<sup>3+</sup> and 5 mM sodium tetrathionate for the evaluation of catalytic capability of three AC: A-powder ( $\bigcirc$ ), B-granular ( $\blacktriangle$ ), and B-powder ( $\bigcirc$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

In order to evaluate the oxidative ability of AC itself, cultures containing each one of three AC and either 10 mM Fe<sup>2+</sup> (Fig. 6.3) or 5 mM sodium tetrathionate (Fig. 6.4) were prepared. The results obviously showed that the oxidation of Fe<sup>2+</sup> and tetrathionate were rather promoted in the presence of B-powder (Fig. 6.3c, Fig. 6.4c), confirming that its stronger oxidative ability than A-powder. This might be due to the difference in the surface functional groups on the AC surface. As Eq. 6-1, oxidative type surface functional group such as quinone and carboxyl catalyzes the H<sub>2</sub>O<sub>2</sub> production, which can be consumed for the oxidation of Fe<sup>2+</sup> (Eq. 6-2). Likewise, Fe<sup>2+</sup> and tetrathionate might be oxidized by H<sub>2</sub>O<sub>2</sub> generated on the surface of B-powder. This hypothesis implies that B-powder would possess the larger amount of oxidative type surface functional group such as quinone and carboxyl on its surface than A-powder. The details will be further discussed in the following section based on the analysis of the surface functional group by ATR-FT-IR.

Cultures containing each one of three AC and 10 mM Fe<sup>3+</sup> were also prepared to evaluate the reductive ability of AC itself (Fig. 6.5). Contrary to the culture evaluating the oxidative ability of AC (Fig. 6.3, 6.4), the difference in Fe<sup>3+</sup>-reducing ability among three AC was not explicit;  $E_h$  reached to the stable phase (around 720 mV) at the beginning of the experiment in any cases (Fig. 6.5b). Since rapid  $E_h$  drop until day 1 is likely the result of the reaction between Fe<sup>3+</sup> and the surface functional group (Fig. 6.5b,c), it was expected that each AC possesses the similar reductive type surface functional group on their surface.

In summary, the difference in the shape of AC (granular or powder) was found less influential in  $E_h$ -controlling ability of AC. Based on the experimental results, although A-powder showed the best  $E_h$ -reducing ability among three AC, the key factor determining the  $E_h$ -controlling ability of AC is still unclear, thus requiring a further discussion about the properties of AC.



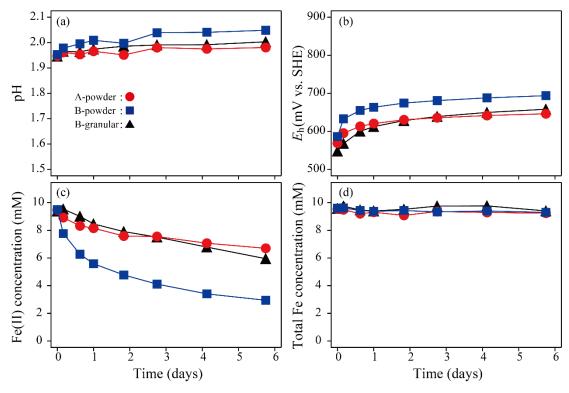
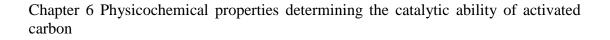


Fig. 6.3 Changes in pH (a),  $E_h$  (b),  $Fe^{2+}$  concentration (c), and total Fe concentration (d), during the abiotic experiment in the presence of 10 mM Fe<sup>2+</sup> for the evaluation of catalytic capability of three AC: A-powder ( $\bigcirc$ ), B-granular ( $\blacktriangle$ ), and B-powder ( $\square$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



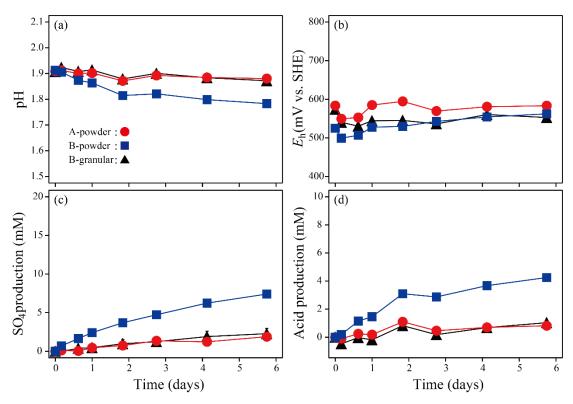
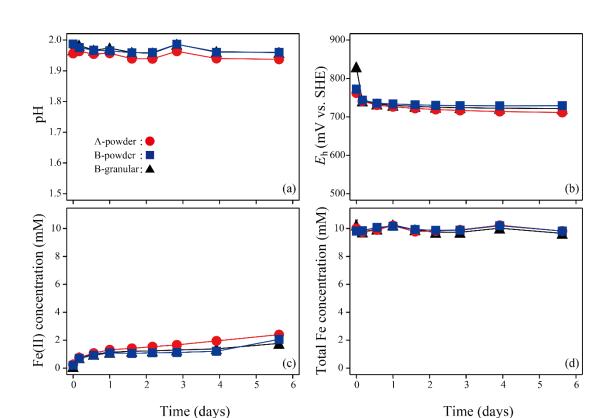


Fig. 6.4 Changes in pH (a),  $E_h$  (b), sulfate production (c), and acid production (d), during the abiotic experiment in the presence of 5 mM sodium tetrathionate for the evaluation of catalytic capability of three AC: A-powder ( $\bigcirc$ ), B-granular ( $\blacktriangle$ ), and B-powder ( $\bigcirc$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



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Fig. 6.5 Changes in pH (a),  $E_h$  (b), Fe<sup>2+</sup> concentration (c), and total Fe concentration (d), during abiotic experiment in the presence of 10 mM Fe<sup>3+</sup> for the evaluation of catalytic capability of three AC: A-powder ( $\bigcirc$ ), B-granular ( $\blacktriangle$ ), and B-powder ( $\Box$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

## **6.3.2** Further comparison of AC properties (specific surface area, pore volume, raw material, and activation method)

Based on the comparison of A-powder, B-granular, and B-powder in the previous section, it was found that  $E_h$ -reduction ability of AC was not affected by the shape of AC (granular or powder). In order to specify the property determining the  $E_h$ -controlling ability of AC, further investigation was carried out by comparing five different powder AC as listed in Table 6.2. Since C-powder possesses larger specific surface area (1683 m<sup>2</sup>/g) and total pore volume (0.807 mL/g) than D-powder (1075 m<sup>2</sup>/g of specific surface area and 0.483 mL/g of total pore volume), the effect of activation degree is able to be clarified through the comparison of them; the former was activated with higher temperature than the latter. The difference of raw material was also studied using D-powder, E-powder, and F-powder made of coconut shell, woody chip, and coal, respectively. Although both E-powder and G-powder were made of the same raw material, woody chip, activation methods are different (E-powder; steam-activated carbon, G-powder; chemical-activated carbon). This comparison also could provide useful information to clarify the property determining the  $E_h$ -controlling ability of AC.

Fig. 6.6 shows the results of the abiotic test adding each AC into the solution containing 10 mM Fe<sup>3+</sup> and 5 mM tetrathionate. Obvious difference was observed in the presence of G-powder, where  $E_h$  rapidly reduced to the 537 mV in the early stage of the experiment, whereas the other type of AC showed less  $E_h$ -reducing capability. Common property between G-powder and A-powder (the best  $E_h$ -reducing AC in the previous section) is the activation method, indicating that chemical-activated carbon is the most suitable for the  $E_h$ -controlling AC catalyst.

Raman spectrum of each AC showed two main peaks at 1350 cm<sup>-1</sup> and 1600 cm<sup>-1</sup> (Fig. 6.7). The former is known as the D-band, which is derived from the defect and/or edge (= surface functional group) structure of AC, while the latter peak is known as G-band, which is derived from the graphene structure of AC (Fig. 6.8). The  $A_D/A_G$  ratio of chemical-activated carbon (A-powder and G-powder) was much smaller (2.3-2.6; Table 6.3) than that of steam-activated carbon (B-powder, C-powder, D-powder, E-powder, and F-powder; 3.1-4.2; Table 6.3), indicating that graphene structure is well-developed in the chemical-activated carbon. This might be due to the difference in the

activation process between steam- and chemical-activated carbons.

In the steam-activation process, carbon is removed from the structure via its transformation into CO or  $CO_2$  to form fine pores as following equations;

$$C + H_2O \rightarrow CO + H_2O$$
 (Eq. 6-3)

$$C + 2H_2O \rightarrow CO_2 + 2H_2 \tag{Eq. 6-4}$$

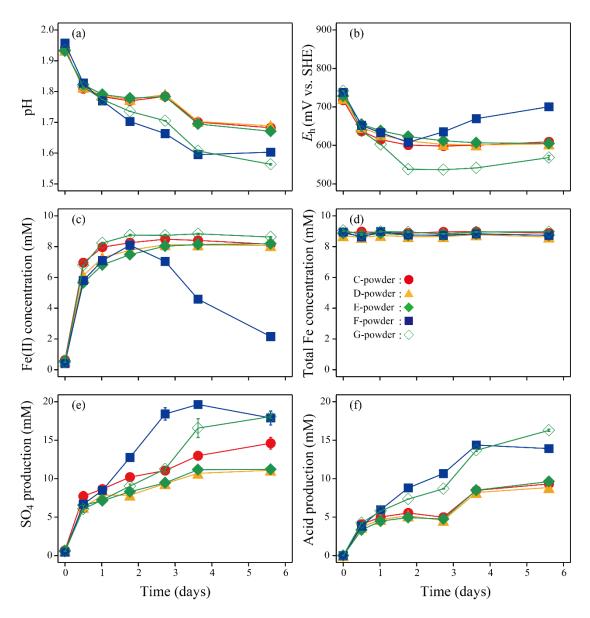
Therefore, graphene structure is selectively decomposed, followed by the formation of finer pores with a large amount of defects (Fig. 6.9), resulting in a relatively bigger  $A_D/A_G$  ratio (Table 6.3).

On the other hand, in the chemical-activation process, fine pore is formed via the dehydration from water-containing organic compounds, but leaving the carbon in the AC structure.

$$n(C_6H_{10}O_5) + ZnCl \rightarrow n(6C + 5H_2O) + ZnCl_2$$
 (Eq. 6-5)

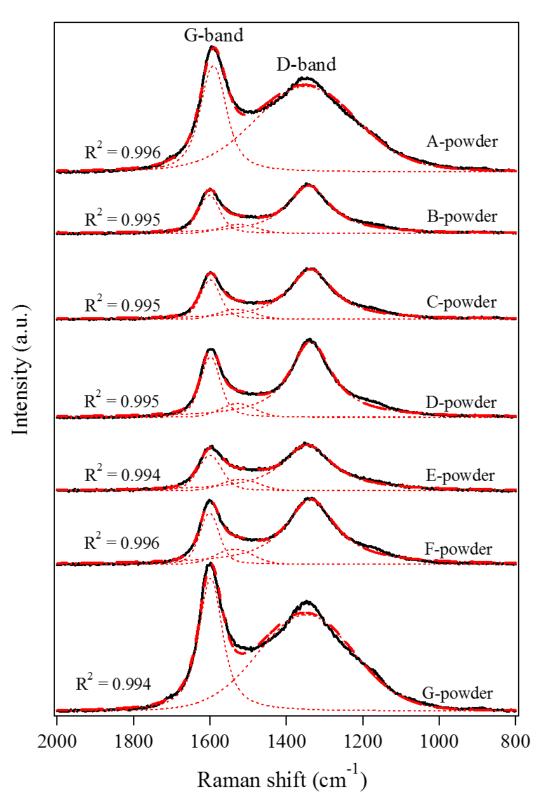
Since the decomposition of graphene structure hardly occurs, relatively coarser defects are formed, resulting in the formation of coarser pores (Fig. 6.10). Remained graphene structure with less defect in the chemical-activated carbon will be the reason of its smaller  $A_D/A_G$  ratio (Table 6.3).

Considering the extremely high electric conductivity of graphene, well-developed graphene structure in the chemical-activated carbon would realize the faster electron transfer mediated by AC. In conclusion, the activated method was found key properties determining the  $E_{\rm h}$ -reducing ability of AC, and chemical-activated carbon (in this experiment, A-powder or G-powder) is considered suitable AC for  $E_{\rm h}$ -controlling catalyst.



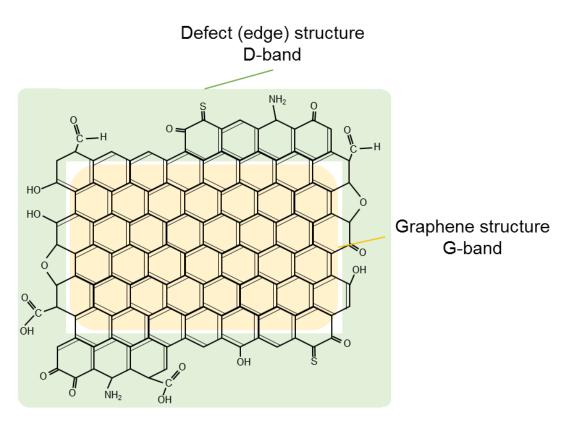
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Fig. 6.6 Changes in pH (a),  $E_h$  (b),  $Fe^{2+}$  concentration (c), total Fe concentration (d), sulfate production (e), and acid production (f) during abiotic experiment in the presence of 10 mM Fe<sup>3+</sup> and 5 mM sodium tetrathionate for the evaluation of catalytic capability of various AC: C-powder ( $\bigcirc$ ), D-powder ( $\blacktriangle$ ), E-powder ( $\diamondsuit$ ), F-powder ( $\blacksquare$ ), and G-powder ( $\diamondsuit$ ). Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



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Fig. 6.7 Raman spectra of various AC (A-powder, B-powder, C-powder, D-powder, E-powder, F-powder, and G-powder). Black solid line and red broken line indicate the original Raman spectra and peak fitting result, respectively.

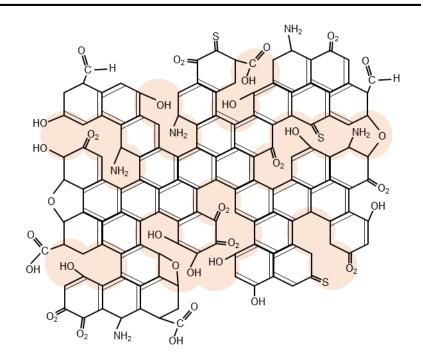


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Fig. 6.8 Schematic image of G-band and D-band structure.

Table 6.3 D-band/G-band ratio of each AC. I<sub>i</sub>, A<sub>i</sub> indicates that fitting peak intensity and area, respectively.

	original	fitt	ing
	$I_D/I_G$	$I_D/I_G$	$A_D / A_G$
A-powder	0.753	0.805	2.627
B-powder	1.127	1.252	3.119
C-powder	1.151	1.253	3.212
D-powder	1.081	1.269	3.449
E-powder	1.032	1.270	4.075
F-powder	1.071	1.287	3.426
G-powder	0.743	0.727	2.263



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Fig. 6.9 Schematic image of steam-activated carbon. Highlighted area with orange color indicates the finer defects formed in the activation process.

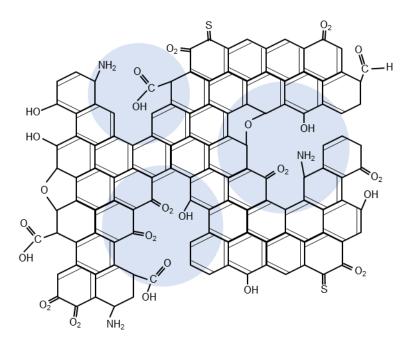


Fig. 6.10 Schematic image of chemical-activated carbon. Highlighted area with blue color indicates the coarser defects formed in the activation process.

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Regarding the C-powder and D-powder, even though the specific surface area of the former (1683  $m^2/g$ ) was rather higher than that of the latter (1075  $m^2/g$ ), almost similar trend of  $E_{\rm h}$  was observed (Fig. 6.6b). Since the difference between two of them is the only activation degree (same activation method and raw material), it was confirmed that E<sub>h</sub>-reducing ability was not determined by activation degree; in other words, specific surface area and total pore volume. Likewise, the difference of raw material (D-powder: coconut shell, E-powder: woody chip) hardly affected on the  $E_h$ -reduction trend. On the other hand, in the culture containing F-powder (made of coal), E<sub>h</sub> started to rapidly increase at day 2 (Fig. 6.6b), accompanied by the continuous oxidation of  $Fe^{2+}$  to  $Fe^{3+}$  until the end of the experiment (Fig. 6.6c). Considering the almost complete consumption of tetrathionate in this case (20 mM of sulfate is theoretically produced when 5 mM of tetrathionate is completely oxidized), it was assumed that tetrathionate-oxidation by H<sub>2</sub>O<sub>2</sub> produced on the AC surface would be the predominant reaction rather than Fe<sup>3+</sup>-reduction coupled with tetrathionate-oxidation. Hence, tetrathoinate would be lacked for continuous Fe<sup>3+</sup>-reduction, resulting in the initiation of  $E_h$  rise via the oxidation of once reduced Fe<sup>2+</sup> to Fe<sup>3+</sup>.

Based on the Eq. 6-1, the presence of large amount of oxidative type surface functional group on the AC surface is thought favorable for  $H_2O_2$  production and following oxidation reaction. In order to clarify the difference of surface functional groups among 7 AC, ATR-FT-IR analysis was conducted (Fig. 6.11); note that FT-IR analysis is often carried out as a qualitative analysis method rather than a quantitative method (Biniak et al., 1997). The bands at around 1700 cm<sup>-1</sup> (1682, 1704, 1752, and 1793 cm<sup>-1</sup>; Fig. 6.11), which were observed in all AC analyses, were likely due to the stretching vibrations of C=O in ketone (derived from carbonyl, quinone, and aldehydes), carboxyl, and anhydride. The other broad peak at 1061 cm<sup>-1</sup> might be assigned to C-O-C bonding in ester (derived from lactone) or ether (Fig. 6.11). Even though slight difference in the peak intensity of these oxidative type surface functional group was observed, notable changes, which is assumed significantly influential on  $H_2O_2$  production ability of AC, was not detected. This resulted in the unclear understanding of the relationship between the oxidative ability of AC and surface functional group on AC.

Unfortunately, the clear difference in surface functional group was not detected by

ATR-FT-IR (Fig. 6.11), though  $A_D/A_G$  ratio of F-powder is indeed the highest among 7 AC tested in this study (Table 6-3), possibly implying that plentiful surface functional groups on the surface of F-powder could be the reason of its stronger oxidative ability. In summary, following reactions are catalyzed by AC with different priority depending on the type of AC;

(i) Fe<sup>3+</sup>-reduction coupled with tetrathionate-oxidation ( $E_h$ -reducing reaction)

(ii)  $Fe^{2+}$ -oxidation (*E*<sub>h</sub>-rising reaction)

(iii) tetrathionate-oxidation (consequently leading to  $E_{\rm h}$ -rise)

Although each reaction could occur in parallel, reaction (i) is basically predominant reaction in the presence of both  $\text{Fe}^{3+}$  and tetrathionate regardless of AC-type. This trend would be more noticeable when chemical-activated carbon is used due to its high performance as an electron mediator based on the high electric conductivity of massive graphene structure. On the other hand, reaction (ii) and (iii) would be strongly promoted by AC made of coal, likely resulting from its plentiful surface functional groups. Overall, it was concluded that chemical-activated carbon is the most desirable  $E_{h-}$  controlling catalyst for the bioleaching process.

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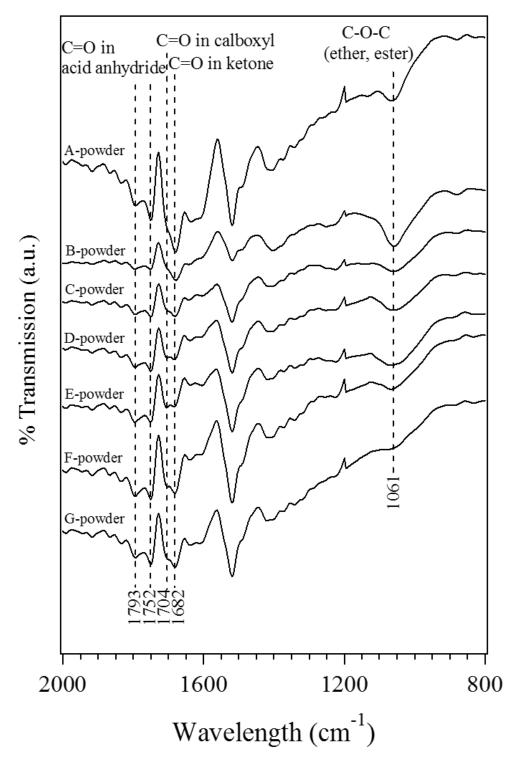
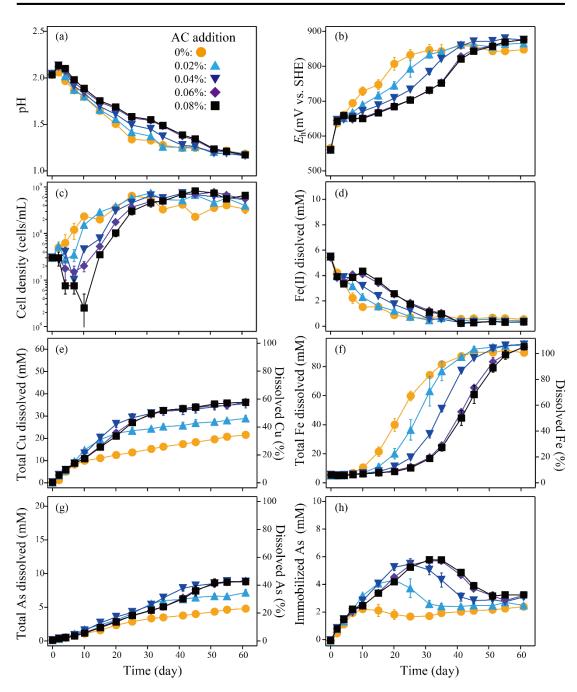


Fig. 6.11 The transmission ATR-FT-IR spectra of various AC (A-powder, B-powder, C-powder, D-powder, F-powder, and G-powder) in the 2000-800 cm<sup>-1</sup> range.

# 6.3.3 Varied catalytic effect of A-powder, B-granular, and B-powder on Cu solubilization and $E_{\rm h}$ -control during bioleaching of enargite concentrate

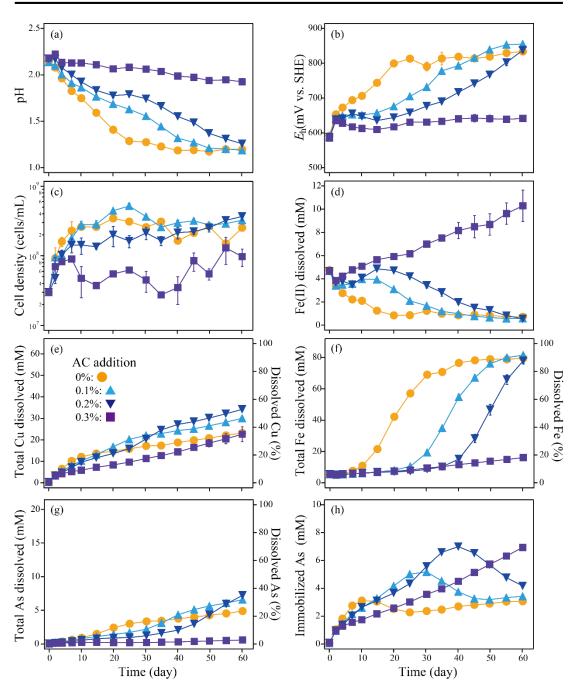
Based on the knowledge obtained by the abiotic test in section 6.3.1 and 6.3.2, the catalytic effect of different AC was evaluated in bioleaching of enargite concentrate. In this study, the AC used in section 6.3.1 (A-powder, B-granular, and B-powder) were also employed, since the contact between enargite and AC, which could contribute to Cu solubilization via the galvanic interaction, must be dominated by the AC size, while  $E_{\rm h}$ -controlling ability was negligibly affected by the shape of AC (granular or powder) in section 6.3.1.

Bioleaching results using A-powder, B-granular, and B-powder as the AC catalyst were summarized in Fig. 6.12, 6.13, 6.14, respectively. In any cases, fundamental phenomena in the presence of each AC were basically same; (i) suppressed  $E_{h}$ -rise (Fig. 6.12b, 6.13b, 6.14b), (ii) deteriorated Fe dissolution (= pyrite dissolution; Fig. 6.12f, 6.13f, 6.14f), (iii) prolonged Cu solubilization (= enargite dissolution; Fig. 6.12e, 6.13e, 6.14e), and (iv) improved As immobilization and its re-solubilization (Fig. 6.12h, 6.13h, 6.14h). Cell density was the only parameter obviously affected by the shape of AC. The sharp decrease in planktonic cell density at the beginning of the experiment was visible in the presence of powder AC (A-powder and B-powder; Fig. 6.12c and 6.14c), which was not confirmed with B-granular (Fig. 6.13c); note that the lowest value of y-axis in Fig. 6.12c and 6.14c was  $10^6$  cells/mL, while that in Fig. 6.13c was  $10^7$  cells/mL. This was likely the result of the difference in contact frequency between microorganisms and AC. Since the number of powder AC particles in solution was extremely higher than that of granular AC, more frequent contacts with the microorganisms occurred, possibly leading to immobilization of cells by attaching on the AC surface.



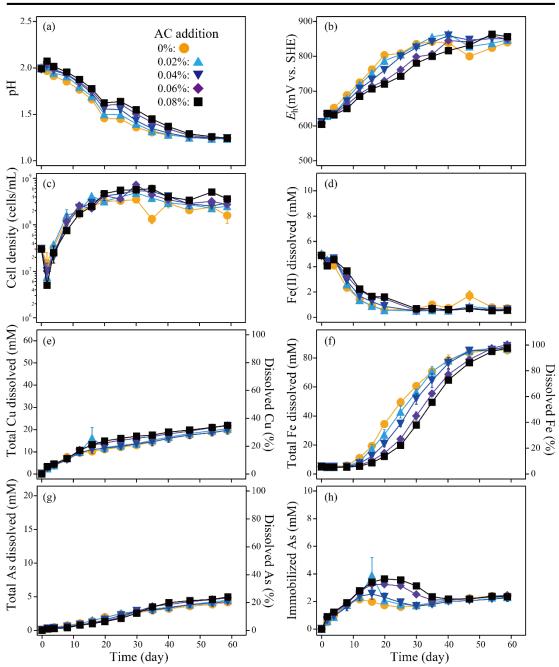
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Fig. 6.12 Summary of results in bioleaching of enargite concentrate in the absence ( $\bigcirc$ ) or presence of 0.02 ( $\triangle$ ), 0.04 ( $\bigtriangledown$ ), 0.06 ( $\diamondsuit$ ), and 0.08% (w/v) ( $\blacksquare$ ) A-powder as the AC catalyst; (a) pH, (b)  $E_{\rm h}$ , (c) cell density , (d) Fe<sup>2+</sup> concentration, (e) total Cu concentration, (f) total Fe concentration, (g) total As concentration, and (f) immobilized As concentration. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



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Fig. 6.13 Summary of results in bioleaching of enargite concentrate in the absence ( $\bigcirc$ ) or presence of 0.1 ( $\triangle$ ), 0.2 ( $\bigtriangledown$ ), and 0.3% (w/v) ( $\blacksquare$ ) B-granular as the AC catalyst; (a) pH, (b)  $E_h$ , (c) cell density , (d) Fe<sup>2+</sup> concentration, (e) total Cu concentration, (f) total Fe concentration, (g) total As concentration, and (f) immobilized As concentration. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.



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Fig. 6.14 Summary of results in bioleaching of enargite concentrate in the absence ( $\bigcirc$ ) or presence of 0.02 ( $\triangle$ ), 0.04 ( $\bigtriangledown$ ), 0.06 ( $\diamondsuit$ ), and 0.08% (w/v) ( $\blacksquare$ ) B-powder as the AC catalyst; (a) pH, (b) *E*<sub>h</sub>, (c) cell density , (d) Fe<sup>2+</sup> concentration, (e) total Cu concentration, (f) total Fe concentration, (g) total As concentration, and (f) immobilized As concentration. Data points are mean values from duplicate cultures. Error bars depicting averages are not visible in some cases as they are smaller than the data point symbols.

For the clear comparison, changes in  $E_h$ , total Cu, Fe, and As concentration in each culture were summarized in Fig. 6.15, respectively. The bioleaching result obtained under similar conditions, in the presence of 0.08% A-powder, 0.08% B-powder, and 0.1% B-granular, were selected for the fair comparison.

Seemingly,  $E_h$  trend was hardly affected by AC-type (Fig. 6.15a), though the difference was more noticeable on the AC-catalyzed  $E_h$ -reduction (Fig. 6.16). Strong  $E_h$ -reduction was maintained by A-powder in the long-term period, proving the superiority of chemical-activated carbon in the  $E_h$ -controlling ability as was found in section 6.3.1 and 6.3.2. As a result of lowered  $E_h$  by AC, Fe dissolution (= pyrite dissolution) was deteriorated (Fig. 6.15c), which enabled the prolonged enargite dissolution without Fe passivation (Fig. 6.15b).

Interestingly, the highest Cu recovery (58% at day 61) was achieved by the addition of A-powder (Fig. 6.15b), even though the successive AC-catalyzed  $E_{\rm h}$ -reduction was realized in this culture (Fig. 6.16); higher  $E_h$  is theoretically favorable for the faster enargite dissolution (Lattanzi et al., 2008). In order to understand the reason of this contradiction, kinetic fitting using shrinking core model was conducted for each culture (Fig. 6.17 and 6.18). All results were obviously well-fit to surface chemical reaction model (Fig. 6.17) rather than diffusion through product film model (Fig. 6.18), indicating that the fundamental reaction mechanism was unlikely changed by AC-type. However, it was found that the increasing addition of powder AC (A-powder, Bpowder) enabled to retain the relatively faster dissolution kinetics of enargite (around 0.006-0.008), while that of granular AC (B-granular) significantly reduced the kinetic constant from 0.0081 (without B-granular) to 0.0021 (with 0.3% B-granular). This suggests that the former AC-type might slightly enhance the enargite dissolution, possibly based on the galvanic reaction, leading to the cancelling out of the slowed enargite dissolution derived from AC-catalyzed lowered E<sub>h</sub>. Even though the effect of galvanic interaction in the individual contact was found negligibly small (see chapter 5), the numerous particle number of powder AC would repeatedly cause the reaction due to its high contact frequency, likely resulting in the noticeable contribution of galvanic effect to enargite dissolution. In conclusion, the utilization of powder AC during bioleaching process was found effective in retaining faster enargite dissolution, but not in AC-catalyzed *E*<sub>h</sub>-controlling.

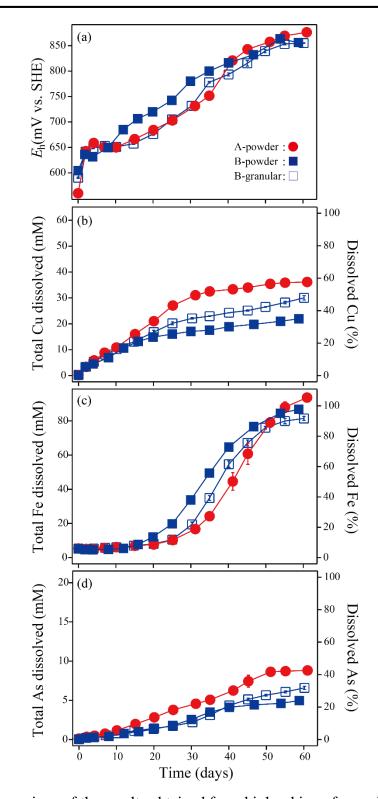


Fig. 6.15 Comparison of the results obtained from bioleaching of enargite concentrate in the presence of 0.08% A-powder ( $\bigcirc$ ), 0.08% B-powder ( $\bigcirc$ ), or 0.1% B-granular ( $\Box$ ); (a) *E*<sub>h</sub>, (b) total Cu concentration, (c) total Fe concentration, and (d) total As concentration.

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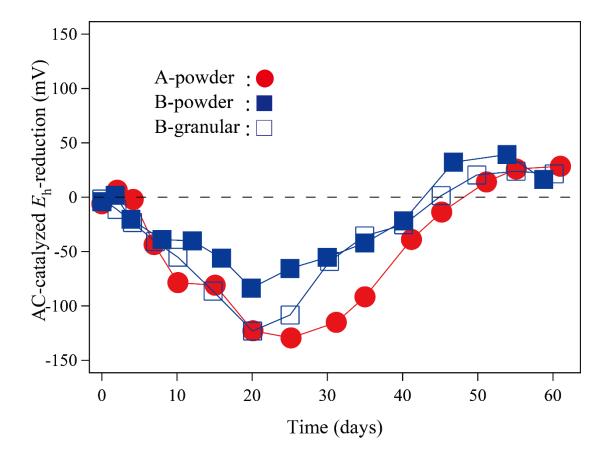
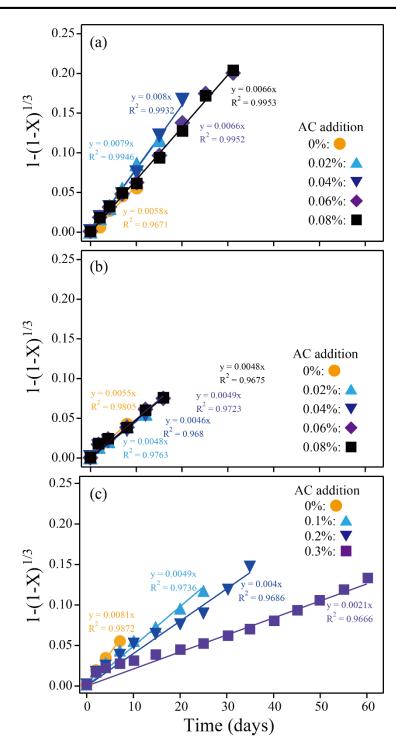


Fig. 6.16 AC-catalyzed  $E_h$ -reduction during bioleaching of enargite concentrate in the presence of 0.08% A-powder ( $\bigcirc$ ), 0.08% B-powder ( $\bigcirc$ ), or 0.1% (w/v) B-granular ( $\Box$ ).  $E_h$  value in each bioleaching culture without AC was normalized to 0 (broken line). The plots depict the difference in  $E_h$  between culture without AC and with AC:  $E_h$  [bioleaching without AC] –  $E_h$  [bioleaching with AC].



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Fig. 6.17 Kinetic fitting with surface chemical reaction model on bioleaching of enargite concentrate in the presence of  $0 (\bigcirc)$ ,  $0.02 (\blacktriangle)$ ,  $0.04 (\heartsuit)$ ,  $0.06 (\diamondsuit)$  and  $0.08\% (\blacksquare)$  A-powder (a) or B-powder (b), or  $0 (\bigcirc)$ ,  $0.1 (\bigtriangleup)$ ,  $0.2 (\heartsuit)$ , and  $0.3\% (\blacksquare)$  B-granular (c). Fitting duration was restricted until when rapid Fe dissolution was initiated during bioleaching.

0.15-(a) 1+2(1-X)-3(1-X)<sup>2/3</sup> 0.10 y = 0.0028xy = 0.0029x $R^2 = 0.8765$  $R^2 = 0.8421$ AC addition y = 0.0029x0.0021x  $R^2 = 0.8975$ 0%: 🔴  $R^2 = 0.8924$ 0.05 0.02%: 🔺 0.04%: 🔻 0.06%: 🔶 0.08%: 0.00 0.15 (b) AC addition  $1+2(1-X)-3(1-X)^{2/3}$ 0%: 🔴 0.02%: 🔺 0.10 0.04%: 🔻 y = 0.0009x0.06%: �  $R^2 = 0.9218$ y = 0.0009x0.08%:  $R^2 = 0.9276$ 0.05 y = 0.0006x $R^2 = 0.9113$ y = 0.0007x $R^2 = 09436$ 0.0008x  $R^2 = 0.9407$ 0.00 0.15 (c) AC addition 0%: 🔴  $1+2(1-X)-3(1-X)^{2/3}$ 0.1%: 🔺 0.2%: 🔻 0.10 0.3%: y = 0.0012x $R^2 = 0.8548$ y = 0.0006xy = 0.0013x $R^2 = 0.8597$  $R^2 = 0.9296$ 0.05 = 0.0011 x= 0.9323 0.00 30 40 50 20 10 60 0 Time (days)

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Fig. 6.18 Kinetic fitting with diffusion through product film model on bioleaching of enargite concentrate in the presence of  $0 (\bigcirc)$ ,  $0.02 (\blacktriangle)$ ,  $0.04 (\heartsuit)$ ,  $0.06 (\diamondsuit)$  and  $0.08\% (\blacksquare)$  A-powder (a) or B-powder (b), or  $0 (\bigcirc)$ ,  $0.1 (\bigtriangleup)$ ,  $0.2 (\heartsuit)$ , and  $0.3\% (\blacksquare)$  B-granular (c). Fitting duration was restricted until when rapid Fe dissolution was initiated during bioleaching.

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### 6.4 Conclusions

Based on the series of abiotic tests evaluating the catalytic effect of various AC and their application into bioleaching culture, catalytic mechanism, especially in terms of  $E_{\rm h}$ -control and Cu solubilization, were summarized as below.

1.  $E_h$ -controlling ability of AC

It was found that  $E_h$ -controlling ability of AC is determined by the structural property such as graphene and defect (edge) structure formed during the activation process, but not shape (powder or granular), specific surface area, and total pore volume. Due to the extremely high electric conductivity of graphene, AC with massive graphene structure would enable faster electron transfer for the coupling reaction that occurred on the AC surface. On the other hand, AC with plentiful defect structure is more advantageous in the oxidation reaction (e.g. Fe<sup>2+</sup>- and tetrathionate-oxidation), since the abundant surface functional group in the defect structure might catalyze the H<sub>2</sub>O<sub>2</sub> production on the AC surface, followed by its consumption for the oxidation reaction. Only AC made of coal, possessing the largest amount of defect structure among AC tested in this study, shows stronger oxidation ability than that made of coconut shell and woody chip, while no difference was confirmed in  $E_h$ -reducing ability among three of them. Chemicalactivated carbon is thought the best  $E_h$ -controlling AC due to its well-developed graphene structure, whilst the abundant defect structure in steam-activated carbon is undesirable for  $E_h$ -controlling catalyst.

2. Enhancement of Cu solubilization from enargite

Even though the contribution of the galvanic effect is negligibly small in the individual contact, extremely increased contact frequency by employing the powder AC could maximize the effect of galvanic interaction. As a result, slowed enargite dissolution by AC-catalyzed  $E_h$ -reduction was likely canceled out, resulting in retained faster enargite dissolution even in the presence of AC. This observation suggests that, therefore, finer AC must be used for the improvement of Cu solubilization from enargite.

Overall, powder AC made by the chemical-activation process is the best AC catalyst for bioleaching of enargite concentrate in terms of  $E_h$ -controlling ability and improved Cu solubilization.

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# Chapter 7

Application study; AC-catalyzed bioleaching of As-bearing copper concentrate at high pulp density in the stirred tank reactor

### Abstract

For the application of AC-catalyzed bioleaching to practical process, catalytic ability of AC was evaluated in bioleaching of As-bearing copper concentrate, composed of refractory (e.g. chalcopyrite, enargite) and easily soluble copper sulfide (chalcocite, geerite, bornite) at the high pulp density in the stirred tank reactor level. The consortia of moderate thermophiles was successfully adapted to As-bearing copper concentrate at high pulp density, by subsequently transferring the culture grown at lower pulp density to that at high pulp density; sterpwisely, increased from 2, 3, 5, 8, finally, to 10% (w/v). Two different amounts of AC (0.05% and 0.5% (w/v)) were indeed added into the 10% pulp density condition to investigate the catalytic ability of AC on high pulp density bioleaching in stirred tank reactor. The difference in final Cu recovery corrected by solution volume was hardly seen (38%, 38%, and 41% with 0, 0.05, and 0.5% AC, respectively), which became noticeable with the correction by both solution volume and the amount of unreacted residue (80%, 100%, and 98% with 0, 0.05, and 0.5% AC, respectively). The drops in abundance of chalcopyrite and enargite by the addition of AC were detected by MLA, likely resulting from their enhanced dissolution based on (i) AC-catalyzed  $E_h$ -control to the optimal potential, and (ii) high frequency of contact with AC accelerating the electron transfer (galvanic interaction). AC was also found effective in promoting As immobilization as the Fe-As precipitates revealed by MLA; the abundance of Fe-As precipitates dramatically improved from 11% (0% AC) to 53% (0.05%) and 61% (0.5%). Overall, AC-catalyzed bioleaching was successively found applicable to practical situation (high pulp density, complex mineralogy, stirred tank reactor).

## 7.1 Introduction

For the development of technique targeting the exploitation of refractory copper sulfides such as chalcopyrite and enargite, a number of bioleaching studies employing the reaction catalyst (e.g. Ag and AC) have been carried out (see Table 1.4). Nevertheless, most of these studies have been basically conducted as the fundamental research, especially in AC-catalyzed bioleaching: low-pulp density, concentrate with high purity, and flask level (Nakazawa et al., 1998; Liang et al., 2010; Ma et al., 2017)., Application study employing high-pulp density, complex mineralogy, and scale-up system must be thus investigated for the future implementation of AC-catalyzed bioleaching system into real mining operation.

There are the limited number of AC-catalyzed bioleaching study targeting complex copper sulfide ores under high pulp density condition (Zhang et al., 2007; Hao et al., 2018); the pulp density of each study was 25% and 10%, respectively. However, the used ores in both studies were low-grade copper sulfide ores containing only 1.1% and 0.38% of primary copper sulfide. The majority of these ores were quartz (SiO<sub>2</sub>) or other kinds of silicate mineral such as feldspar and mica, indicating that physical contact between copper sulfides and AC was expected less occurred. For more appropriate evaluation of catalytic effect by AC, complex copper concentrate with less gangue minerals should be utilized instead of low-grade ores.

Arsenic accumulation in the leachate must be also serious issue during bioleaching of As-bearing mineral (e.g. enargite) at the high pulp density. Gradual increase in pulp density from 5% to 30% was tested in bioleaching of flotation gold concentrate containing As-bearing mineral such as enargite and tennantite ( $Cu_{12}As_4S_{13}$ ), where obvious depression of metal extraction with increase of pulp density was indeed observed; almost 100% Cu at the pulp density of 5% was dropped to 30% at the pulp density of 30% (Astudillo and Acevedo, 2008). In this study, adapted culture to Asbearing gold concentrate was also prepared, which showed better metal extraction ability than non-adapted culture. These might be the indication that the condensed As during high pulp density bioleaching of As bearing concentrate could toxically inhibit the microbial activity, and it would become worse at the high pulp density condition.

Moreover, based on our knowledge, all AC-catalyzed bioleaching have been carried out in the flask shaking experiment (see Table 1.4). When this process would be scaled up to stirred tank reactor, in addition to the factors ascribed above, the effects of physical collision between microorganisms and minerals, oxygen transfer, stirring efficiency, and mechanochemical damage to microbes by agitating propeller have to be taken into account. This could lead to different bioleaching behavior from flask level AC-catalyzed bioleaching, suggesting the necessity of test in stirred tank reactor level. In this section, based on the knowledge obtained in chapter 5 and 6, AC-catalyzed bioleaching system was therefore up-graded form flask to stirred tank reactor. At the same time, the catalytic effect of AC on the dissolution of As-bearing copper sulfide at the high pulp density was evaluated.

## 7.2 Materials and Methods

# 7.2.1 Adaptation of moderate thermophiles consortia to high pulp density bioreactor

The pulp density of bioreactor experiment was stepwisely increased from 2% to 10% in order to gradually adapt the consortia of moderate thermophiles to higher pulp density condition.

HBS media (1 L; pH adjusted to 2.0 with 1 M H<sub>2</sub>SO<sub>4</sub>) containing 0.02% (w/v) yeast extract was sterilized by autoclaving, which was added into the tank reactor vessel with 30 g of unwashed As-bearing copper sulfide concentrate, D3 concentrate (2% pulp density). These media were stirred and mixed at 45°C for 1 day prior to inoculation, in order to solubilize the acid-soluble minerals and stabilize the solution condition. Pregrown culture of four bacteria (*Am. ferrooxidans* ICP, *Sb. sibiricus* N1, *At. caldus* KU, and *Lp. ferriphilum* P<sub>3</sub>A) and one archaeon (*Acidiplasma* sp. Fv-Ap) were collected (100 mL for each; 500 mL in total) and directly inoculated into the reactor so as to set the final culture volume to be 1.5 L. In this leaching experiment, pH was automatically kept at 2.0 by adding 0.5 M H<sub>2</sub>SO<sub>4</sub> and 0.5 M NaOH throughout the experiment. Temperature was held constant at 45°C. The bioreactor were aerated with 0.5 L/min and stirred at 150 rpm. Samples were regularly withdrawn to monitor pH, *E*<sub>h</sub>, cell density, and concentrations of total Fe, As, and Cu.

For the bioreactor experiment at the pulp density of 3%, 300 mL of bioreactor culture at the 2% pulp density was used as the inoculum and 1.2 L of HBS media containing 0.02% yeast extract was also added (final volume: 1.5 L) with 45 g of D3 concentrate. At the beginning, the pH was set to be 1.8 to prevent excess Fe precipitation, while it was re-set to 2.0 at day 7 since no cell growth was observed. To enhance the microbiological activity, aeration rate was increased to 1.0 L/min. Other experimental conditions were same with that at 2% pulp density.

For the further improvement of pulp density (5, 8, 10%), pH setting was kept at 2.0 throughout the experiment. Desired amount of D3 concentrate (75 g, 120 g, and 150 g for 5, 8, and 10% pulp density, respectively) was added into the tank reactor vessel with 1.2 LHBS media and 300 mL of previous bioreactor culture ( $3 \rightarrow 5\%$ ,  $5 \rightarrow 8\%$ ,  $8 \rightarrow 10\%$ ).

# 7.2.2 AC-catalyzed bioleaching of D3 concentrate at the pulp density of 10% in the stirred tank reactor

HBS media (1.2 L; pH adjusted to 2.0 with 1 M H<sub>2</sub>SO<sub>4</sub>) containing 0.02% (w/v) yeast extract was sterilized by autoclaving, which was added into the tank reactor vessel with 150 g of unwashed D3 concentrate (10% pulp density). Two different amount of AC (0.05% and 0.5% (w/v) of A-powder) were also added as the catalyst. These media were stirred and mixed at 45°C for 1 day prior to inoculation, in order to solubilize the acid-soluble minerals and stabilize the solution condition. Pre-grown bioreactor culture at the pulp density of 10% (300 mL) was added as the inoculum so as to set the final volume to be 1.5 L. Solution pH was automatically kept at 2.0 by adding 0.5 M H<sub>2</sub>SO<sub>4</sub> and 0.5 M NaOH throughout the experiment. Temperature was held constant at 45°C. The bioreactor were aerated with 1.0 L/min and stirred at 150 rpm. Samples were regularly withdrawn to monitor pH, *E*<sub>h</sub>, cell density, and concentrations of Fe<sup>2+</sup> (*o*phenanthroline method), As(III) (molybdenum blue method), and total Fe, As, and Cu (ICP-OES).

### 7.3 Results and Discussion

# 7.3.1 Stepwise adaptation of moderate thermophiles to high pulp density of D3 concentrate

The adaptation of moderate thermophiles to high pulp density of D3 concentrate were successfully achieved by subsequently transferring the culture pre-grown at lower pulp density to new culture at higher pulp density. At the beginning of the experiment, high pH varied from 2.4 to5.4 were observed in any cultures, whereas the pH of medium was set to 2.0 (Fig. 7.1a). This would be due to the dissolution of easily soluble copper sulfide and small fraction of chalcopyrite, which consume the proton during their dissolution process as follows;

$$CuFeS_2 + O_2 + 4H^+ \rightarrow Cu^{2+} + Fe^{2+} + 2S^0 + 2H_2O$$
 (Eq. 7.1)

$$2CuS_2 + O_2 + 4H^+ \rightarrow 2Cu^{2+} + 4S^0 + 2H_2O$$
 (Eq. 7.2)

$$2CuS + O_2 + 4H^+ \rightarrow 2Cu^{2+} + 2S^0 + 2H_2O$$
 (Eq. 7.3)

After day 1, pH were lowered and perfectly controlled to 2.0 in all cultures (or 1.8 in 3% pulp density culture) to prepare the suitable condition for active cell growth (Fig. 7.1a). Rapid increase of cell density up to around  $6 \times 10^8$  cells/mL with short lag phase were thus observed in almost all cultures, while the lag phase was longer in the culture at the pulp density of 3% (Fig. 7.1c). Lower initial pH (1.8) compared to other cultures (2.0) might cause less Fe precipitation, likely allowing the toxic elements contained in D3 concentrate (e.g. As, Cd, Pb) to be mobile in solution phase. This was prevented by re-setting the pH to 2.0 at day 7, followed by rapid increase in cell number (Fig. 7.1c). The faster cell growth with increase in pulp density were apparently seen, which might be attributed to (i) microbial adaptation to this concentrate or (ii) miss-counting of mineral particles. Although the microbiological analyses have been insufficient, it was assumed the possibility that (i) each microorganism has acquired the tolerance against the D3 concentrate (or toxic metal in the concentrate), or (ii) population structure has been optimized for bioleaching of the concentrate by modifying the abundance of each microbes.

With increase in the pulp density,  $E_{\rm h}$ -rise was deteriorated, which consequently reached a plateau at around 750 mV in any cases (Fig. 7.1b). This delayed  $E_{\rm h}$  increase was caused by the presence of larger amount of easily soluble copper sulfide at higher pulp density; Cu solubilization was indeed dramatically improved with increase in pulp density (Fig. 7.1d), from 49 mM (2%) to 89 mM (3%), 156 mM (5%), 228 mM (8%), and 233 mM (10%). Relatively similar final Cu recovery confirmed that easily soluble copper sulfide was mainly subjected to Fe(III) oxidation, but not refractory copper sulfide: 54, 59, 61, 60 at the pulp density of 2, 3, 5, 8%, respectively (Fig. 7.2a). Only the 10% pulp density culture resulted in the lower Cu recovery (41%), suggesting the possibility of inefficient stirring. Likewise, final Fe and As recovery showed similar value regardless of the pulp density, even though the dissolved concentration were obviously increased with increase in the pulp density. In any cultures, only around 10% of Fe was stable as the ionic form in the solution, since once-dissolved Fe was easily immobilized by forming ferric sulfate precipitates such as jarosite (KFe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub>) at pH 2. Accompanying with this Fe precipitates, it was expected that As would be also immobilized as ferric arsenate or co-precipitated with jarosite, resulting in only around 7% of final recovery. Final recovery of Cu, As, Fe at the variety of pulp density were summarized in Table 7.1.

Pulp density (%)	ŀ	Recovery (%	)
	Cu	As	Fe
2	54.1	7.4	11.3
3	59.1	7.6	10.4
5	60.5	7	9
8	60.1	6.9	7.8
10	41.4	5.6	7.9

Table 7.1 Final recovery of Cu, As, and Fe in the bioreactor experiment at different pulp density.

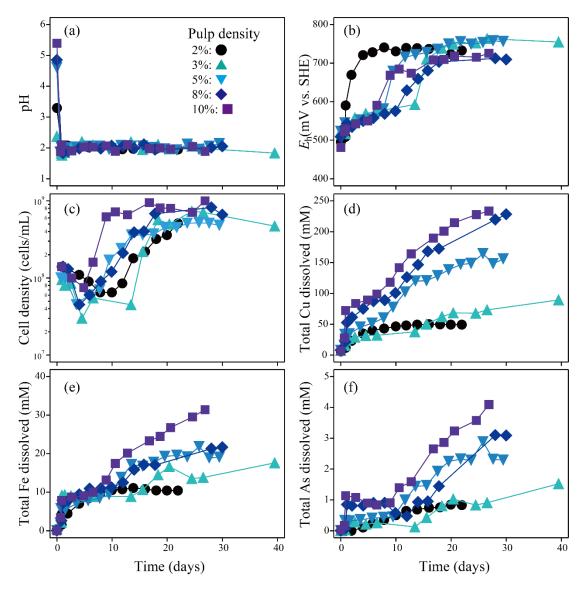
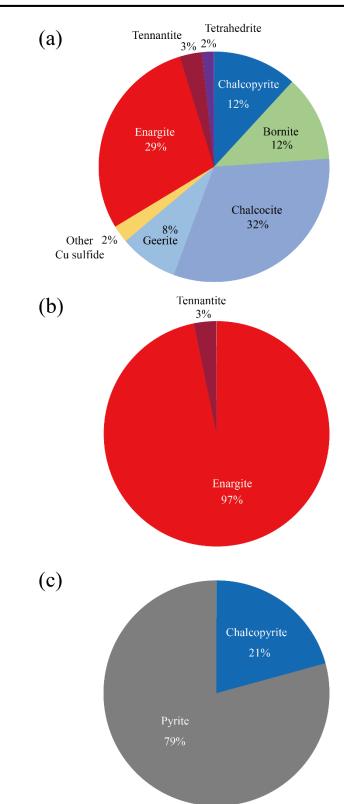


Fig. 7.1 Changes in pH (a),  $E_h$  (b), cell density (c), total soluble Cu concentration (d), total soluble Fe concentration (e), and total soluble As concentration (f) during bioleaching of D3 concentrate at the pulp density of 2% ( $\bigcirc$ ), 3% ( $\checkmark$ ), 5% ( $\checkmark$ ), 8% ( $\diamondsuit$ ), and 10% ( $\blacksquare$ ). Pre-grown culture was inoculated at day 1.



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Fig. 7.2 Composition of Cu (a), Fe (b), and As (c) contents dissolved from each mineral in D3 concentrate.

### 7.3.2 Catalytic effect of AC on bioleaching of D3 concentrate

For the practical evaluation, AC-catalyzed bioleaching of copper sulfide at the pulp density of 10% were carried out in the stirred tank reactor and its catalytic effect was investigated. In the absence of AC, planktonic cell density actively increased more than  $10^9$  cells/mL, while long lag phase of cell growth was apparently seen in the culture with 0.5% AC addition (Fig. 7.3c). Considering the  $E_{\rm h}$ -rise in this culture at the early stage of the experiment (Fig. 7.3b), however, larger amount of AC enabled adsorbing the majority of planktonic cells on its surface, possibly leading to the invisible increase of the cell density occurred on the AC surface. Consequently, cell density in any cultures reached at the same level in the late stage of the experiment, indicating that cell growth itself was hardly inhibited by the addition of AC. Even though slightly lower  $E_{\rm h}$  was maintained by 0.05% AC addition compared to the culture without AC, almost similar trend in both cases suggest that 0.05% AC was insufficient to control the  $E_{\rm h}$  to lower level (< 700 mV). The addition of 0.5% AC retained the lowered  $E_{\rm h}$ less than 700 mV throughout the experiment with two-stage  $E_h$  increase (Fig. 7.3b): (i) relatively rapid  $E_{\rm h}$  rise until day 10 (1st stage), followed by (ii) gradual re-increase of once-dropped  $E_h$  from day 10 to 30 (2nd stage). This two-stage  $E_h$  increase might be attributed to the presence of yeast extract, supplemented to support the initial cell growth. Heterotrophic Fe-oxidizer, Am. ferrooxidans ICP, Sb. sibiricus N1, Acidiplasma sp. Fv-Ap was likely activated by using yeast extract as a carbon source, which led to the rapid increase of  $E_{\rm h}$  to 682 mV until day 10 (Fig. 7.3b). Once yeast extract was completely consumed for their growth,  $E_{\rm h}$  was dropped to 631 mV in 3 days possibly due to (i) the deactivation of heterotrophic Fe-oxidizer and (ii) the  $E_{\rm h}$ lowering effect by sufficient amount of AC (0.5%). After this, heterotrophic Feoxidizer would switch their energy source to the organic metabolite produced by autotrophic S-oxidizer, At. caldus KU, resulting in the slower but steady increase of E<sub>h</sub>. Since the activity of microorganism in reactor was rather higher than that in the flask, larger amount of AC (0.5%) was found necessary to maintain the lower  $E_h$  level compared to the bioleaching in the flask level.

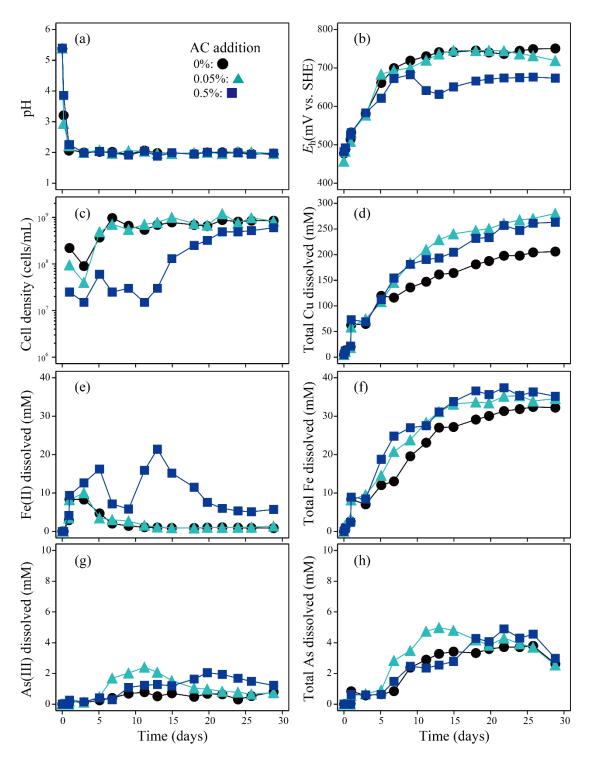
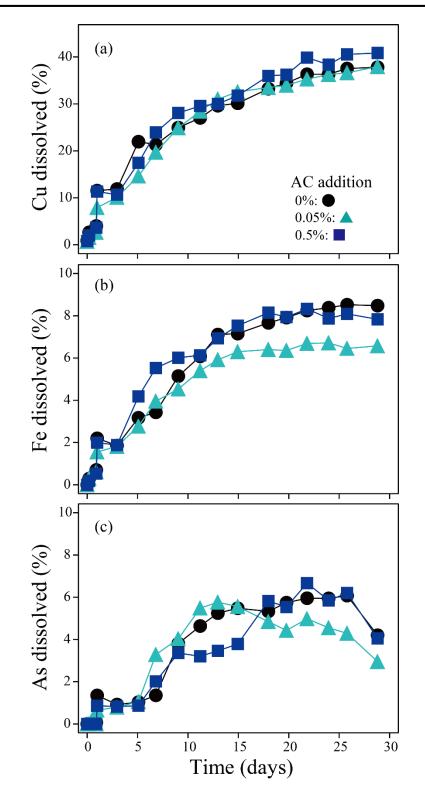


Fig. 7.3 Changes in pH (a),  $E_h$  (b), cell density (c), total soluble Cu concentration (d), Fe(II) concentration (e), total soluble Fe concentration (f), As(III) concentration (g) and total soluble As concentration (h) during bioleaching of D3 concentrate at the pulp density of 10% in the absence ( $\bigcirc$ ) or presence of 0.05% ( $\blacktriangle$ ) and 0.5% (w/v) ( $\square$ ) AC. Pre-grown culture was inoculated at day 1.



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Fig. 7.4 Changes in the Cu (a), Fe (b), and As recovery (c) corrected by the solution volume during bioleaching of D3 concentrate at the pulp density of 10% in the absence ( $\bullet$ ) or presence of 0.05% ( $\blacktriangle$ ) and 0.5% (w/v) ( $\blacksquare$ ) AC. Pre-grown culture was inoculated at day 1.

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In the presence of AC, higher Cu solubilization was observed (280 and 263 mM with 0.05 and 0.5% AC addition, respectively) than that without AC (205 mM) (Fig. 7.3d), while Cu recovery corrected by solution volume showed similar value in each cases (Fig. 7.4a): 38% (0% AC), 38% (0.05%), and 41% (0.5%). Although it seemed that the enhanced Cu dissolution was the results of the concentration of Cu ion due to the water evaporation, it was found that some part of leaching solid sank to the bottom of reactor, which would be unreacted with leaching solution throughout the experiment (defined as "unreacted residue"). As shown in Fig. 7.5, reacted part of solid residue (defined as "reacted residue") were easily separated from the unreacted residue since the latter was firmly solidified at the bottom of reactor vessel.

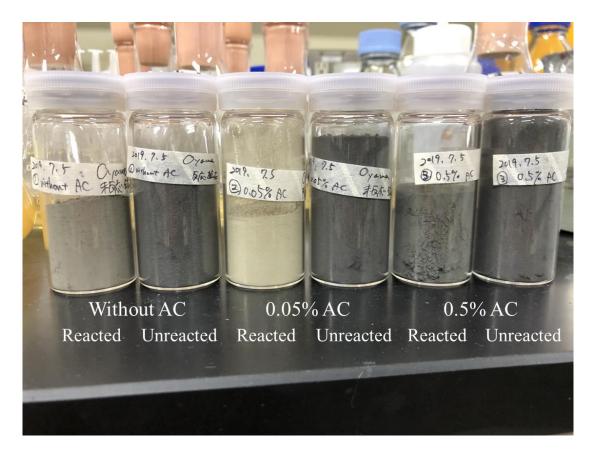


Fig. 7.5 Separately collected solid residue after 30 days of bioleaching of D3 concentrate in the absence or presence of 0.05% and 0.5% AC. Reacted residue: floated and well-mixed part of leaching reside with whiter color. Unreacted residue: settled and coagulated part of leaching residue with black color.

In order to eliminate the effect of unreacted solid from the consideration, Cu, Fe, and As recovery were re-corrected by the amount of unreacted residue (Fig. 7.6). The presence of AC realized the almost complete dissolution of copper sulfides regardless of AC amount: final Cu recovery improved from 80% (0% AC) to 100% (0.05% AC9 and 98% (0.5% AC). Contrary to slight contribution of AC to enargite dissolution (see chapter 5 and 6), it has been well-known that chalcopyrite dissolution is dramatically promoted by the presence of AC (Nakazawa et al., 1998; Zhang et al., 2007; Liang et al., 2010; Hao et al., 2018). This was confirmed by MLA results, where abundance of chalcopyrite was suddenly dropped by the addition of AC (16% (0% AC) to 3% (0.05%) and < 1% (0.5%); Table 7.2; Fig.7.7).

Hiroyoshi et al. (2000, 2001, 2002, 2007, 2008) reported that chalcopyrite dissolution is promoted at lower  $E_h$  rather than higher  $E_h$  via the transformation into chalcocite as an intermediate, followed by its dissolution to solubilize the Cu ion (Eqs. 7-4 and 7-5).

$$CuFeS_2 + 3Cu^{2+} + 4e^- = 2Cu_2S + Fe^{2+}$$
 (Eq. 7-4)

$$Cu_2S = 2Cu^{2+} + S^0 + 4e^-$$
 (Eq. 7-5)

The  $E_h$  when Eq. 7-4 and 7-5 occur were defined as  $E_c$  and  $E_{ox}$ , which are thermodynamically calculated by Eq. 7-6 and 7-7.

$$E_{\rm c} ({\rm V}) = 0.72 + 0.059 \log \frac{(a_{Cu^{2+}})^{0.75}}{(a_{Fe^{2+}})^{0.25}}$$
 (Eq. 7-6)

$$E_{\rm ox} (V) = 0.60 + 0.059 \log (a_{Cu^{2+}})^{0.5}$$
 (Eq. 7-7)

where R, T, F, and  $a_i$  are gas constant (J/Kmol), temperature (K), faraday constant (C/mol), and the activities of species *I*, respectively. When  $E_h$  satisfied the optimal range,  $E_{ox} < E_h < E_c$ , the reactions of Eq. 7-4 and 7-5 occur at the same time, leading to faster chalcopyrite dissolution. Since  $E_c$  and  $E_{ox}$  are varied depending on Cu<sup>2+</sup> and Fe<sup>2+</sup> concentration, Okamoto et al (2004) introduced " $E_{normal}$ " to normalize the optimal  $E_h$  range in any experimental condition, with the definition as below;

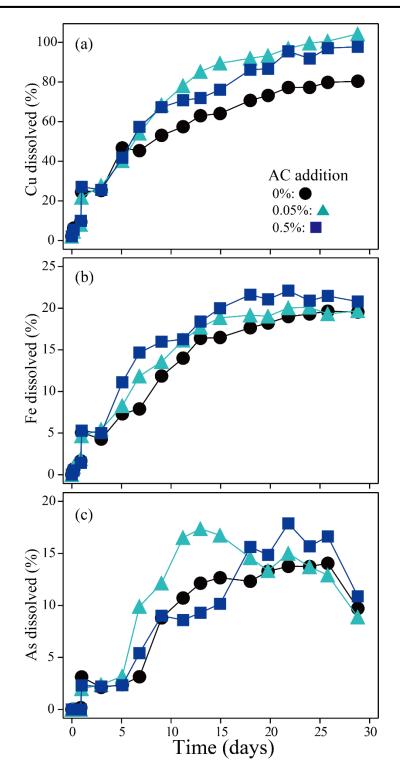
$$E_{\text{normal}} = (E - E_{\text{ox}}) / (E_{\text{c}} - E_{\text{ox}})$$
 (Eq. 7-8)

In this definition, optimal potential range for the enhanced chalcopyrite dissolution,  $E_{ox} < E_h < E_c$ , is set to be  $0 < E_{normal} < 1$ .

Fig. 7.8 shows the changes in  $E_{normal}$  during bioleaching of D3 concentrate in the absence or presence of AC. The results showed that  $E_{normal}$  value slightly exceed over 1 after day 10 in the absence of AC, while the presence of AC basically enabled controlling the  $E_{\text{normal}}$  into the optimal range,  $0 < E_{\text{normal}} < 1$ , throughout the experiment. This AC-catalyzed  $E_{normal}$  control would contributed to the enhanced chalcopyrite dissolution, resulting in the dropped abundance of chalcopyrite confirmed by MLA (Fig. 7.7). Although the catalytic effect of AC on the dissolution of easily soluble copper sulfide (bornite, chalcocite, and geerite) has been poorly investigated, the decrease in their proportion by the addition of AC from 6% (0% AC) to < 1% (0.5% AC) was likely the evidence that the presence of AC also catalytically facilitate the dissolution of them (Table 7.2; Fig. 7.7). This suggests that the dissolution of chalcocite formed by Eq. 7-4 also could be promoted by AC catalyst, probably leading to further enhancement of chalcopyrite dissolution. In summary, chalcopyrite dissolution would be dramatically enhanced by AC based on the following two mechanisms; (i) AC-catalyzed E<sub>h</sub>-control achieved optimal  $E_{normal}$  range to facilitate the chalcopyrite transformation into easily soluble copper sulfide such as chalcocite, and (ii) the dissolution of chalcocite produced via chalcopyrite transformation is accelerate by AC.

Enargite dissolution was also greatly enhanced by the addition of AC: the proportion of enargite measured by MLA dropped from 24% (0% AC) to 7% (0.05%) and 6% (0.1%) (Table 7.2; Fig. 7.7). Although lowered  $E_h$  by the addition of 0.5% AC was assumed undesirable for the enargite dissolution (Fig. 7.3b), larger amount of AC would lead to high contact frequency between enargite and AC, possibly supporting the continuous enargite dissolution.

Overall, even though the condition of bioreactor operation must be further optimized, catalytic effect of AC was found useful to enhance the Cu solubilization during bioleaching of As-bearing copper concentrate even in the stirred tank reactor level.



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Fig. 7.6 Changes in the Cu (a), Fe (b), and As recovery (c) corrected by the solution volume and the amount of unreacted residue during bioleaching of D3 concentrate at the pulp density of 10% in the absence ( $\bigcirc$ ) or presence of 0.05% ( $\triangle$ ) and 0.5% (w/v) ( $\square$ ) AC. Pre-grown culture was inoculated at day 1.

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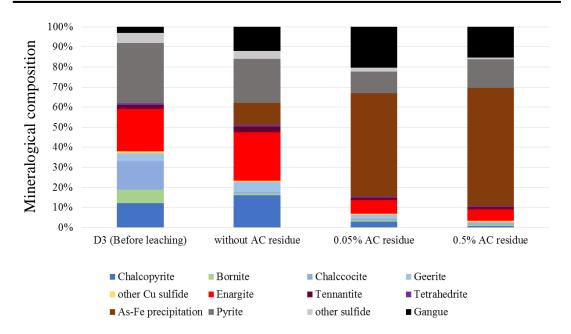


Fig. 7.7 MLA results of original D3 concentrate and bioleached reacted residue recovered on day 30 from cultures containing 0%, 0.05%, or 0.5% AC.

Table 7.2 Mineralogical composition of original D3 concentrate and bioleached reacted residue recovered on day 30 from cultures containing 0%, 0.05%, or 0.5% AC determined by MLA.

Mineral (wt%)	Original D3 concentrate	Without AC reacted residue	0.05% AC reacted residue	0.5%AC reacted residue
Chalcopyrite	12	16	3	<1
Bornite	7	1	<1	<1
Chalcocite	14	<1	<1	<1
Geerite	4	5	2	<1
other Cu sulfide	1	<1	<1	<1
Enargite	21	24	7	6
Tennantite	2	3	1	1
Tetrahedrite	1	<1	<1	<1
As-Fe precipitation	-	11	53	61
Pyrite	30	22	11	15
other sulfide	5	4	2	<1
Gangue	3	12	21	16

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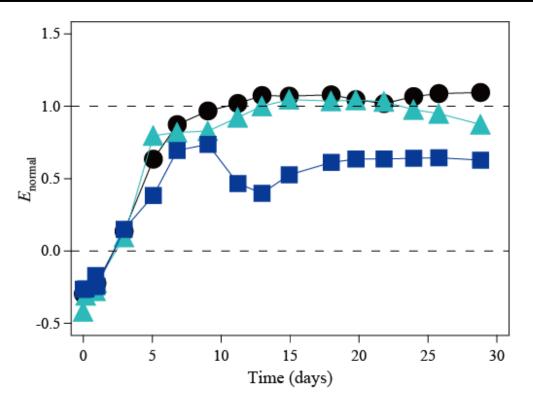


Fig. 7.8 Changes in the  $E_{normal}$  during bioleaching of D3 concentrate at the pulp density of 10% in the absence ( $\bigcirc$ ) or presence of 0.05% ( $\checkmark$ ) and 0.5% (w/v) ( $\square$ ) AC.

Contrary to the improved final Cu recovery by the addition of AC, both final Fe and As recovery reached to the similar values in any cultures at the end of the experiment, approximately 20% and 10%, respectively. Since 97% of As and 21% of Fe are derived from enargite and chalcopyrite dissolution, respectively, considering almost complete Cu extraction from the concentrate, it was expected that majority of Fe and As were immobilized in the solid phase, which led to their lower recovery. MLA results indeed revealed that As was co-precipitated with Fe, whose dominance became noticeable with the addition of AC (11%, 53%, and 61% in the presence of 0%, 0.05%, 0.5% AC, respectively; Table 7.2; Fig. 7.7). Based on XRD analysis, however, jarosite was found the only secondary mineral formed during bioleaching, but no As-bearing minerals (Fig. 7.9). Interestingly, fine particle (< 1  $\mu$ m) composed of Fe, S, O, As and Cu were uniformly detected by SEM observation (Fig. 7.10). The composition of these fine particles indicates that Cu and As could be incorporated into the structure of jarosite, resulting in the formation of Fe-As precipitations. Previous study regarding the As immobilization as biogenic scorodite reported that increasing As-inclusion into ferric

sulfate structure gradually changed the color of precipitates from brownish orange to whitish pale green (Tanaka et al., 2018). Likewise, whiter color of reacted leaching residue obtained from the culture containing 0.05% AC proved that As-inclusion into jarosite structure indeed occurred, resulting in the immobilization of As as the Fe-As precipitates; note that blackish color of reacted residue obtained from the culture in the presence of 0.5% AC could be derived from the contamination of AC.

This facilitated Fe-As co-precipitation would be due to the relatively higher pH automatically maintained at around 2.0 throughout the experiment (Fig. 7.3a); Fe(III) is easily immobilized as jarosite at such pH, accompanying with co-immobilization of As. Since larger amount of As were theoretically once-solubilized by the addition of AC owing to the enhanced enargite dissolution, the resultant formation of Fe-As precipitates would be consequently facilitated (Fig. 7.7). These results suggested that, even though immobilization ratio was not able to be calculated, AC was also likely useful for the immobilization of once-dissolved As from enargite during bioleaching of As-bearing copper concentrate.

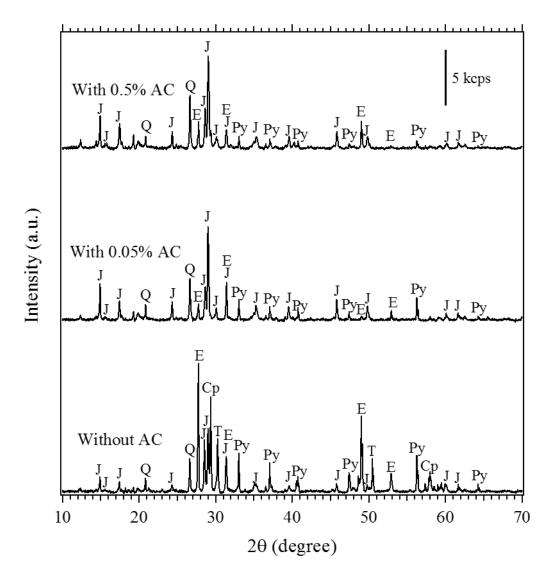


Fig. 7.9 X-ray diffraction patterns of bioleached residue recovered on day 30 from cultures containing 0%, 0.05%, or 0.5% AC. E: enargite (Cu<sub>3</sub>AsS<sub>4</sub>; PDF No. 00-035-0775), Py: pyrite (FeS<sub>2</sub>; PDF No. 00-042-1340), Q: quartz (SiO<sub>2</sub>; PDF No. 01-070-3755), J: jarosite (K(Fe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub>); PDF No. 01-076-0629), Cp: chalcopyrite (CuFeS<sub>2</sub>; PDF No. 01-075-6866), Tennantite (Cu<sub>12</sub>As<sub>4</sub>S<sub>13</sub>; PDF No. 01-074-1027).

Chapter 7 Application study; AC-catalyzed bioleaching of As-bearing copper concentrate at high pulp density in the stirred tank reactor

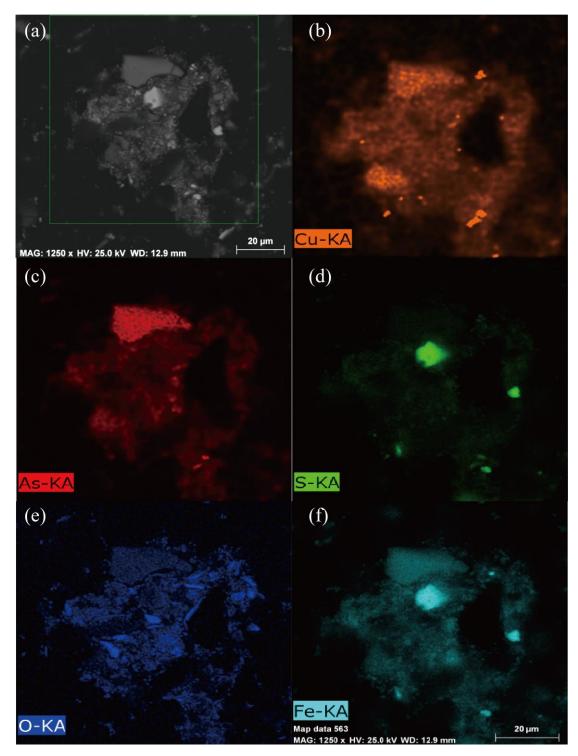


Fig. 7.10 SEM image (a) and elemental mapping (b-f) of reacted residue recovered at day 30 from the culture containing 0.5% AC: Cu (b), As (c), S (d), O (e), and Fe (f). Aggregation of ultrafine particle (< 1  $\mu$ m) composed of Cu, As, S, O, and Fe was found.

# 7.4 Conclusions

AC-catalyzed bioleaching system was scaled up to stirred tank reactor in order to investigate the catalytic effect of AC on As-bearing copper concentrate at high pulp density. Pre-grown bioleaching cultures were subsequently transferred to the new media with higher pulp density, aiming to the gradual adaptation of moderate thermophile consortia to As-bearing copper concentrate. Finally, the pulp density successfully increased from 2% up to 10% with retaining the great cell activity. AC catalyst was indeed added for its evaluation to high pulp density culture, whereas the improvement of Cu recovery corrected by solution volume was hardly seen even in the presence of AC. Since the unreacted residue was found settled and solidified at the bottom of the reactor, the correction by solution volume as well as the amount of unreacted residue was carried out, leading to the more noticeable difference in final Cu recovery: 80%, 100%, and 98% in the presence of 0%, 0.05%, and 0.5% AC, respectively. This might be due to the enhanced chalcopyrite and enargite dissolution determined by MLA, where obvious disappearances of chalcopyrite and enargite by the addition of AC was observed. AC-catalyzed  $E_{\rm h}$ -control and contact between AC and these minerals could offer the desirable condition for faster dissolution of these refractory minerals. The dissolution of easily soluble copper sulfide (chalcocite, geerite, bornite) was also facilitated by AC, which could indirectly contribute to the enhancement of chalcopyrite dissolution. XRD, SEM, and MLA results revealed that the presence of AC was also effective in promoting the As immobilization based on the co-precipitation with jarosite. Overall, the applicability of AC-catalyzed bioleaching to high pulp density of As-bearing copper concentrate was successfully confirmed.

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# Chapter 8

Conclusions

#### 8.1 Conclusions

Slow dissolution kinetic of refractory primary copper sulfides such as chalcopyrite and enargite even in bioleaching process suggests the necessity of some reaction catalyst. Especially for enargite bioleaching system, less attention has been paid than that of chalcopyrite; hence, limited information about possible catalyst is available. Considering the serious increase in the As contamination in copper deposits, however, the exploitation of As-bearing copper mineral as a copper resource is urgently necessitated. Therefore, this thesis aimed to evaluate the candidate catalysts, silver and activated carbon, in enargite bioleaching for the development of Cu production process from As-bearing copper sulfides.

Firstly, silver catalyst was tested in bioleaching of enargite concentrate (chapter 4), which has been long recognized as a promising catalyst for the chalcopyrite leaching. Addition of Ag<sub>2</sub>S as a silver catalyst enabled selective Cu dissolution from enargite while suppressing pyrite oxidation: at the highest Ag<sub>2</sub>S concentration of 0.04%, Cu recovery reached 96%, while Fe dissolution was suppressed to reach only 29% by day 72. Lowered  $E_h$  level by Ag<sub>2</sub>S addition (i) and high subjectivity of Ag<sub>2</sub>S to Fe<sup>3+</sup>oxidation (ii) could be the reason of suppressed pyrite dissolution. Based on the results from the thermodynamic calculation and solid analyses, faster enargite dissolution proceeds via the formation of at least two types of secondary products (chalcocite, Cu<sub>2</sub>S; trisilver arsenic sulfide, Ag<sub>3</sub>AsS<sub>4</sub>). Addition of Ag<sub>2</sub>S thermodynamically and microbiologically contributed to lowering  $E_{\rm h}$  during bioleaching, consequently satisfying  $E_{ox}$  (Cu<sub>2</sub>S)  $< E_h < E_c$  (Ag<sup>+</sup>) to enhance enargize dissolution via formation of chalcocite intermediate. Detection of trisilver arsenic sulfide (Ag<sub>3</sub>AsS<sub>4</sub>) and its intermediate layer (Cu,Ag)<sub>3</sub>AsS<sub>4</sub> on the enargite surface indicated that Cu ion in the enargite lattice would be gradually substituted with Ag ion in the solution. Such secondary products did not impose a rate-limiting step, since the Ag-catalyzed bioleaching was shown to be controlled by a chemical surface reaction, rather than diffusion through product film, which was the case in the absence of Ag<sub>2</sub>S. An economical and environmentally-friendly alternative catalyst possessing similar catalytic properties with silver was not found, while complete Ag-recovery as trisilver arsenic sulfide was thought one of the possibilities to implement this process into real operation.

Even though the strong catalytic ability of Ag was desirable for the Cu recovery from enargite, loss of A was inevitable, leading to the uneconomical process. This motivated us to search for the cheaper catalyst, which is certainly disposable after the leaching process. Since activated carbon has also been tested as a useful but cheaper catalyst in chalcopyrite bioleaching, its catalytic effect on enargite bioleaching was also evaluated (chapter 5). In the absence of AC, co-existing pyrite ( $FeS_2$ ) in enargite concentrate began to rapidly solubilize at day 7, which was increasingly delayed by the addition of 0.1% and 0.2% AC to day 25 and 35, respectively. This was likely the result of the lowered  $E_{\rm h}$  level via Fe<sup>3+</sup>-reduction coupled with reduced inorganic sulfur compounds (RISCs)-oxidation on the AC surface acting as an electron-mediator. Real-time PCR analysis found that the abundance of S-oxidizing bacteria dropped in the presence of AC, proving that RISCs as an energy source for S-oxidizing bacteria were indeed consumed via the coupling reaction. While final Cu recovery was improved from 36% (0% AC) to 53% (0.2%), the electrochemical study suggested that this was not much contributed by the galvanic interaction between enargite and AC. A kinetic study using the shrinking core model revealed that AC addition let Cu solubilize slowly but steadily and continuously. Suppressed pyrite dissolution by AC addition was followed by suppressed Fe-passivation, which would contribute to steady enargite dissolution. Addition of AC also facilitated the As immobilization from 3.1 mM (0% AC at day 10) to 5.2 mM (0.1% AC at day 30), 7.0 mM (0.2% AC at day 40), and 6.9 mM (0.3% AC at day 60). EPMA analysis found that As was immobilized as ferric arsenate selectively on the enargite surface, while its re-solubilization was observed coincided with rapid pyrite dissolution. This observation implied that rapid supply of sulfate ion via pyrite dissolution might trigger the re-solubilization of As-precipitates. Based on the results obtained above, AC-catalyzed  $E_{\rm h}$ -control played an important role in controlling pyrite dissolution, which is indirectly but strongly influential on steady enargite dissolution without Fe-passivation and stable As immobilization. Therefore, further investigation in the catalytic ability of AC was expected beneficial for the development of ACcatalyzed bioleaching system.

For the clarification of the fundamental catalytic ability of AC, various AC were compared in the abiotic experiment, followed by their application into the bioleaching experiment (**chapter 6**). The former experiment mainly aimed at the elucidation of the

property determining E<sub>h</sub>-control ability of AC, while the latter was conducted to investigate if different AC properties affect on Cu solubilization from enargite. It was found that  $E_{\rm h}$ -controlling ability of AC is determined by the structural property such as graphene and defect (edge) structure formed during the activation process, but not shape (powder or granular), specific surface area, and total pore volume. Due to the extremely high electric conductivity of graphene, AC with massive graphene structure would enable faster electron transfer for the coupling reaction that occurred on the AC surface. On the other hand, AC with plentiful defect structure is more advantageous in the oxidation reaction (e.g.  $Fe^{2+}$  and tetrathionate-oxidation), since the abundant surface functional group in the defect structure might catalyze the H<sub>2</sub>O<sub>2</sub> production, followed by its consumption for the oxidation reaction. Chemical-activated carbon was thought the best  $E_{\rm h}$ -controlling AC due to its well-developed graphene structure, whilst the abundant defect structure in steam-activated carbon is undesirable for  $E_{\rm h}$ controlling catalyst. Even though the contribution of the galvanic effect was found negligibly small through the individual contact in chapter 5, extremely increased contact frequency by employing the powder AC could maximize the effect of galvanic interaction. As a result, slowed enargite dissolution by AC-catalyzed  $E_{\rm h}$ -reduction was likely canceled out, resulting in the retention of faster enargite dissolution even under  $E_{\rm h}$ -lowered condition by AC catalysis. This observation suggests that, therefore, finer AC must be used for the improvement of Cu solubilization from enargite. As a conclusion, powder AC made by chemical-activation process was found the best AC catalyst for bioleaching of enargite concentrate in terms of  $E_{\rm h}$ -controlling ability and improvement of Cu solubilization.

Finally, AC-catalyzed bioleaching system was scaled up to stirred tank reactor targeting complex copper concentrate, D3 concentrate, at high pulp density for the practical evaluation of AC (**chapter 7**). Pre-grown bioleaching cultures were subsequently transferred to the new media with higher pulp density, aiming to the gradual adaptation of moderate thermophile consortia to complex copper concentrate. Consequently, the pulp density successfully increased from 2% up to 10% with retaining the great cell activity. AC catalyst was indeed added to high pulp density culture for its evaluation, whereas the improvement of Cu recovery corrected by solution volume was hardly seen. Since the unreacted residue was found settled and solidified at the bottom of the reactor,

the correction by solution volume as well as the amount of unreacted residue was carried out, resulting in the more noticeable difference in final Cu recovery: 80%, 100%, and 98% in the presence of 0%, 0.05%, and 0.5% AC, respectively. This might be due to the enhanced chalcopyrite and enargite dissolution determined by MLA, where obvious disappearances of chalcopyrite and enargite were observed. AC-catalyzed  $E_{h-}$  control and contact between AC and these minerals could offer the desirable condition for faster dissolution of these refractory minerals. The dissolution of easily soluble copper sulfide (chalcocite, geerite, bornite) was also facilitated by AC, which might indirectly contribute to the enhancement of chalcopyrite dissolution. XRD, SEM, and MLA results revealed that the presence of AC was also effective in promoting the As immobilization based on the co-precipitation with jarosite. In summary, the applicability of AC-catalyzed bioleaching to high pulp density of As-bearing complex copper sulfide was successfully confirmed.

Overall, the utility of catalyst (Ag and AC) in bioleaching of As-bearing copper concentrate has been successfully confirmed by the fundamental study, which was also scaled up to the practical level to provide the helpful information for the future implementation into a real mining operation. Whole findings in this work would provide us the new aspects and future direction for the further development of biomining technologies.

#### 8.2 Recommendations for future work

In this work, two different As-bearing concentrates, enargite concentrate and D3 concentrate, were employed as the target samples. These samples were produced from the process to obtain high Cu-grade copper concentrate from As-bearing copper ore. The brief flowsheet of the process for the exploitation of As-bearing copper ore is described in Fig. 8.1. Unfortunately, since the current industrial technique is not capable of economic Cu production from As-bearing minerals, the repeated separations are conducted to minimize the As contamination in the final copper concentrate. Through this process, crushing and milling of ores are also repeated to improve mineral liberation for the following separation. This led to the production of extremely fine concentrate, which is not applicable to conventional bio-heap leaching due to the low water-flowage. Therefore, the development of the leaching process enabling copper production form fine concentrate is thought necessary. Stirred tank reactor, as was also employed in this work, is considered as one of the options, while further investigation regarding the agitation efficiency, aeration system, pH management, pulp density, and mechanical effect, is inevitable. Innovation of aeration system (e.g. installation of fine bubble technologies) could also provide a new aspect for the novel process to obtain the Cu from such fine concentrate.

Moreover, the effect of the presence of easily soluble copper sulfide (e.g. chalcocite, covellite, bornite) on the dissolution of refractory primary copper sulfide must be clarified. The dissolution behavior of complex copper sulfide has been less discussed, remaining uncertainties in the relationship between two types of minerals. The investigation on this would be beneficial to determine the appropriate concentrate, As bearing complex copper concentrate (e.g. D3 concentrate) or As-bearing copper concentrate (e.g. enargite concentrate) for bioleaching installation.

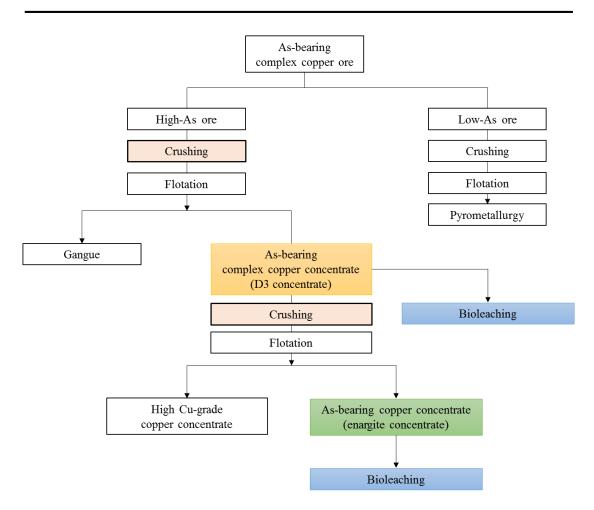


Fig. 8.1 Brief flowsheet of the exploitation process for As-bearing copper ores.

Regardless of its economic obstacle, Ag-catalyzed bioleaching is the possible option for the exploitation of As-bearing copper concentrate (e.g. enargite concentrate) as proposed in Fig. 8.2; note that the stirred tank reactor is employed under the assumption of fine concentrate. It is expected that economic loss would be reduced by (i) employing originally Ag-containing concentrate as a target material, (ii) re-using Ag-containing solid residue, and (iii) adding the waster Ag resources such as printed circuit board (PCB). As was found in chapter 4, separation of Ag as Ag<sub>3</sub>AsS<sub>4</sub> is surely the promising Ag-recycling system, suggesting that the development of Ag-separation technique is the most important for the application of this process into real operation.

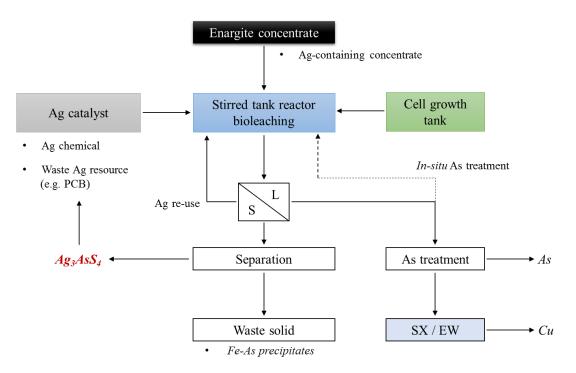


Fig. 8.2 Proposed flowsheet of Ag-catalyzed bioleaching of enargite concentrate.

In the AC-catalyzed bioleaching system, the basic concept of the process is similar to that in the presence of Ag; since AC is the more economical catalyst, the separation step is excluded (Fig. 8.3). The re-use of solid residue containing AC as the catalyst is, however, desirable for the low-cost process; this indicates that the investigation of repeatedly used AC in bioleaching provides us the valuable information. Based on the findings in this work, graphene structure was found a key factor controlling  $E_h$  behavior. This implies that graphite with high specific surface area could be replaceable with much stronger catalytic ability. Therefore, bioleaching of enargite concentrate using ultrafine graphite must also be tested for the further developed carbon-assisted bioleaching system.

### **Chapter 8 Conclusions**

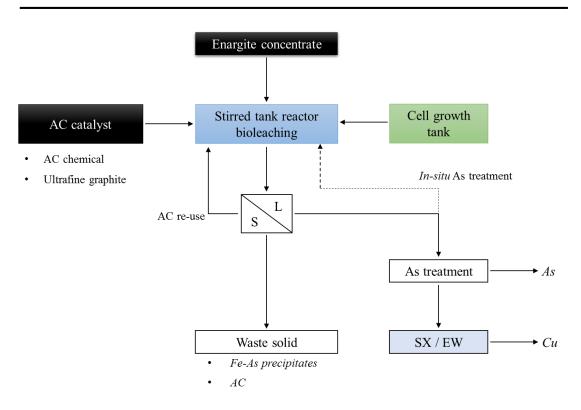


Fig. 8.3 Proposed flowsheet of AC-catalyzed bioleaching of enargite concentrate.

In both cases, As immobilization process still needs to be improved to achieve the selective leaching of Cu rather than As. Solubilized As is post-treated to be removed from the leachate, which is the reason of high-cost processing. In order to eliminate this post-treatment process, transferring the As-containing leachate back to the tank reactor is thought advantageous in *in-situ* As immobilization as Fe-As precipitates. Especially for AC-catalyzed bioleaching, circulation of As-containing leachate enables to gradually oxidize the As(III) to As(V), with former being mobile than the latter, which establishes the appropriate condition for further As immobilization. It is also expected that this circulation facilitates the aging of amorphous precipitates to highly crystalline scorodite (FeAsO4·2H<sub>2</sub>O). Therefore, stable As immobilization would be achievable, realizing safety Cu production from As-bearing concentrate.

#### Acknowledgements

First of all, I would like to express my sincere gratitude to my supervisor, associate Prof. Naoko Okibe, for her warm supervision, supports and encouragement throughout my doctor's course. Almost 9 years have passed since I met her for the first time, she always put her efforts into giving me opportunities to improve my research skills. I could not finish this work without her help. I am really honored to be her PhD student.

Besides, I would like to thank Prof. Tsuyoshi Hirajima, Prof. Keiko Sasaki, and associate Prof. Hajime Miki for their kind advices and constant encouragements. They always showed me what the ideal researcher is. I also wish to acknowledge the secretary in our lab., Mrs. Makiko Semba, for her technical supports.

I would like to show my appreciation to Prof. Hiroaki Nakano from Department of Materials Science and Engineering, Kyushu University as a member of my thesis committee, for his important suggestions and invaluable comments.

My appreciation also goes to Dr. Sabrina Hedrich, Dr. Axel Schipper, Dr. Ruiyong Zhang from Bundesanstalt fur Geowissenschaften und Rohstoffe (BGR), Germany. Dr. Naoaki Kataoka and Mr. Ono from Swing Corporation for accepting me as an internship student and for taking care of me.

I would like to thank associate Prof. Maiko Nishibori (Department of Energy and Material Sciences, Kyushu University), associate Prof. Junichiro Ishibashi and Mr. Kazuhiko Shimada (Department of Earth and Planetary Sciences, Graduate School of Science, Kyushu University), for giving me a valuable opportunity of lab-rotation. My special thanks also go to assistant Prof. Takahiro Funatsu and Ms. Miwa Hirashima and Ms. Minako Matsue in Advanced Graduate Program in Global Strategy for Green Asia, for their kind supports.

I would like to express my appreciation to Advanced Graduate Program in Global Strategy for Green Asia. This educational program provided me with meaningful opportunities to learn and understand a relationship between technologies and society. I am also grateful for financial support provided by the program.

I would like to show my acknowledgment to JX Nippon Mining & Metals Corporation for kindly providing us with enargite concentrate.

The XAFS experiments were performed at Kyushu University Beamline (Saga-

LS/BL06) with the proposal of No. 2016IK003, 2016IIK013, and 2016IIIK006 under the supervision of associate Prof. Takeharu Sugiyama.

Many thanks to Lab. Members in Mineral Processing, Recycling and Environmental Remediation Laboratory as follows; Dr. Sayo Moriyama, Dr. Mohsen M. Farahat, Dr. Ahmed M. Elmahdy, Dr. Paulmanickam Koilraj, Dr. Widi Astuti, Dr. Mutia Dewi Yuniati, Dr. Wuhui Luo, Dr. Yusei Masaki, Dr. Atsunori Tayaoka, Dr. XiangChun Liu, Dr. Gde Pandhe Wisnu Suyantara, Dr. Binglin Guo, Dr. Intan Nurul Rizki, Dr. Masahito Tanaka, Dr. Santisak Kitjanukit, Dr. Kojo Twum Konadu, Dr. Chitiphon Chuaicham, Masaharu Koga, Masashi Maki, Shiori Morishita, Taichi Momoki, Osamu Ichikawa, Mari Yoshida, Yuken Fukano, Daisuke Nakayama, Hidekazu Matsuoka, Yu Takaki, Kenta Toshiyuki, Akinobu Iguchi, Katsutoshi Tsutsumi, Takahiro Matsumoto, Tsubasa Oji, Akihiro Inoue, Shugo Nagato, Kazuyoshi Oka, Melisa Pramesti Dewi, Yuta Era, Takeru Fukumori, Taigen Masuyama, Ryota Matsushita, Yusuke Hotta, Kyohei Takamatsu, Yuta Kamura, Yoshikazu Hayashi, Yu Hirayama, Yukihiro Muta, Tian Quanzhi, Ryohei Nishi, Haruki Noguchi, Shunsuke Imamura, Shingo Nakama, Shogo Nagano, Yu Tanaka, Yuya Komori, Yuta Orii, Yuna Watanabe, Kinato Yagi, Wang Mengmeng, Diego Moizes Mendoza Flores, Kohei Nonaka, Kaito Hayashi, Ryotaro Sakai, Zenta Shirozu, and Yuki Semoto. It was great pleasure to be together in the laboratory.

Last but not least, my great respect and gratitude go to my parents, Kumi Oyama and Eiji Oyama, for their affectionate support and encouragement.

March 2020, Keishi Oyama Kyushu University Fukuoka, Japan